

Appendix B – Hydrologic Parameters & HEC-1 Analyses

- Proposed Condition Standard Form 4
- Proposed Condition HEC-1

TIME OF CONCENTRATION / LAG TIME DETERMINATION - less than 1 mi2



**DURANGO & GRAND MONTECITO
ULTIMATE CONDITION**

Project No: 090935040
Date: 6/20/24
Calculated by: CK

SUB-BASIN DATA					INITIAL / OVERLAND TIME (Ti)			TRAVEL TIME (Tt)						T _{lag}	REMARKS		
Basin ID	DEV./UNDEV. (D or U)	CN	K	AREA	AREA	INITIAL LENGTH	SLOPE	Ti	TRAVEL LENGTH	SLOPE	V ₁	V ₂	Tt	Tc	Tc Check	T _{lag}	100 YR RAINFALL
				Ac	Mi ²	Feet	%	Min	Feet	%	VELOCITY	VELOCITY	Min	Min	Min	0.6Tc/60	INCHES
(1)	(2)	(3)	(4)	(5a)	(5b)	(6)	(7)	(8)	(9)	(10)	(10a)	(10b)	(11)	(12)	(13)	(14)	(15)
ON	D	92.0	0.8244	8.80	0.0138	35	1.00	2.9	845	1.20	2.2	3.4	5.5	8.4	14.9	0.084	3.00
GMP	D	98.0	0.9036	0.75	0.0012	13	2.30	1.0	344	0.40	1.3	1.9	4.5	5.5	12.0	0.055	3.00

NOTE:

(1) Subbasin Name	(7) Initial Slope	(10b) V ₂ applies to the remaining travel distance;	(15) Rainfall in inches
(2) Developed or Undeveloped Subbasin	(8) $T_i = 1.8 (1.1 - K) L^{1/2} / S^{1/3}$	Developed $V_2 = 30.6(S/100)^{1/2}$	
(3) Curve Number (See Subbasin CN Calculations)	(9) Travel Length	(11) $T_t = 500/(V_1*60) + (Travel\ Length - 500)/(V_2*60)$	
(4) $K = 0.0132 (CN) - 0.39$	(10) Slope	(12) $T_c = T_i + T_t$	
(5a) & (5b) Area	(10a) Slope V ₁ applies to the first 500 feet of travel distance;	(13) Tc Check = L/180+10 (select smaller Tc)	
(6) Initial Length	Developed $V_1 = 20.2(S/100)^{1/2}$	(14) Tlag = 0.6 Tc/60	

REFERENCE: Calculations based on the Clark County Regional Flood Control District HCDDM

STANDARD FORM 4

*Referenced/Revised from Ariva Retail and Office Center Study (PW21-12227)

ULT. OUT

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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 20JUN24 TIME 13:00:47 *
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS: WRITE STAGE FREQUENCY, DSS: READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE: GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*DIAGRAM

*** FREE ***

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1 ID
2 ID *****
3 ID *
4 ID * DURANGO & GRAND MONTECITO *
5 ID * ULTIMATE CONDITION *
6 ID *
7 ID * PROJECT No: _ _ _ 192438000 *
8 ID * FILE: _ _ _ _ _ ULT.H1 *
9 ID * DATE MODELED: _ _ 04/16/24 *
10 ID * MODELED BY: _ _ _ SS *
11 ID *
12 ID *****
13 ID
14 ID *****
15 ID * RETURN PERIOD: _ _ 100- & 10- YEAR *
16 ID * DISTRIBUTION: _ _ 6-HOUR SDN3 *
17 ID *****
18 ID
19 *DIAGRAM
IT 5 0 0 300
20 IO 5 0 0
21 IN 5 0 0
22 JR PREC 0.56 1.00
*
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23 KK *DOF3
24 BA .0016
25 PB 3.00
26 PC .000 .020 .057 .070 .087 .108 .124 .130 .130 .130
27 PC .130 .130 .130 .133 .140 .142 .148 .158 .172 .181
28 PC .190 .197 .199 .200 .201 .204 .214 .229 .241 .249
29 PC .251 .256 .270 .278 .281 .283 .295 .322 .352 .409
30 PC .499 .590 .710 .744 .781 .812 .819 .835 .851 .856
31 PC .860 .868 .876 .888 .910 .926 .937 .950 .970 .976
32 PC .982 .985 .987 .989 .990 .993 .993 .994 .995 .998
33 PC .998 .999 1.00
34 LS 0 92.0
35 UD .053
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36 KK *DOF1
37 BA .0093
38 LS 0 92.0
39 UD .076
*
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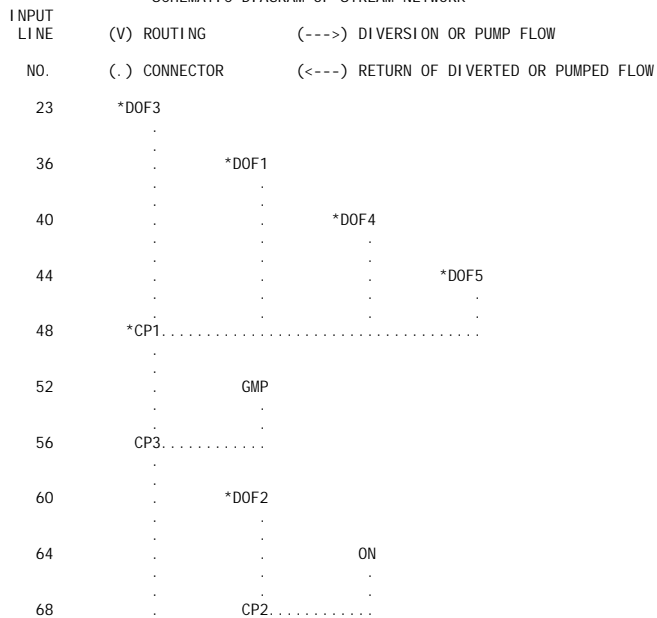
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40 KK *DOF4
41 BA .0027
42 LS 0 92.0
43 UD .079
*
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LINE	ID	1	2	3	4	5	6	7	8	9	10
44	KK	*DOF5									
45	BA	.0011									
46	LS	0	92.0								
47	UD	.050									
	*										
48	KK	*CP1									
49	KM	COMBINES *DOF3, *DOF1, *DOF4, AND *DOF5									
50	KM	SURFACE FLOW IN GRAND MONTECITO PKWY									
51	HC	4									
	*										
52	KK	GMP									
53	BA	.0012									
54	LS	0	98.0								
55	UD	.055									
	*										
56	KK	CP3									
57	KM	COMBINES *CP1 AND GMP									
58	KM	SURFACE FLOW IN GRAND MONTECITO PKWY									
59	HC	2									
	*										
60	KK	*DOF2									
61	BA	.0066									
62	LS	0	92.0								
63	UD	.092									
	*										
64	KK	ON									
65	BA	.0138									
66	LS	0	92.0								
67	UD	.084									
	*										
68	KK	CP2									
69	KM	COMBINES *DOF2 AND ON									
70	KM	STORM DRAIN FLOW									
71	HC	2									
	*										
72	ZZ										

1

SCHEMATIC DIAGRAM OF STREAM NETWORK



(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 20JUN24 TIME 13:00:47 *
    
```

```

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* U. S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
    
```

```

*****
*
*   DURANGO & GRAND MONTECITO
*   ULTIMATE CONDITION
*
*   PROJECT No:  _ _ _ 192438000
*   FILE:  _ _ _ _ _ ULT.H1
*   DATE MODELED:  _ _ 04/16/24
*   MODELED BY:  _ _ _ SS
*
*****
*
*   RETURN PERIOD:  _ _100- & 10- YEAR
*   DI STRI BUTION:  _ _ 6-HOUR SDN3
*
*****
    
```

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20 IO      OUTPUT CONTROL VARIABLES
           IPRNT      5  PRINT CONTROL
           IPLOT      0  PLOT CONTROL
           OSCAL      0. HYDROGRAPH PLOT SCALE

IT         HYDROGRAPH TIME DATA
           NMIN       5  MINUTES IN COMPUTATION INTERVAL
           IDATE      1  0  STARTING DATE
           I TIME     0000 STARTING TIME
           NQ         300 NUMBER OF HYDROGRAPH ORDINATES
           NDDATE     2  0  ENDING DATE
           NDTIME     0055 ENDING TIME
           ICENT      19  CENTURY MARK

           COMPUTATION INTERVAL .08 HOURS
           TOTAL TIME BASE     24.92 HOURS
    
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ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME    ACRE- FEET
SURFACE AREA      ACRES
TEMPERATURE       DEGREES FAHRENHEIT
    
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JP         MULTI-PLAN OPTION
           NPLAN      1  NUMBER OF PLANS
    
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JR         MULTI-RATIO OPTION
           RATIOS OF PRECIPITATION
           .56      1.00
    
```

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	*DOF3	.00	1	FLOW	2. 4.
				TIME	3.50 3.50
HYDROGRAPH AT					
+	*DOF1	.01	1	FLOW	9. 19.
				TIME	3.50 3.50
HYDROGRAPH AT					
+	*DOF4	.00	1	FLOW	3. 5.
				TIME	3.50 3.50
HYDROGRAPH AT					
+	*DOF5	.00	1	FLOW	1. 2.
				TIME	3.50 3.50
4 COMBINED AT					
+	*CP1	.01	1	FLOW	14. 30.
				TIME	3.50 3.50
HYDROGRAPH AT					
+	GMP	.00	1	FLOW	2. 3.

				TIME	3.50	3.50	ULT. OUT
2 COMBINED AT							
+	CP3	.02	1	FLOW	16.	33.	
				TIME	3.50	3.50	
HYDROGRAPH AT							
+	*DOF2	.01	1	FLOW	6.	13.	
				TIME	3.50	3.50	
HYDROGRAPH AT							
+	ON	.01	1	FLOW	13.	27.	
				TIME	3.50	3.50	
2 COMBINED AT							
+	CP2	.02	1	FLOW	19.	40.	
				TIME	3.50	3.50	

*** NORMAL END OF HEC-1 ***

Appendix C – Hydraulic Calculations

- Normal Depth Calculations – Onsite Streets
- Drop Inlet Calculations
- WSPG Model

Worksheet for ON3S

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	0.840 %
Discharge	8.00 cfs

Section Definitions

	Station (ft)	Elevation (ft)	
	0+00.00		0.48
	0+05.00		0.38
	0+06.50		0.00
	0+07.50		0.08
	0+07.50		0.13
	0+42.50		0.83
	0+42.50		0.78
	0+43.50		0.70
	0+45.00		1.08

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00.00, 0.48)	(0+45.00, 1.08)	0.016

Options

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results

Normal Depth	0.44 ft
Roughness Coefficient	0.016
Elevation	0.44 ft
Elevation Range	0.00 to 1.08 ft
Flow Area	3.3 ft ²
Wetted Perimeter	21.07 ft
Hydraulic Radius	0.15 ft
Top Width	20.97 ft
Normal Depth	0.44 ft
Critical Depth	0.45 ft
Critical Slope	0.693 %
Velocity	2.45 ft/s

Worksheet for ON3S

Results

Velocity Head	0.09 ft
Specific Energy	0.53 ft
Froude Number	1.097
Flow Type	Supercritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

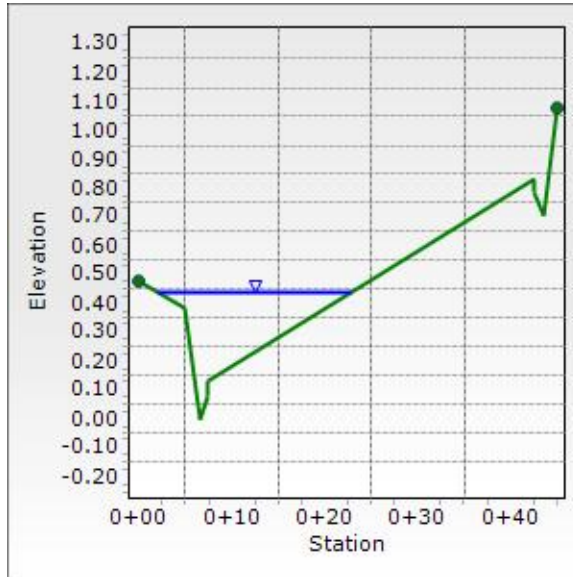
GVF Output Data

Upstream Depth	0.00 ft
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	0.44 ft
Critical Depth	0.45 ft
Channel Slope	0.840 %
Critical Slope	0.693 %

Cross Section for ON3S

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth

Input Data	
Channel Slope	0.840 %
Normal Depth	0.44 ft
Discharge	8.00 cfs



Worksheet for ON8

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	1.890 %
Discharge	4.00 cfs

Section Definitions

	Station (ft)	Elevation (ft)	
	0+00.00		0.38
	0+01.50		0.00
	0+02.50		0.08
	0+02.50		0.13
	0+20.00		0.48
	0+37.50		0.13
	0+37.50		0.08
	0+38.50		0.00
	0+40.00		0.38

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient	
(0+00.00, 0.38)	(0+40.00, 0.38)		0.016

Options

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results

Normal Depth	0.26 ft
Roughness Coefficient	0.016
Elevation	0.26 ft
Elevation Range	0.00 to 0.48 ft
Flow Area	1.6 ft ²
Wetted Perimeter	17.25 ft
Hydraulic Radius	0.09 ft
Top Width	17.08 ft
Normal Depth	0.26 ft
Critical Depth	0.29 ft
Critical Slope	0.799 %
Velocity	2.57 ft/s

Worksheet for ON8

Results

Velocity Head	0.10 ft
Specific Energy	0.36 ft
Froude Number	1.502
Flow Type	Supercritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

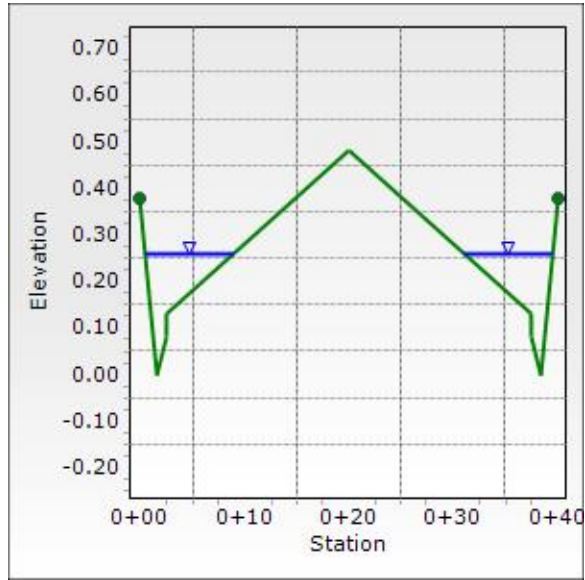
GVF Output Data

Upstream Depth	0.00 ft
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	0.26 ft
Critical Depth	0.29 ft
Channel Slope	1.890 %
Critical Slope	0.799 %

XS for ON8

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth

Input Data	
Channel Slope	1.890 %
Normal Depth	0.26 ft
Discharge	4.00 cfs



Worksheet for ON13

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Channel Slope	1.890 %
Discharge	3.00 cfs

Section Definitions

	Station (ft)	Elevation (ft)	
	0+00.00		0.38
	0+01.50		0.00
	0+02.50		0.08
	0+02.50		0.13
	0+15.00		0.38
	0+27.50		0.13
	0+27.50		0.08
	0+28.50		0.00
	0+30.00		0.38

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00.00, 0.38)	(0+30.00, 0.38)	0.016

Options

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results

Normal Depth	0.24 ft
Roughness Coefficient	0.016
Elevation	0.24 ft
Elevation Range	0.00 to 0.38 ft
Flow Area	1.2 ft ²
Wetted Perimeter	15.17 ft
Hydraulic Radius	0.08 ft
Top Width	15.00 ft
Normal Depth	0.24 ft
Critical Depth	0.27 ft
Critical Slope	0.828 %
Velocity	2.41 ft/s

Worksheet for ON13

Results

Velocity Head	0.09 ft
Specific Energy	0.33 ft
Froude Number	1.471
Flow Type	Supercritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

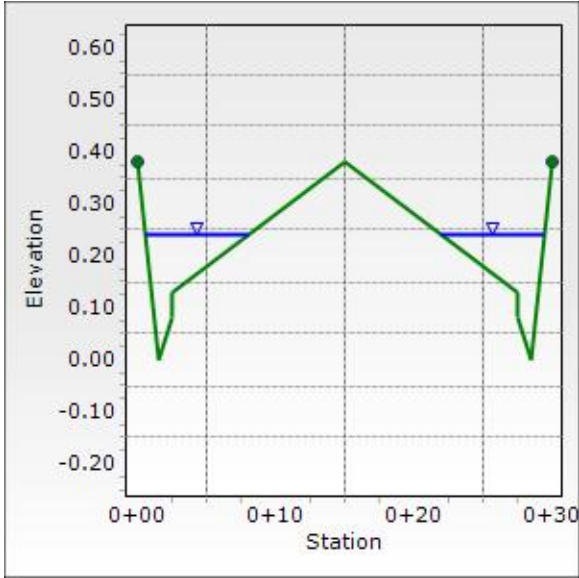
GVF Output Data

Upstream Depth	0.00 ft
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	0.24 ft
Critical Depth	0.27 ft
Channel Slope	1.890 %
Critical Slope	0.828 %

XS for ON13

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth

Input Data	
Channel Slope	1.890 %
Normal Depth	0.24 ft
Discharge	3.00 cfs



Worksheet for ON14

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth

Input Data	
Channel Slope	0.500 %
Discharge	4.90 cfs

Section Definitions

	Station (ft)	Elevation (ft)
	0+00.00	0.48
	0+05.00	0.38
	0+06.50	0.00
	0+07.50	0.08
	0+07.50	0.13
	0+42.50	0.83
	0+42.50	0.78
	0+43.50	0.70
	0+45.00	1.08

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00.00, 0.48)	(0+45.00, 1.08)	0.016

Options

Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results

Normal Depth	0.41 ft
Roughness Coefficient	0.016
Elevation	0.41 ft
Elevation Range	0.00 to 1.08 ft
Flow Area	2.7 ft ²
Wetted Perimeter	18.03 ft
Hydraulic Radius	0.15 ft
Top Width	17.92 ft
Normal Depth	0.41 ft
Critical Depth	0.38 ft
Critical Slope	0.715 %
Velocity	1.84 ft/s

Worksheet for ON14

Results

Velocity Head	0.05 ft
Specific Energy	0.46 ft
Froude Number	0.839
Flow Type	Subcritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

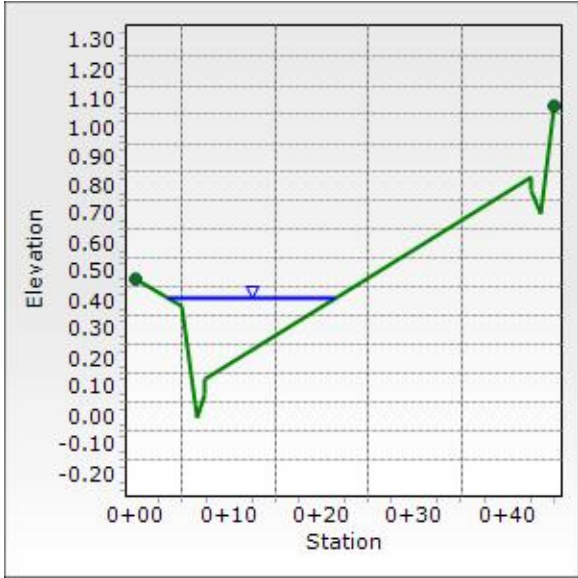
GVF Output Data

Upstream Depth	0.00 ft
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	0.00 ft/s
Upstream Velocity	0.00 ft/s
Normal Depth	0.41 ft
Critical Depth	0.38 ft
Channel Slope	0.500 %
Critical Slope	0.715 %

XS for ON14

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth

Input Data	
Channel Slope	0.500 %
Normal Depth	0.41 ft
Discharge	4.90 cfs



Type CM Drop Inlet Sizing in Sump

DI#3

Known:

D_p = Ponding Depth at Inlet	0.33	ft
W = Gutter Width	1.5	ft
L_g = Length of Grate	12.5	ft
L_c = Length of Curb Opening	14.5	ft
H_c = Curb Opening Height	0.5	ft
C_{wc} = Weir coefficient for curb opening	2.3	
C_{wg} = Weir coefficient for grate	3.0	
C_o = Orifice coefficient	0.67	
R_o = Grate opening factor	0.60	
C_{fg} = Clogging Factor for Grate	50	%
C_{fc} = Clogging Factor for Curb Opening	50	%

Grate Capacity Calculations:

P_g = Active grate weir length (agwl) = $2*W+L_g$	15.50 ft
P_{agl} Adjusted agwl = $2*(1-C_{fg}/100)*W+L_g$	14.00 ft
A_g = Grate area = $W*L_g$	18.75 ft ²
A_{aga} = Adjusted open grate area = $A_g*R_o*(1-C_{fg}/100)$	5.63 ft ²
check - If $D_p < 1.792*A_{aga}/P_{agl}$; weir; else orifice	weir
Q_{ig} = Flow intercepted by grate If "weir" controls $Q_{ig}=C_{wg}*P_{agl}*D_p^{1.5}$ If "orifice" controls $Q_{ig}=C_o*A_{aga}*(64.4*D_p)^{0.5}$	8.0 cfs

Curb Opening Capacity Calculations

P_c = Active curb opening weir length (acowl) = $L_c+1.8*W$	17.20 ft
P_{acl} Adjusted acowl = $L_c+1.8*(1-C_{fc}/100)*W$	15.85 ft
A_c = curb opening area (coa) = L_c*H_c	7.25 ft ²
A_{aca} = Adjusted coa = $A_c*(1-C_{fc}/100)$	3.63 ft ²
check - If $D_p < H_c$; weir; else orifice	weir
Q_{ic} = Flow intercepted by curb opening If "weir" controls $Q_{ic}=C_{wc}*P_{acl}*D_p^{1.5}$ If "orifice" controls $Q_{ic}=C_o*A_{aca}*(64.4*D_p-H_c/2)^{0.5}$	7.0 cfs

Total Inlet Calculations

Q_{ti} = Total flow intercepted = $Q_{ig}+Q_{ic}$	15.0 cfs
q = Interception per unit ratio = Q_{ti}/L_g	1.03 cfs/ft

Type CM Drop Inlet Sizing on a C. G.

DI#4

Known:

Q _s = Half Street Flow	4.9	cfs
S _o = Longitudinal Slope	0.005	ft/ft
n= Manning's Roughness Coefficient	0.016	
V _s = Flow Velocity	1.84	fps
D= Flow Depth	0.41	ft
S _x = Street Transverse Slope	0.02	ft/ft
W= Gutter Width	2	ft
a= Gutter Depression	5.0	in
L _g = Length of Grate	7.5	ft
L _c = Length of Curb Opening	9.5	ft
C _{fg} = Clogging Factor for Grate	50	%
C _{fc} = Clogging Factor for Curb Opening	50	%

Grate Capacity Calculations:

R _f = Frontal flow factor = $1-0.09*(V_s-V_o)$ if $V_s>V_o$; else $R_f=1$	1.00
V _o = Splash over velocity= $p+q*(L_g*(1-(C_{fg}/100)))-r*(L_g*(1-(C_{fg}/100)))^2+s*(L_g*(1-(C_{fg}/100)))^3$	8.71 fps
E _o = Grate flow ratio = Q_w/Q_s	0.28
Q _w = Frontal flow= A_w*V_s	1.36 cfs
Q _x = Side flow = Q_s-Q_w	3.54 cfs
R _s = Side flow factor = $1/(1+(0.15*V_s^{1.8})/(S_x*(L_g*(1-C_{fg}/100))^{2.3}))$	0.48
Q _{ig} = Flow intercepted = $[R_f*E_o+R_s*(1-E_o)]*Q_s$	3.1 cfs
†p=1.76;q=3.12;r=0.45;s=0.03 (based on Bar P 1-1/8 grate)	

Curb Opening Capacity Calculations

S _e = Equivalent cross slope = $S_x+S_w*E_o$	0.079 ft/ft
S _w = Gutter cross slope = $(0.137+afeet)/W$	0.214 ft/ft
L _t = Total interception L = $0.60*Q_s^{0.42}*S_o^{0.30}*(1/n*S_e)^{0.6}$	13.06 ft
Q _{ic} = Flow intercepted = $(1-(1-(L_c*(1-C_{fc}/100))/L_t)^{1.8})*Q_s$	2.7 cfs

Total Inlet Calculations

Q _{ti} = Total flow intercepted = $Q_{ig}+Q_{ic}$	4.9 cfs
Q _{tq} = Flow bypass = Q_s-Q_{ti}	0.0 cfs
q= Interception per unit ratio = Q_{ti}/L_g	0.52 cfs/ft
E _q = Efficiency = $(Q_{ti}/Q_s)*100$	100 %

Type CM Drop Inlet Sizing on a C. G.

DI#5

Known:

Q _s = Half Street Flow	5.5	cfs
S _o = Longitudinal Slope	0.0064	ft/ft
n= Manning's Roughness Coefficient	0.016	
V _s = Flow Velocity	2.07	fps
D= Flow Depth	0.41	ft
S _x = Street Transverse Slope	0.02	ft/ft
W= Gutter Width	2	ft
a= Gutter Depression	5.0	in
L _g = Length of Grate	5.0	ft
L _c = Length of Curb Opening	7.0	ft
C _{fg} = Clogging Factor for Grate	50	%
C _{fc} = Clogging Factor for Curb Opening	50	%

Grate Capacity Calculations:

R _f = Frontal flow factor = 1-0.09*(V _s -V _o) if V _s >V _o ; else R _f =1	1.00
V _o = Splash over velocity= $p+q*(L_g*(1-(C_{fg}/100)))-r*(L_g*(1-(C_{fg}/100)))^2+s*(L_g*(1-(C_{fg}/100)))^3$	7.22 fps
E _o = Grate flow ratio = Q _w /Q _s	0.28
Q _w = Frontal flow=A _w *V _s	1.52 cfs
Q _x = Side flow = Q _s -Q _w	3.98 cfs
R _s = Side flow factor = $1/(1+(0.15*V_s^{1.8})/(S_x*(L_g*(1-C_{fg}/100))^{2.3}))$	0.23
Q _{ig} = Flow intercepted = [R _f *E _o +R _s *(1-E _o)]*Q _s	2.4 cfs
†p=1.76;q=3.12;r=0.45;s=0.03 (based on Bar P 1-1/8 grate)	

Curb Opening Capacity Calculations

S _e = Equivalent cross slope = S _x +S _w *E _o	0.079 ft/ft
S _w = Gutter cross slope = (0.137+afeet)/W	0.214 ft/ft
L _t = Total interception L = $0.60*Q_s^{0.42}*S_o^{0.30}*(1/n*S_e)^{0.6}$	14.75 ft
Q _{ic} = Flow intercepted = $(1-(1-(L_c*(1-C_{fc}/100))/L_t)^{1.8})*Q_s$	2.1 cfs

Total Inlet Calculations

Q _{ti} = Total flow intercepted = Q _{ig} +Q _{ic}	4.6 cfs
Q _{tq} = Flow bypass = Q _s -Q _{ti}	0.9 cfs
q= Interception per unit ratio = Q _{ti} /L _g	0.65 cfs/ft
E _q = Efficiency = (Q _{ti} /Q _s)*100	83 %

Type CM Drop Inlet Sizing in Sump

DI#6

Known:

D_p = Ponding Depth at Inlet	0.42	ft
W = Gutter Width	1.5	ft
L_g = Length of Grate	7.5	ft
L_c = Length of Curb Opening	9.5	ft
H_c = Curb Opening Height	0.5	ft
C_{wc} = Weir coefficient for curb opening	2.3	
C_{wg} = Weir coefficient for grate	3.0	
C_o = Orifice coefficient	0.67	
R_o = Grate opening factor	0.60	
C_{fg} = Clogging Factor for Grate	50	%
C_{fc} = Clogging Factor for Curb Opening	50	%

Grate Capacity Calculations:

P_g = Active grate weir length (agwl) = $2*W+L_g$	10.50	ft
P_{agl} Adjusted agwl = $2*(1-C_{fg}/100)*W+L_g$	9.00	ft
A_g = Grate area = $W*L_g$	11.25	ft ²
A_{aga} = Adjusted open grate area = $A_g*R_o*(1-C_{fg}/100)$	3.38	ft ²
check - If $D_p < 1.792*A_{aga}/P_{agl}$; weir; else orifice	weir	
Q_{ig} = Flow intercepted by grate If "weir" controls $Q_{ig}=C_{wg}*P_{agl}*D_p^{1.5}$ If "orifice" controls $Q_{ig}=C_o*A_{aga}*(64.4*D_p)^{0.5}$	7.3	cfs

Curb Opening Capacity Calculations

P_c = Active curb opening weir length (acowl) = $L_c+1.8*W$	12.20	ft
P_{acl} Adjusted acowl = $L_c+1.8*(1-C_{fc}/100)*W$	10.85	ft
A_c = curb opening area (coa) = L_c*H_c	4.75	ft ²
A_{aca} = Adjusted coa = $A_c*(1-C_{fc}/100)$	2.38	ft ²
check - If $D_p < H_c$; weir; else orifice	weir	
Q_{ic} = Flow intercepted by curb opening If "weir" controls $Q_{ic}=C_{wc}*P_{acl}*D_p^{1.5}$ If "orifice" controls $Q_{ic}=C_o*A_{aca}*(64.4*D_p-H_c/2)^{0.5}$	6.7	cfs

Total Inlet Calculations

Q_{ti} = Total flow intercepted = $Q_{ig}+Q_{ic}$	14.0	cfs
q = Interception per unit ratio = Q_{ti}/L_g	1.47	cfs/ft

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia. -FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1000.000	2473.000	3.400	2476.400	38.50	7.84	.96	2477.36	.00	2.10	.00	2.500	.000	.00	0 .0
35.720	.0100					.0088	.31	3.40	.00	1.92	.013	.00	.00	PIPE
1035.720	2473.357	3.358	2476.715	38.50	7.84	.96	2477.67	.00	2.10	.00	2.500	.000	.00	0 .0
4.000	.0123					.0088	.04	3.36	.00	1.77	.013	.00	.00	PIPE
1039.720	2473.406	3.675	2477.081	38.50	7.84	.96	2478.04	.00	2.10	.00	2.500	.000	.00	0 .0
100.715	.0143					.0088	.89	3.68	.00	1.67	.013	.00	.00	PIPE
1140.435	2474.846	3.123	2477.969	38.50	7.84	.96	2478.92	.00	2.10	.00	2.500	.000	.00	0 .0
JUNCT STR	.0123					.0069	.03	.00	.00		.013	.00	.00	PIPE
1144.435	2474.895	3.906	2478.801	29.00	5.91	.54	2479.34	.00	1.84	.00	2.500	.000	.00	0 .0
56.404	.0100					.0050	.28	3.91	.00	1.55	.013	.00	.00	PIPE
1200.839	2475.459	3.624	2479.083	29.00	5.91	.54	2479.63	.00	1.84	.00	2.500	.000	.00	0 .0
JUNCT STR	.0128					.0031	.01	.00	.00		.013	.00	.00	PIPE
1204.839	2475.510	4.130	2479.640	14.00	4.46	.31	2479.95	.00	1.35	.00	2.000	.000	.00	0 .0
179.353	.0157					.0038	.68	4.13	.00	.99	.013	.00	.00	PIPE
1384.192	2478.327	2.000	2480.327	14.00	4.46	.31	2480.64	.00	1.35	.00	2.000	.000	.00	0 .0
6.632	.0157					.0035	.02	2.00	.00	.99	.013	.00	.00	PIPE
1390.825	2478.431	1.909	2480.340	14.00	4.53	.32	2480.66	.00	1.35	.83	2.000	.000	.00	0 .0

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia. -FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1390.825	2478.431	.918	2479.349	14.00	9.95	1.54	2480.89	.00	1.35	1.99	2.000	.000	.00	0 .0
7.828	.0157					.0206	.16	.92	2.09	.99	.013	.00	.00	PIPE
1398.652	2478.554	.918	2479.472	14.00	9.95	1.54	2481.01	.00	1.35	1.99	2.000	.000	.00	0 .0
19.252	.0157					.0220	.42	.92	2.09	.99	.013	.00	.00	PIPE
1417.904	2478.856	.885	2479.741	14.00	10.43	1.69	2481.43	.00	1.35	1.99	2.000	.000	.00	0 .0
4.000	.0198					.0236	.09	.89	2.24	.93	.013	.00	.00	PIPE
1421.904	2478.935	.882	2479.817	14.00	10.49	1.71	2481.53	.00	1.35	1.99	2.000	.000	.00	0 .0
85.339	.0237					.0237	2.03	.88	2.26	.88	.013	.00	.00	PIPE
1507.243	2480.962	.882	2481.844	14.00	10.49	1.71	2483.55	.00	1.35	1.99	2.000	.000	.00	0 .0
85.119	.0237					.0246	2.10	.88	2.26	.88	.013	.00	.00	PIPE
1592.362	2482.983	.864	2483.848	14.00	10.77	1.80	2485.65	.00	1.35	1.98	2.000	.000	.00	0 .0
42.642	.0237					.0273	1.16	.86	2.34	.88	.013	.00	.00	PIPE
1635.004	2483.996	.834	2484.830	14.00	11.29	1.98	2486.81	.00	1.35	1.97	2.000	.000	.00	0 .0
5.000	.0298					.0290	.14	.83	2.51	.83	.013	.00	.00	PIPE
1640.004	2484.145	.834	2484.979	14.00	11.28	1.98	2486.95	.00	1.35	1.97	2.000	.000	.00	0 .0

MAIN OUT

9.341	.0360						.0281	.26	.83	2.51	.79	.013	.00	.00	PIPE
1649.345	2484.481	.849	2485.330	14.00	11.02	1.89	2487.22	.00	1.35	1.98	2.000	.000	.00	0	.0
13.383	.0360						.0255	.34	.85	2.42	.79	.013	.00	.00	PIPE

FILE: MAIN.WSW
 W S P G W - CIVILDESIGN Version 14.06
 Program Package Serial Number: 1911
 WATER SURFACE PROFILE LISTING
 DURANGO AND GRAND MONTECITO
 MAIN1
 KHA JOB# 092935040 BY: SS/MS
 Date: 6-20-2024 Time: 2: 2:29
 0
 PAGE 3

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia. -FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1662.728	2484.963	.880	2485.843	14.00	10.51	1.72	2487.56	.00	1.35	1.99	2.000	.000	.00	0 .0
9.080	.0360					.0224	.20	.88	2.26	.79	.013	.00	.00	PIPE
1671.807	2485.290	.913	2486.203	14.00	10.02	1.56	2487.76	.00	1.35	1.99	2.000	.000	.00	0 .0
6.606	.0360					.0197	.13	.91	2.11	.79	.013	.00	.00	PIPE
1678.414	2485.528	.947	2486.475	14.00	9.56	1.42	2487.89	.00	1.35	2.00	2.000	.000	.00	0 .0
4.995	.0360					.0174	.09	.95	1.97	.79	.013	.00	.00	PIPE
1683.409	2485.708	.983	2486.691	14.00	9.11	1.29	2487.98	.00	1.35	2.00	2.000	.000	.00	0 .0
3.843	.0360					.0153	.06	.98	1.83	.79	.013	.00	.00	PIPE
1687.252	2485.846	1.020	2486.866	14.00	8.69	1.17	2488.04	.00	1.35	2.00	2.000	.000	.00	0 .0
2.977	.0360					.0135	.04	1.02	1.71	.79	.013	.00	.00	PIPE
1690.229	2485.953	1.060	2487.013	14.00	8.28	1.07	2488.08	.00	1.35	2.00	2.000	.000	.00	0 .0
2.297	.0360					.0119	.03	1.06	1.59	.79	.013	.00	.00	PIPE
1692.525	2486.036	1.101	2487.137	14.00	7.90	.97	2488.11	.00	1.35	1.99	2.000	.000	.00	0 .0
1.740	.0360					.0105	.02	1.10	1.47	.79	.013	.00	.00	PIPE
1694.265	2486.099	1.145	2487.244	14.00	7.53	.88	2488.12	.00	1.35	1.98	2.000	.000	.00	0 .0
1.272	.0360					.0093	.01	1.14	1.37	.79	.013	.00	.00	PIPE
1695.538	2486.145	1.191	2487.335	14.00	7.18	.80	2488.14	.00	1.35	1.96	2.000	.000	.00	0 .0
.865	.0360					.0082	.01	1.19	1.27	.79	.013	.00	.00	PIPE

FILE: MAIN.WSW
 W S P G W - CIVILDESIGN Version 14.06
 Program Package Serial Number: 1911
 WATER SURFACE PROFILE LISTING
 DURANGO AND GRAND MONTECITO
 MAIN1
 KHA JOB# 092935040 BY: SS/MS
 Date: 6-20-2024 Time: 2: 2:29
 0
 PAGE 4

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia. -FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1696.402	2486.176	1.239	2487.416	14.00	6.85	.73	2488.14	.00	1.35	1.94	2.000	.000	.00	0 .0
.499	.0360					.0073	.00	1.24	1.18	.79	.013	.00	.00	PIPE
1696.901	2486.194	1.291	2487.485	14.00	6.53	.66	2488.15	.00	1.35	1.91	2.000	.000	.00	0 .0
.163	.0360					.0064	.00	1.29	1.09	.79	.013	.00	.00	PIPE
1697.065	2486.200	1.348	2487.547	14.00	6.22	.60	2488.15	.00	1.35	1.88	2.000	.000	.00	0 .0

MAIN_LAT1.WSW

T1 DURANGO AND GRAND MONTECITO
T2 MAIN_LAT1
T3 KHA JOB# 092935040 BY: SS/MS

0

SO	1000.0002475.478	30		2479.9					
R	1032.7722475.806	30	.013		.000	.000	.000	.000	0
R	1036.7722475.901	30	.013		.000	-64.300	.000	.000	1
R	1055.3232476.596	30	.013		.000	.000	.000	.000	0
SH	1055.3232476.596	30							
CD	6	4	0	.000	0.500	.000	.000	.000	.00
CD	8	4	0	.000	0.670	.000	.000	.000	.00
CD	12	4	0	.000	1.000	.000	.000	.000	.00
CD	18	4	0	.000	1.500	.000	.000	.000	.00
CD	24	4	0	.000	2.000	.000	.000	.000	.00
CD	30	4	0	.000	2.500	.000	.000	.000	.00
CD	36	4	0	.000	3.000	.000	.000	.000	.00
CD	42	4	0	.000	3.500	.000	.000	.000	.00
CD	48	4	0	.000	4.000	.000	.000	.000	.00
CD	54	4	0	.000	4.500	.000	.000	.000	.00
CD	60	4	0	.000	5.000	.000	.000	.000	.00
CD	66	4	0	.000	5.500	.000	.000	.000	.00
CD	72	4	0	.000	6.000	.000	.000	.000	.00
Q				15.000	.0				

WATER SURFACE PROFILE LISTING
 DURANGO AND GRAND MONTECITO
 MAIN_LAT1
 KHA JOB# 092935040 BY: SS/MS

Date: 6-20-2024 Time: 1:57:44

0

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia. -FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1000.000	2475.478	4.422	2479.900	15.00	3.06	.14	2480.04	.00	1.31	.00	2.500	.000	.00	0 .0
32.772	.0100					.0013	.04	4.42	.00	1.05	.013	.00	.00	PIPE
1032.772	2475.806	4.138	2479.944	15.00	3.06	.14	2480.09	.00	1.31	.00	2.500	.000	.00	0 .0
4.000	.0237					.0013	.01	4.14	.00	.83	.013	.00	.00	PIPE
1036.772	2475.901	4.086	2479.987	15.00	3.06	.14	2480.13	.00	1.31	.00	2.500	.000	.00	0 .0
18.551	.0375					.0013	.02	4.09	.00	.74	.013	.00	.00	PIPE
1055.323	2476.596	3.416	2480.012	15.00	3.06	.14	2480.16	.00	1.31	.00	2.500	.000	.00	0 .0

MAI N2. WSW

T1 DURANGO AND GRAND MONTECITO
T2 MAI N2
T3 KHA JOB# 092935040 BY: SS/MS
SO 1000.0002474.874 24 2479.0
R 1049.8202476.304 24 .013
JX 1053.8202476.381 18 18 .013 4.9 2474.874 .000 .000 0
R 1210.8722477.952 18 .013 .000 .000 0
R 1214.8722477.994 18 .013 .000 61.400 1
R 1233.9472478.186 18 .013 .000 .000 0
SH 1233.9472478.186 18
CD 6 4 0 .000 0.500 .000 .000 .000 .00
CD 8 4 0 .000 0.670 .000 .000 .000 .00
CD 12 4 0 .000 1.000 .000 .000 .000 .00
CD 18 4 0 .000 1.500 .000 .000 .000 .00
CD 24 4 0 .000 2.000 .000 .000 .000 .00
CD 30 4 0 .000 2.500 .000 .000 .000 .00
CD 36 4 0 .000 3.000 .000 .000 .000 .00
CD 42 4 0 .000 3.500 .000 .000 .000 .00
CD 48 4 0 .000 4.000 .000 .000 .000 .00
CD 54 4 0 .000 4.500 .000 .000 .000 .00
CD 60 4 0 .000 5.000 .000 .000 .000 .00
CD 66 4 0 .000 5.500 .000 .000 .000 .00
CD 72 4 0 .000 6.000 .000 .000 .000 .00
Q 4.600 .0

W S P G W - CIVILDESIGN Version 14.06
 Program Package Serial Number: 1911
 WATER SURFACE PROFILE LISTING
 DURANGO AND GRAND MONTECITO
 MAIN2
 KHA JOB# 092935040 BY: SS/MS

Date: 6-20-2024 Time: 2: 0: 0

0

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia. -FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1000.000	2474.874	4.126	2479.000	9.50	3.02	.14	2479.14	.00	1.10	.00	2.000	.000	.00	0 .0
49.820	.0287					.0018	.09	4.13	.00	.68	.013	.00	.00	PIPE
1049.820	2476.304	2.784	2479.088	9.50	3.02	.14	2479.23	.00	1.10	.00	2.000	.000	.00	0 .0
JUNCT STR	.0193					.0018	.01	2.78	.00		.013	.00	.00	PIPE
1053.820	2476.381	2.805	2479.186	4.60	2.60	.11	2479.29	.00	.82	.00	1.500	.000	.00	0 .0
157.052	.0100					.0019	.30	2.80	.00	.69	.013	.00	.00	PIPE
1210.872	2477.952	1.535	2479.487	4.60	2.60	.11	2479.59	.00	.82	.00	1.500	.000	.00	0 .0
4.000	.0105					.0019	.01	1.53	.00	.68	.013	.00	.00	PIPE
1214.872	2477.994	1.527	2479.521	4.60	2.60	.11	2479.63	.00	.82	.00	1.500	.000	.00	0 .0
3.332	.0101					.0019	.01	1.53	.00	.69	.013	.00	.00	PIPE
1218.204	2478.027	1.500	2479.527	4.60	2.60	.11	2479.63	.00	.82	.00	1.500	.000	.00	0 .0
15.377	.0101					.0018	.03	1.50	.00	.69	.013	.00	.00	PIPE
1233.581	2478.182	1.361	2479.543	4.60	2.73	.12	2479.66	.00	.82	.87	1.500	.000	.00	0 .0
.366	.0101					.0017	.00	1.36	.35	.69	.013	.00	.00	PIPE
1233.947	2478.186	1.358	2479.543	4.60	2.73	.12	2479.66	.00	.82	.88	1.500	.000	.00	0 .0

MAIN2_LAT1.WSW

T1 DURANGO AND GRAND MONTECITO
T2 MAIN2_LAT1 0
T3 KHA JOB# 092935040 BY: SS/MS
S0 1000.0002476.362 18 2479.2
R 1026.1752477.158 18 .013 .000 .000 0
SH 1026.1752477.158 18
CD 6 4 0 .000 0.500 .000 .000 .000 .00
CD 8 4 0 .000 0.670 .000 .000 .000 .00
CD 12 4 0 .000 1.000 .000 .000 .000 .00
CD 18 4 0 .000 1.500 .000 .000 .000 .00
CD 24 4 0 .000 2.000 .000 .000 .000 .00
CD 30 4 0 .000 2.500 .000 .000 .000 .00
CD 36 4 0 .000 3.000 .000 .000 .000 .00
CD 42 4 0 .000 3.500 .000 .000 .000 .00
CD 48 4 0 .000 4.000 .000 .000 .000 .00
CD 54 4 0 .000 4.500 .000 .000 .000 .00
CD 60 4 0 .000 5.000 .000 .000 .000 .00
CD 66 4 0 .000 5.500 .000 .000 .000 .00
CD 72 4 0 .000 6.000 .000 .000 .000 .00
Q 4.900 .0

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia. -FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1000.000	2476.362	2.838	2479.200	4.90	2.77	.12	2479.32	.00	.85	.00	1.500	.000	.00	0 .0
26.175	.0304					.0022	.06	2.84	.00	.53	.013	.00	.00	PIPE
1026.175	2477.158	2.099	2479.257	4.90	2.77	.12	2479.38	.00	.85	.00	1.500	.000	.00	0 .0