

TECHNICAL DRAINAGE STUDY RESPONSE TO COMMENTS

TROPICAL PKWY/CENTENNIAL PKWY ROADWAY IMPROVEMENTS

City of North Las Vegas, Clark County, Nevada

Job No.: MGL1101.000

Date: December 2011

Prepared By:

Slater Hanifan Group, Inc.
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Prepared For:

M Grape LLC
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Ray Frederickksen
NV Professional Engineer No. 17471

HYDROLOGIC CRITERIA AND DRAINAGE MANUAL
DRAINAGE STUDY INFORMATION FORM

Name of Development: Tropical Pkwy/Centennial Pkwy Roadway Improvements - Add 1 Date: December 12, 2011

Location of Development: a) Descriptive (Cross Streets) North/South: Centennial Parkway

East/West: Tropical Parkway

b) Section: 30 Township: 19 Range: 61

c) APN: 124-30-204-008

Name of Owner: M Grape LLC

Telephone No.: _____ Fax No.: _____ E-Mail Address: _____

Address: 2460 Professional Court, Suite 120

Contact Person-Name: Ray Fredericksen, P.E. Telephone No.: 702-284-5300

* E-Mail Address: rfredericksen@shg-inc.com Fax No.: 702-284-5399

Firm: Slater Hanifan Group

Address: 5740 S. Arville Street #216, Las Vegas, NV 89118

Type of Land Development/Land Disturbance Process:

☐	Rezoning	☐	Subdivision Map	☐	Clearing and Grading Only
☐	Parcel Map	☐	Planned Unit Development	☒	Other (Please specify below)
☐	Large Parcel Map	☐	Building Permit		Roadway Improvements

1. Total Owned Land Area: At Site: 2.1 Ac Being Developed/Disturbed: 2.1 AC

2. Is a portion or all of the subject property located in a designated FEMA Flood Hazard Area? ☐ Yes** ☒ No

3. Is the property bordered or crossed by an existing or proposed Clark County Regional Flood Control District Master Planned Facility? ☐ Yes** ☒ No

4. Proposed type of development (Residential, Commercial, Etc.): Roadway Improvements

5. Approximate upstream land area which drains to the subject site: 10 acres

6. Has the site drainage been evaluated in the past? ☒ YES ☐ NO If yes, please identify documentation: Offsites - Twilight North

7. If known, please briefly identify the proposed discharge point(s) of runoff from the site: East in Tropical Parkway to existing storm water improvements

8. Briefly describe your proposed schedule for the subject project: As soon as possible



Engineer's Seal

Submit this form as part of the required drainage study to the local entity which has jurisdiction over the subject property. This form may provide sufficient information to serve as the Conceptual Drainage Study.

*New Required Field

**Review and concurrence of the Clark County Regional Flood Control District is required.

Local Entity File No.	Revision	Date

REFERENCE:

STANDARD FORM 1

MGL1101.000

December 12, 2011

City of North Las Vegas
Land Development & Flood Control Division
2250 North Las Vegas Blvd, Suite 220
North Las Vegas, NV 89030

Re: **Technical Drainage Study for Tropical Pkwy./Centennial Pkwy. Roadway
Improvements
CNLV No. 43988**

Land Development & Flood Control Division:

The purpose of this letter is to address comments contained in the November 30, 2011 review memorandum prepared for the above referenced project. The comments are addressed as follows:

1. **Comment:** *Concurrence must be obtained by the City of Las Vegas (CLV) due to the proposed improvement's proximity to the CLV jurisdiction. Please submit a copy of this study and all addenda to CLV upon acceptance from CNLV.*

Response: Noted. A copy of the TDS and all addenda will be submitted to the CLV upon approval by CNLV.

2. **Comment:** *The Technical Drainage Study (TDS) is only for the proposed street improvements adjacent to the site, a separate drainage study and planning commission conditions must be submitted, in the future, for the undeveloped area within the same parcel.*

Response: Noted. An on-site Technical Drainage Study will be submitted for all on-site improvements for the adjacent site.

3. **Comment:** *A quick review of the general topography in the area shows that the area surrounding the project site drains southeasterly direction. It appears that Decatur Boulevard, adjacent to the site, may intercept some offsite flows from upstream of the project site.*

Section 1.5 of TDS states that "Improvements west of Decatur have effectively cut off flows and routed them into the existing storm drain in Decatur." Please provide approved reference materials to illustrate that all flows are being contained within the existing storm drain in Decatur Boulevard. Please note that all 10-year and 100-year street capacity calculations must be revised to reflect any flow changes. Also, 12' dry lane criterion must also be met for the future condition.

Response: Based on reference studies provided by the City of Las Vegas for Winco Las Vegas (Thienes Engineering, 2011) which was an Update to the TDS for Decatur/215 (Southwest Engineering, 2008) there is an existing surface flow (section G in reference files) south in Decatur Blvd of 9 cfs during the 10-year storm event and 155 cfs during the 100-year storm event at the intersection of Decatur and Tropical, this flow proceeds remains in the Decatur right-of-way and heads south. At the Rice and Decatur intersection there is a surface flow of 0 cfs and 138 cfs during the 100-year storm event (Section E in the reference files). The existing 54" storm drain conveys 86 cfs. The street flow calculations show that the 10-year dry lane criteria is met. The 100-year storm event will produce a depth of flow 0.98 ft deep. The velocities however are non-erosive. Any developments proposed to front on Decatur Blvd will provide flood protection to prevent flood water from inundating the property. Any future on-site developments will address this issue within their technical study. Copies of the reference material documenting these surface flows are included in Appendix A. All relevant Figures and calculations have been revised and included in the appendix. Based on review of the reference material it states that the storm water flow in Decatur Blvd will continue south and will not be picked up by any future storm drain. The downstream properties appear to have been designed to accommodate this storm water flow.

4. **Comment:** *Please note that the CNLV requires that all drop inlet sizing be performed with the HEC-22 software which can be acquired from the Federal Highway Administration's website.*

Response: Please refer to Appendix B for all revised drop inlet sizing calculations using the HEC-22 software. The drop inlet on the west side of Centennial is now sized at 15-ft Modified Type C. The drop inlet along the east side of Centennial Pkwy is designed as a 7.5-ft Modified Type C.

5. **Comment:** *Please explain and demonstrate how the $Q_{100}=118$ cfs and $Q_{10}=38$ cfs (hydraulic Section D-D of the Existing Condition Street Flows) were obtained since the flows for the Interim and Future conditions at hydraulic section D-D are $Q_{100}=3$ cfs and $Q_{10}=2$ cfs.*

Response: For the Existing Condition street flow calculations the CNLV North Neighborhood Study (CNLVNNS) was referenced. The Existing Condition, Figure E-9, in the CNLVNNS shows a surface flow of $Q_{10}=36$ cfs and $Q_{100}=115$ cfs heading east. This flow value was used for the existing condition. However, the current design of Rice Avenue with a highpoint just east of Decatur Blvd does not allow storm water to head east on Rice Ave. In addition, this flow was referenced from the City of Las Vegas NNS study and is no longer a valid quantity of water as discussed in the response to comment 3.

6. **Comment:** *Please explain/show how the Q_{100}/Q_{10} in This Study and the Twilight Study were obtained in Tables 3 and 5 of TDS. The flow values in Tables 3 and 5 do not match with the flow values in the drainage basin maps and the reference materials for the Twilight Study.*

Response: In compiling the first submittal of this TDS the NNS value at the intersection of Decatur Blvd. and Tropical Pkwy was used incorrectly in relation to

the previous studies in the area. The following excerpt is from the TDS for Twilight at Riverwalk, by Slater Hanifan Group. This excerpt clarifies why the future condition value was used at the intersection from the NNS. The exhibits and street flow calculations have been revised to match.

Reference Material (from Twilight at Riverwalk):

“Response: Table 2 summarizes the existing condition peak 100-year flow rates to perimeter streets established by the CNLV Study. Note that both streets show no flow contained in storm drain. With completion of this project, the local facility in Tropical, south of the project, will be constructed to convey the 10-year storm flow and 100-year flow at the intersection of Valley & Tropical. Also, local facilities in Decatur and Tropical, west of Decatur, are complete and connect to the regional facility in Ann. The 10-year flow at Decatur is collected by this existing offsite storm drain. With these facilities, it is appropriate to utilize the CNLV Future Drainage conditions as existing condition in determining offsite flow for this project; therefore no street flow computations were performed based on the existing condition CNLV flow values. See Table 3 below regarding future drainage condition flow in the perimeter streets. Note that values in parenthesis represent flow conveyed in storm drain.

Table 2: Summary of Existing Condition Flows Established By CNLV Study		
Location	Q ₁₀₀ (cfs)	Q ₁₀ (cfs)
Tropical / Decatur	267 (0)	62 (0)
Tropical / Centennial	282 (0)	70 (0)

Table 3: Summary of Future Condition Flows Established By CNLV Study		
Location	Q ₁₀₀ (cfs)	Q ₁₀ (cfs)
Tropical / Decatur	223 (0)	0 (0)
Tropical / Centennial	229 (0)	19 (0)

(End insertion of reference material)

The HEC-1 analysis from the approved TDS for Twilight at Riverwalk was referenced and the hydrograph for the NNS quantity was added to the HEC-1 for this study. By incorporating this flow and hydrograph the flows became equal at the “intersection” of Centennial Parkway and Tropical Parkway as summarized in the revised Table 3 and 5 below:

Table 3: Interim Condition Comparison – This Study vs. Twilight Study				
Location	Concentration Point ID	Q _{100/10} (cfs)	Concentration Point ID (Twilight Study)	Q _{100/10} (cfs)
Intersection of Centennial Pkwy & Tropical Pkwy	CP.I5	233/21	CP.D6	241/16

Table 5: Future Condition Comparison -- This Study vs. Twilight Study				
Location	Concentration Point ID	Q _{100/10} (cfs)	Concentration Point ID (Twilight Study)	Q _{100/10} (cfs)
Intersection of Centennial Pkwy & Tropical Pkwy	CP.D5	235/30	CP.D6	234/31

As you can see from the tables listed above the reference study and the proposed study are not the same incorporating the HEC-1 and hydrograph from the previously approved studies. Copies of the relevant reference material have been included in the Appendix.

7. **Comment:** *Please explain and demonstrate how the Q_{approaching}=26 cfs in Table 8 of the TDS was obtained. The Interim and Future Condition Basin Maps show that Q₁₀₀=21 cfs instead of Q₁₀₀=26 cfs at Section E-E.*

Also, it appears that a portion of the Q₁₀₀=302 cfs and Q₁₀=78 cfs from Tropical Parkway will turn north adding to the flows in Centennial Parkway at the proposed drop inlets. Please evaluate and perform the necessary flow split calculations and revise all street and drop inlet capacity calculations to reflect the revision as necessary.

Response: Please refer to the grading plans enclosed with this submittal. The grading concept for this intersection has been revised. The grading will no longer allow for storm water from Tropical Parkway to head north in Centennial Parkway. The drop inlets will remain to capture the 21 cfs conveyed south in Centennial Parkway. The west DI (15-ft) will capture the 17 cfs from the west half of the street while the 7.5-ft modified Type C will capture the 3/4 cfs from the east half of Centennial. Please see the drop inlet sizing calculations in Appendix F as well as the revised grading plans. No additional calculations are required.

8. **Comment:** *Please discuss and show how soil type boundaries were determined as delineated on the drainage basin maps? Provide any pertinent soil type chart for the project area.*

Response: Please refer to Appendix D for a Soils Map of the project vicinity. The majority of the soils associated with this project are soils type 305 which has is a hydrologic soils group 'C' the minor soils type used in compiling this report is 301 which is in hydrologic soils group 'D'. Also, note that both the onsite future project and the roadway basins are comprised of pavement and used a CN value of 98.

9. **Comment:** *It is unclear where is drainage basin DEC_5 as shown in the Soil and Curve Number Computation table of the TDS.*

Response: This basin ID has been revised to call out basin DEC_3. The basin name was changed during composition of the analysis and not changed on this spreadsheet. Please refer to the revised Soil and Curve Number Computation spreadsheet in Appendix E.

- 10. Comment:** Please revise the Flowmaster calculations for the interim and future conditions of Centennial Parkway and Tropical Parkway to show the proposed concrete median islands.

Response: Noted. Please refer to Appendix F for the revised worksheets. All street flow calculations have been revised to the current values. Street sections have been revised to include the center median.

Perimeter Street Flow Summary Interim Condition							
Section	Slope (%)	Q ₁₀₀ (cfs)	Depth (ft)	Velocity (fps)	VxD	Q ₁₀ (cfs)	Dry Lane Width (ft)
SECTION A Tropical Pkwy (100' ROW) (Q = CP.I2)	0.70	224.0	1.12	4.76	5.3	3.0	36.50
SECTION B Tropical Pkwy (100' ROW) (Q = CP.I3)	0.60	230.0	1.03	4.25	4.4	12.0	21.50
SECTION C Decatur Blvd (100' ROW) (Q = North of C-Store)	0.40	144.0	0.98	3.14	3.1	3.0	24.0
SECTION D Rice Ave (60' ROW) (Q = RIC1)	0.61	3.0	0.32	1.62	0.5	2.0	n/a
SECTION E (West 1/2 St) Centennial Pkwy (90' ROW) (Q = CP.D7)	0.70	17.0	0.52	2.57	1.3	8.0	36'
SECTION E (East 1/2 St) Centennial Pkwy (90' ROW) (Q = CP.D7)	0.90	4.0	0.31	1.79	0.6	2.0	36'

Perimeter Street Flow Summary Future Condition							
Section	Slope (%)	Q ₁₀₀ (cfs)	Depth (ft)	Velocity (fps)	VxD	Q ₁₀ (cfs)	Dry Lane Width (ft)
SECTION A Tropical Pkwy (100' ROW) (Q = CP.D2)	0.70	224.0	1.13	4.81	5.4	3.0	36.50
SECTION B Tropical Pkwy (100' ROW) (Q = CP.D3)	0.60	232.0	1.03	4.26	4.4	21.0	17.50
SECTION C Decatur Blvd (100' ROW) (Q = North of C-Store)	0.40	144.0	0.98	3.14	3.1	3.0	24.0

SECTION D Rice Ave (60' ROW) (Q = RIC1)	0.61	3.0	0.32	1.62	0.5	2.0	n/a
SECTION E (West 1/2 St) Centennial Pkwy (90' ROW) (Q = CP.D7)	0.70	17.0	0.52	2.57	1.3	8.0	36'
SECTION E (East 1/2 St) Centennial Pkwy (90' ROW) (Q = CP.D7)	0.90	4.0	0.31	1.79	0.6	2.0	36'

Based on the above table you can see that 10-year dry lane criteria is met under both scenarios. The depth of flow in many instances is above the top of curb however the velocities are non-erosive. The on-site developer will be required to flood protect his development per requirements set forth in the HC&DDM manual.

11. Comment: *Below are comments pertaining to the Improvement Plans:*

- a. *If the landscapes areas along the meandering sidewalks are to be installed with the street improvements, the Engineer must show grades and flow lines within all landscape areas. Flows from the landscape areas will not be allowed to sheet flow over the adjacent sidewalks. Drainage swales should be graded to direct flows to discharge into the sidewalk underdrains.*

Response: Please refer to the grading plans. Swales within the landscape area have been added as well as sidewalk under drains where necessary.

- b. *Since the 100-year depth of flows will overtop the curbs (i.e. Tropical Parkway), the proposed landscape berms used to protect future developed properties from flows in the adjacent streets must meet the criterium of being twice the depth of flow above the adjacent flowline up to 18-inches above adjacent water surface.*

Also, for 100-year street flow with depths greater than 0.6' and velocities higher than 5 fps, erosion resistant landscaping or pony walls must be provided

Response: A berm has been added along Decatur Blvd and Tropical Parkway to ensure that storm water flow remains in the adjacent right-of-way. The berms are designed to be a minimum of twice the depth of flow from the adjacent flow line. The depth of flow is above the curb however the velocities are below 5 fps. Therefore, no erosion protection was provided with this plan set. Please refer to the enclosed grading plans and detail sheet for the berm design.

- c. *Please note that any proposed storm drains within the public right of way must be reinforced concrete pipe with diameter of 18" minimum. Please revise the portion of the proposed storm drain pipe on the east half of Centennial Parkway to reflect the above described requirements. Also, CNLV highly discourages the installation of storm drain under the curb and gutter. Please redesign the proposed storm drain lateral on the east side of Centennial Parkway to locate away from the curb and gutter.*

Response: Noted. The storm drain in Centennial Pkwy has been redesigned to remove the storm drain from under the curb and gutter. Please refer to the plan and profile sheets.

- d. *Please provide the Benchmark information.*

Response: Noted. The Benchmark has been added to all sheets.

- e. *The size of the drop inlets on Sheet P-6 are different from the sizes shown in the drop-inlet calculations in the TDS. Please revise the drawing to reflect the correct size of the drop inlets.*

Response: Noted. Drop inlet sizes have been corrected. Please refer to profile sheets for Centennial Pkwy.

- f. *Please provide two driveways per the conditions of the approved Site Plan Review (SPR 11-11). The first driveway should be located on Rice Ave. at approximate station 13+00 and second driveway should be on Tropical Pkwy. At approximate station 108+50.*

Response: Noted. All driveways have been added to the grading plans.

- g. *Please note that tack-on curb is not allowed in the Public ROW. Please revise Sheets P-3 and P-4 to show "A" type curb per CCAUSD #219 for Tropical Pkwy.*

Response: Noted. "A" curb callout has been revised to the above mentioned design.

- h. *The proposed meandering sidewalk on Tropical Pkwy. At approximate station 105+00, does not tie into the existing sidewalk at that location. Please revise drawing accordingly.*

Response: Noted. Meandering sidewalk has been revised to tie into existing C-store design.

- i. *Since Rice Ave. is a new street (undeveloped on both sides), please submit a design for a new street without saw cutting and matching the existing asphalt pavement. All existing asphalt pavements on Rice Ave. are temporary and need to be removed and a half street improvements with 16' overpaved will be required as part of this development. In addition, a median island and a concrete valley gutter must be constructed within Rice Ave. at Decatur Blvd. intersection.*

Response: Noted. The revised street section shows the south half street to be removed and replaced with a full pavement section. The median conditioned in SPR-11-11 has been added to the plans. Please refer to the grading plans.

- j. Please remove approval signature line for CNLV Traffic Engineer from all Plan and Profile sheets.

Response: Noted. The Traffic Engineer's signature block has been removed from all profile sheets.

12. **Comment:** Additional comments may be generated on the second review.

Response: Noted.

13. **Comment:** A copy of this letter must accompany the subsequent submittal to the City of North Las Vegas.

Response: Noted. Please refer to Appendix G.

If you have any further comments, or questions, please feel free to contact me at (702) 284-5300.

Respectfully submitted,

SLATER HANIFAN GROUP



Ray Fredericksen, P.E.
Project Manager

APPENDIX

Appendix A – Response to Comment No. 3:

- a. Revised FlowMaster calcs for Decatur Blvd
- b. Reference material from Decatur/215

Appendix B – Response to Comment No.4:

- a. Drop Inlet Sizing calculations

Appendix C – Response to Comment No. 6

- a. 10-Year Interim Condition HEC-1
- b. 100-Year Interim Condition HEC-1
- c. 10-Year Developed Condition HEC-1
- d. 100-Year Developed Condition HEC-1
- e. 10-Year Existing Condition HEC-1
- f. 100-Year Existing Condition HEC-1
- g. Reference Material from Twilight at Riverwalk

Appendix D – Response to Comment No.8:

- a. Soils Map

Appendix E – Response to Comment No. 9

- a. Revised Soil and CN Table

Appendix F – Response to Comment No.10

- a. Revised Flowmaster calcs

Appendix G – Response to Comment No.14

- a. City of North Las Vegas comment letter

Appendix H – Exhibits

- a. Existing Condition Exhibit E
- b. Interim Condition Exhibit F
- c. Future Condition Exhibit G

APPENDIX A

Response to Comment 3

Reference Material from Adjacent Study
Revised Flowmaster Calcs for Decatur Blvd.

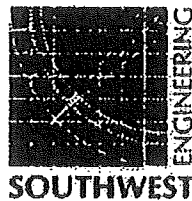
Rec'd 2/27/2008
DS 4261
A-25
Supp. Info
W/C.

**SUPPLEMENT TO
ADDENDUM #2 TO THE
TECHNICAL DRAINAGE STUDY
DECATUR / 215
SWE JOB # 070619**

February 27, 2008

**Prepared for:
AM PM Enterprises
655 Madison Avenue, 25th Floor
New York, New York 10021**

Prepared by:



**SOUTHWEST ENGINEERING
3610 North Rancho Drive
Las Vegas, Nevada 89130
Ph: (702) 648-9700 Fax (702) 648-9700**

February 27, 2008

Oh Sang Kwon, P.E.
Flood Control Project Engineer
Department of Public Works
Land Development Services
City of Las Vegas, Nevada 89101

**RE: Supplement to Addendum #2 to the Drainage Study for Decatur / 215-
located at the northwest corner of Decatur Blvd. and Tropical Pkwy.**

Dear Mr. Kwon:

This is in response to issues discussed in a February 20, 2008 meeting with Southwest Engineering and the City of Las Vegas (Robert Welch and Albert Sung). The City of Las Vegas is concerned about potential impacts to the existing flows downstream of the intersection of Tropical Parkway and Decatur Boulevard caused by the development of the project. It is important to add that the existing beltway, and existing improvements in Decatur Boulevard and Tropical Boulevard that were built with the Lodge III project have essentially established the drainage patterns at the intersection. The Lodge III site is located at the southwest corner of the intersection of Tropical Parkway and Decatur Boulevard.

The approved Lodge III Drainage Study (refer to attached excerpts) had established that the design flow for the 42-inch storm drain in Tropical Parkway is 52 cfs and the future design flow for the 54-inch storm drain in Decatur Boulevard is 149 cfs. The additional 97 cfs was assumed to enter the storm drain in Decatur Boulevard, north of Tropical Parkway, in the future. The Lodge III study also established that a total of 334 cfs would drain east in Tropical Parkway and a total of 444 cfs would drain south in Decatur Boulevard adjacent to the Lodge III site. Hence, the existing surface flow in Tropical Parkway is 282 cfs and the existing surface flow in Decatur Boulevard is 392 cfs at this location.

The Lodge III study essentially established the hydrologic design criteria in this area. The City of North Las Vegas had concurred with the conclusions of the Lodge III study. It is also important to note that the flows established in the Lodge III study somewhat deviate from the 1999 City of Las Vegas Northwest Neighborhood Study Update (see attached excerpt).

The following flows were established in the subject Decatur/215 drainage study:

Flows draining east in Tropical Parkway (west of Decatur):

Existing $Q_{10}=59$ cfs total (52 cfs in storm drain and 7 cfs surface flow)

Existing $Q_{100}=350$ cfs total (52 cfs in storm drain and 298 cfs surface flow)

Developed $Q_{10}=58$ cfs total (52 cfs in storm drain and 6 cfs surface flow)

Developed $Q_{100}=346$ cfs total (52 cfs in storm drain and 294 cfs surface flow)

Flows draining south in Decatur Boulevard (north of Tropical):

Existing $Q_{10}=72$ cfs total (72 cfs surface flow)

Existing $Q_{100}=197$ cfs total (197 cfs surface flow)

Developed $Q_{10}=95$ cfs total (86 cfs in storm drain and 9 cfs surface flow)

Developed $Q_{100}=241$ cfs total (86 cfs in storm drain and 155 cfs surface flow)

The flows draining to the intersection are not significantly impacted by the development of the Decatur/215 project. The existing and developed flows in Tropical Parkway (west of Decatur) are essentially the same. The flows in Decatur Boulevard (north of Tropical Parkway) have increased by 44 cfs in the 100-year storm, but the storm drain reduces the surface flow to 155 cfs. Hence, the development of the project will not cause significant negative impact the drainage patterns at the intersection of Tropical Parkway and Decatur Boulevard. The City of Las Vegas had requested that a flow split calculation be performed for this intersection. The previous drainage study did not provide a flow split calculation, but only provided calculations showing the maximum flow in Decatur if no split occurred:

The Pima County Method was utilized to estimate a flow split at the intersection for the developed condition. Since most of the flow in Decatur Boulevard (north of the intersection) is contained in the west side of the street-it was assumed that this flow would essentially continue south in Decatur. The flow draining east to the intersection in Tropical Parkway was assumed to split based on the Pima County Method. It was also assumed that no surface flow split would occur at the intersection for the 10-year storm. The flow split estimate (see attached calculations) yields the following flows downstream of the intersection:

Flows draining east in Tropical Parkway (east of Decatur):

Developed $Q_{10}=0$ cfs total (0 cfs surface flow)

Developed $Q_{100}=193$ cfs total (193 cfs surface flow)

Flows draining south in Decatur Boulevard (south of Tropical):

Developed $Q_{10}=153$ cfs total (138 cfs in storm drain and 15 cfs surface flow)

Developed $Q_{100}=394$ cfs total (138 cfs in storm drain and 256 cfs surface flow)

The resulting flow split estimate shows that the flows in Decatur, south of Tropical Parkway, are about the same as the previous surface flow of 392 cfs. Also, the storm drain design flow at this location (149 cfs) is not exceeded. For these reasons it is concluded that the development of the Decatur/215 project is consistent with established flows and drainage patterns in this vicinity.

If you have any questions or require additional information, please call me at Southwest Engineering at (702) 648-9700.

Sincerely,
SOUTHWEST ENGINEERING

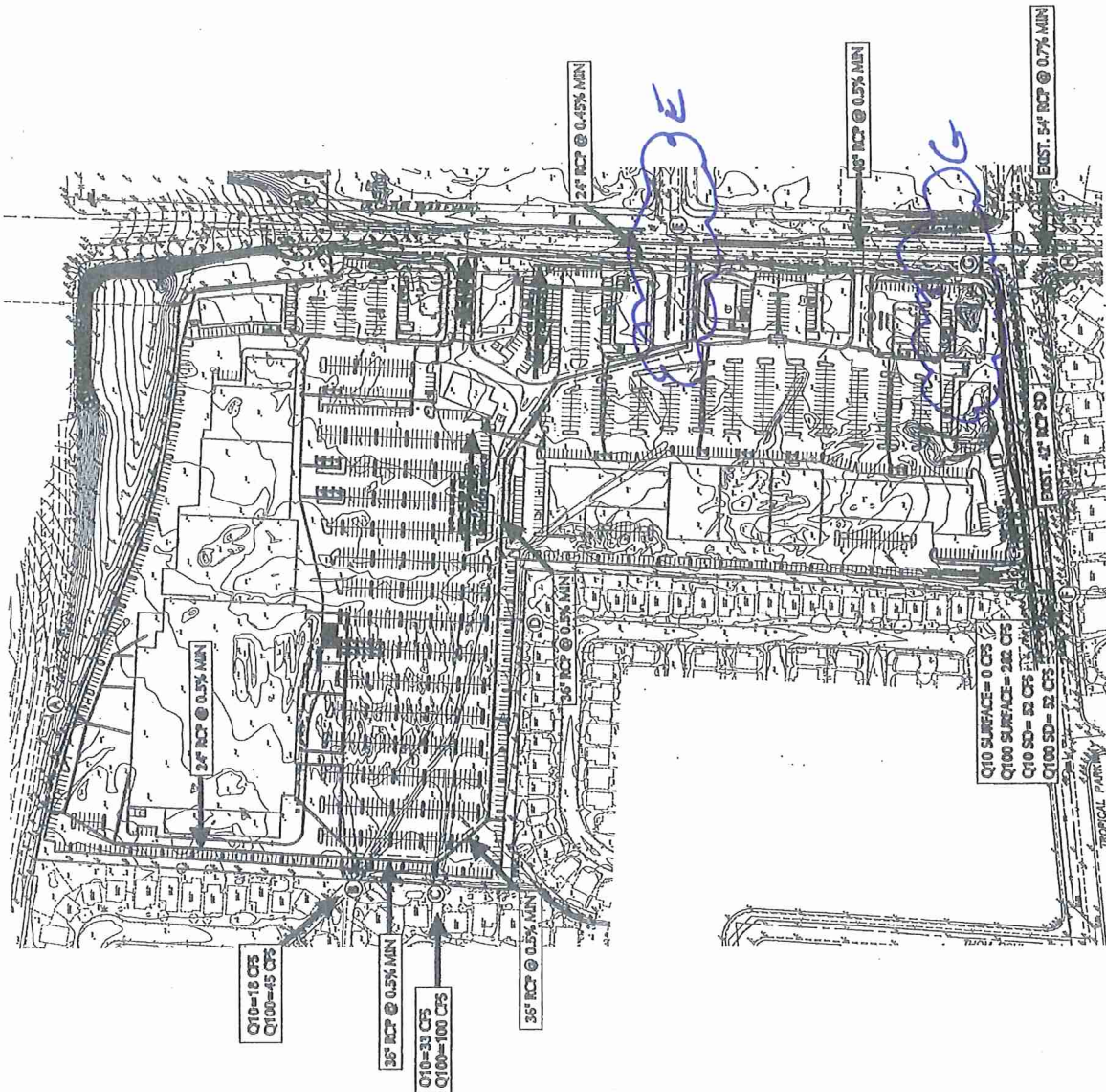

Ed Rajnovich
Project Manager

STORM DRAIN SUMMARY				
PT	Q10 IN SD	Q100 IN SD	Q10 INTO DI	Q100 INTO DI
A	4 CFS	9 CFS	4	9
B	22 CFS	34 CFS	18	25
C	55 CFS	55 CFS	33	21
D	55 CFS	55 CFS	0	0
E	86 CFS	86 CFS	31	31
F	52 CFS	52 CFS	0	0
G	86 CFS	86 CFS	0	0
H	138 CFS	138 CFS	0	0

SURFACE FLOW SUMMARY		
PT	Q10	Q100
A	0 CFS	0 CFS
B	0 CFS	20 CFS
C	0 CFS	99 CFS
D	8 CFS	114 CFS
E	0 CFS	138 CFS
F	0 CFS	282 CFS
G	9 CFS	155 CFS
H	15 CFS	439 CFS

DECATUR/TROPICAL
070619.00

FIGURE 8
STORM DRAIN
SYSTEM (REVISED 01/08)
1"=100'



This plan is a part of drainage study which was received on 12/20/00 and dated on 12/20/00. It is located at 1000 North 1000 East, Las Vegas, Nevada 89130. Telephone: (702) 648-0700 Fax: (702) 648-4143

SOUTHWEST
LAND PLANNING • MAPPING • DEVELOPMENT

Decatur Blvd Q10 EX Sec C

Worksheet for Irregular Channel

Project Description	
Worksheet	Decatur Boulevard Q10 EX Sec C
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.60 %
Discharge	3.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.013
Water Surface Elevation	79.17 ft
Elevation Range	78.82 to 80.11
Flow Area	1.8 ft ²
Wetted Perimeter	20.94 ft
Top Width	20.47 ft
Actual Depth	0.35 ft
Critical Elevation	79.17 ft
Critical Slope	0.59 %
Velocity	1.68 ft/s
Velocity Head	0.04 ft
Specific Energy	79.22 ft
Froude Number	1.00
Flow Type	Supercritical

Calculation Messages:

Water elevation exceeds lowest end station by 0.1015464 ft.
Flow is divided.

Dry Lane

$$\frac{79.41 - 79.17}{0.02} = 22 \text{ ft}$$

OK

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+08.50	0.033
0+08.50	0+10.00	0.013
0+10.00	0+46.00	0.016
0+46.00	0+50.00	0.013
0+50.00	0+94.00	0.016

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	79.36
0+08.00	79.32
0+08.50	79.32
0+08.50	78.82
0+10.00	78.99

Decatur Blvd Q10 EX Sec C
Worksheet for Irregular Channel

Natural Channel Points	
Station (ft)	Elevation (ft)
0+46.00	79.61
0+46.00	80.11
0+50.00	80.10
0+50.00	79.60
0+94.00	79.07

Decatur Blvd Q10 Ex Sec C

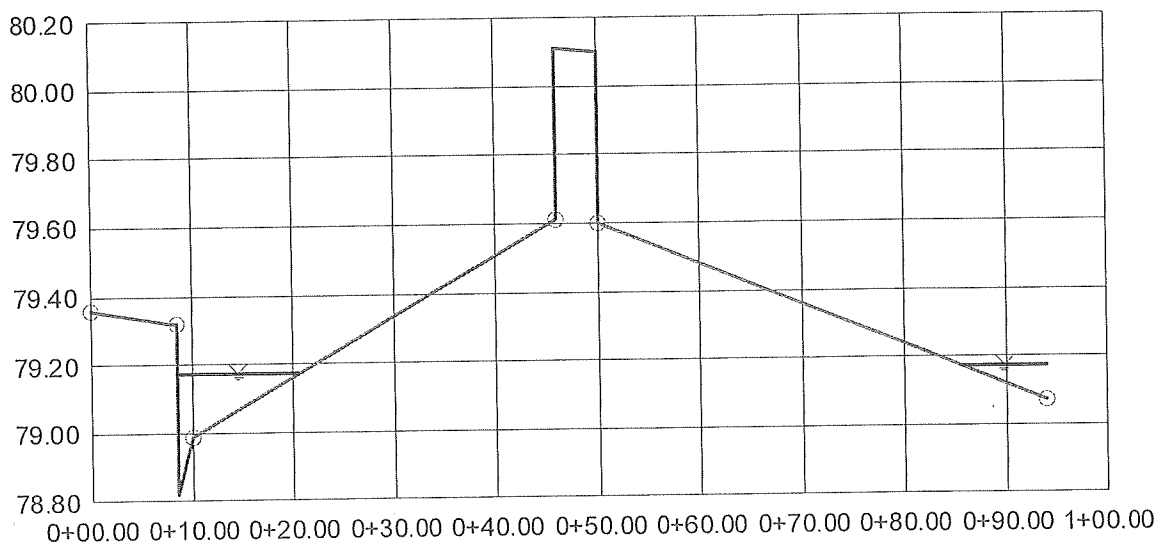
Cross Section for Irregular Channel

Project Description

Worksheet	Decatur Boulevard Q10 EX Sec C
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data

Mannings Coefficient	0.013
Channel Slope	0.60 %
Water Surface Elevation	79.17 ft
Elevation Range	78.82 to 80.11
Discharge	3.00 cfs



V:33.333333
H:1
NTS

Decatur Blvd Q10 EX Sec C

Worksheet for Irregular Channel

Project Description	
Worksheet	Decatur Boulevard Q100 EX Sec C
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.60 %
Discharge	144.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.016
Water Surface Elevation	79.73 ft
Elevation Range	78.82 to 80.11
Flow Area	37.5 ft ²
Wetted Perimeter	91.80 ft
Top Width	90.00 ft
Actual Depth	0.91 ft
Critical Elevation	79.74 ft
Critical Slope	0.54 %
Velocity	3.84 ft/s
Velocity Head	0.23 ft
Specific Energy	79.96 ft
Froude Number	1.05
Flow Type	Supercritical

Calculation Messages:

Water elevation exceeds lowest end station by 0.66057292 ft.
Flow is divided.

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+08.50	0.033
0+08.50	0+10.00	0.013
0+10.00	0+46.00	0.016
0+46.00	0+50.00	0.013
0+50.00	0+94.00	0.016

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	79.36
0+08.00	79.32
0+08.50	79.32
0+08.50	78.82
0+10.00	78.99

$$V \times D$$

$$3.84 \times 0.91 = 3.49$$

Decatur Blvd Q10 EX Sec C
Worksheet for Irregular Channel

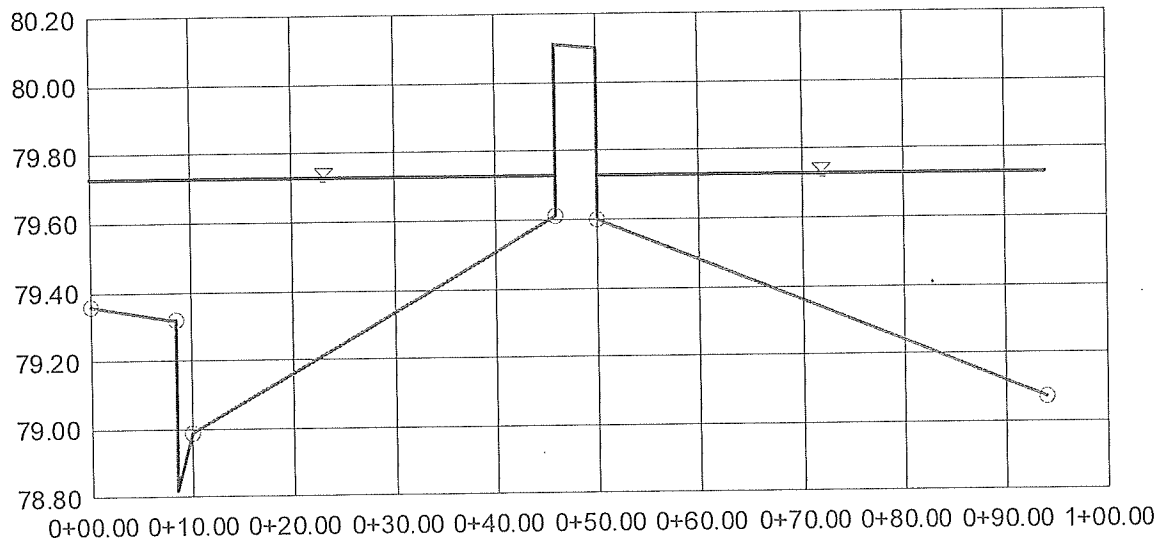
Natural Channel Points	
Station (ft)	Elevation (ft)
0+46.00	79.61
0+46.00	80.11
0+50.00	80.10
0+50.00	79.60
0+94.00	79.07

Decatur Blvd Q10 Ex Sec C

Cross Section for Irregular Channel

Project Description	
Worksheet	Decatur Boulevard Q100 EX Sec C
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.016
Channel Slope	0.60 %
Water Surface Elevation	79.73 ft
Elevation Range	78.82 to 80.11
Discharge	144.00 cfs



V:33.3333333
H:1
NTS

Decatur Blvd Q10 INT Sec C

Worksheet for Irregular Channel

Project Description	
Worksheet	Decatur Boulevard Q10 INT Sec C
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.40 %
Discharge	3.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.013
Water Surface Elevation	79.13 ft
Elevation Range	78.74 to 80.11
Flow Area	2.0 ft ²
Wetted Perimeter	21.77 ft
Top Width	21.35 ft
Actual Depth	0.39 ft
Critical Elevation	78.74 ft
Critical Slope	0.00 %
Velocity	1.47 ft/s
Velocity Head	0.03 ft
Specific Energy	79.16 ft
Froude Number	0.84
Flow Type	Subcritical

Calculation Messages:
Flow is divided.

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+08.50	0.033
0+08.50	0+10.00	0.013
0+10.00	0+46.00	0.016
0+46.00	0+50.00	0.013
0+50.00	1+00.00	0.016
1+00.00	1+02.00	0.013
1+02.00	1+12.00	0.033

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	79.36
0+08.00	79.32
0+08.50	79.32
0+10.00	78.99

Dry Lane

79.61 - 79.13

0.02

= 24-st

ok

2

Decatur Blvd Q10 INT Sec C
Worksheet for Irregular Channel

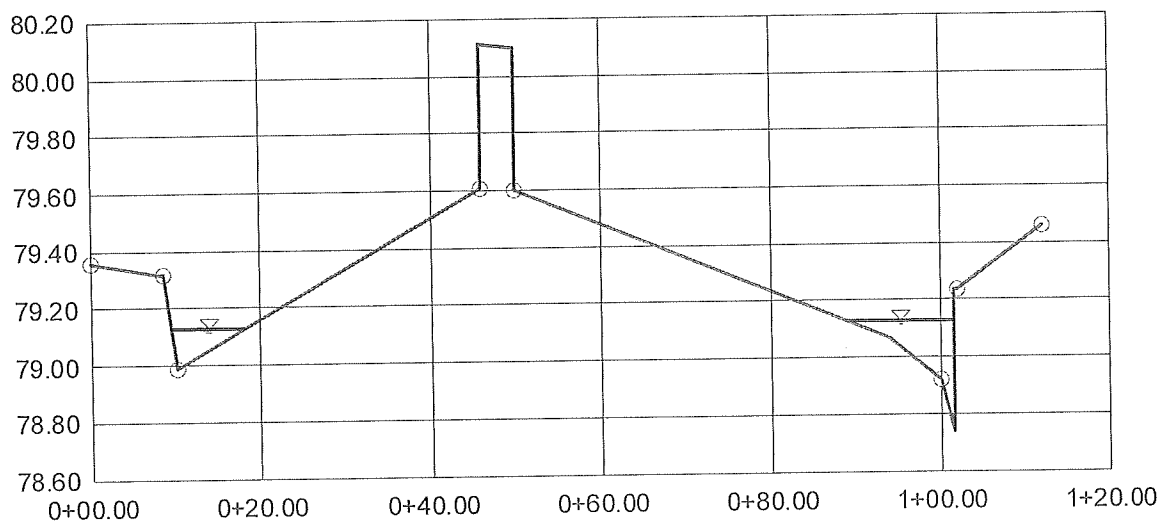
Natural Channel Points	
Station (ft)	Elevation (ft)
0+46.00	79.61
0+46.00	80.11
0+50.00	80.10
0+50.00	79.60
0+94.00	79.07
1+00.00	78.92
1+01.50	78.74
1+01.50	79.24
1+02.00	79.24
1+12.00	79.46

Decatur Blvd Q10 Int Sec C

Cross Section for Irregular Channel

Project Description	
Worksheet	Decatur Boulevard Q10 INT Sec C
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.013
Channel Slope	0.40 %
Water Surface Elevation	79.13 ft
Elevation Range	78.74 to 80.11
Discharge	3.00 cfs



V:33.3333333
H:1
NTS

Decatur Blvd Q100 INTSec C

Worksheet for Irregular Channel

Project Description	
Worksheet	Decatur Boulevard Q100 INT Sec C
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.40 %
Discharge	144.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.017
Water Surface Elevation	79.72 ft
Elevation Range	78.74 to 80.11
Flow Area	45.9 ft ²
Wetted Perimeter	109.41 ft
Top Width	108.00 ft
Actual Depth	0.98 ft
Critical Elevation	78.74 ft
Critical Slope	0.00 %
Velocity	3.14 ft/s
Velocity Head	0.15 ft
Specific Energy	79.87 ft
Froude Number	0.85
Flow Type	Subcritical

Calculation Messages:

Water elevation exceeds lowest end station by 0.36115375 ft.
Flow is divided.

$$\frac{V \times D}{2}$$

$$3.14 \times 0.98 = 3.1$$

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+08.00	0.033
0+08.00	0+10.00	0.013
0+10.00	0+46.00	0.016
0+46.00	0+50.00	0.013
0+50.00	1+00.00	0.016
1+00.00	1+02.00	0.013
1+02.00	1+12.00	0.033

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	79.36
0+08.00	79.32
0+08.50	79.32

Decatur Blvd Q100 INTSec C
Worksheet for Irregular Channel

Natural Channel Points	
Station (ft)	Elevation (ft)
0+10.00	78.99
0+46.00	79.61
0+46.00	80.11
0+50.00	80.10
0+50.00	79.60
0+94.00	79.07
1+00.00	78.92
1+01.50	78.74
1+01.50	79.24
1+02.00	79.24
1+12.00	79.46

Decatur Blvd Q100 Int Sec C

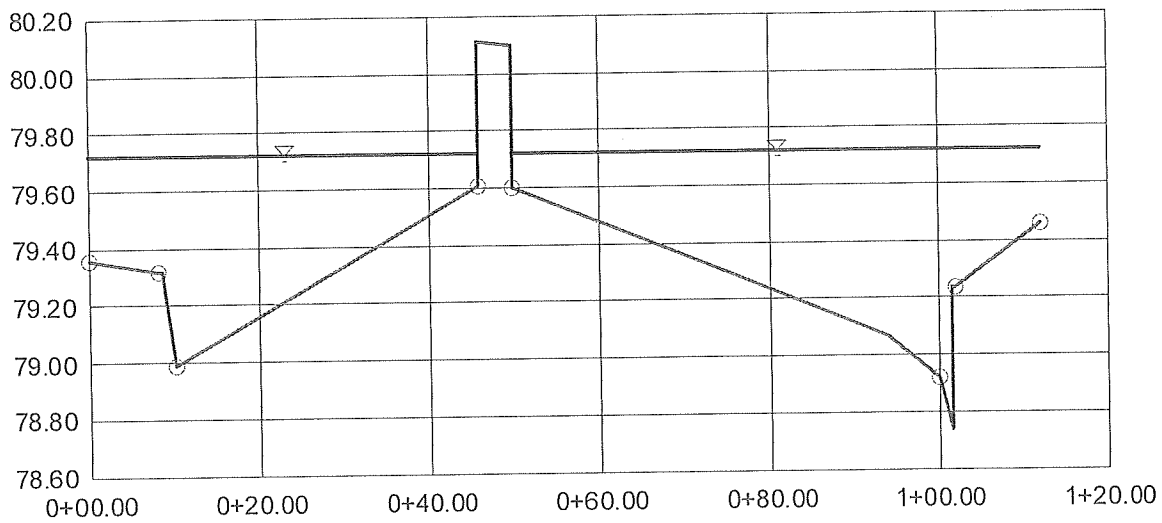
Cross Section for Irregular Channel

Project Description

Worksheet	Decatur Boulevard Q100 INT Sec C
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data

Mannings Coefficient	0.017
Channel Slope	0.40 %
Water Surface Elevation	79.72 ft
Elevation Range	78.74 to 80.11
Discharge	144.00 cfs



V:33.3333333
H:1
NTS

Decatur Blvd Q10 Dev Sec C

Worksheet for Irregular Channel

Project Description

Worksheet	Decatur Boulevard Q10 Sec C
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Channel Slope	0.40 %
Discharge	3.00 cfs

Options

Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results

Mannings Coefficient	0.013
Water Surface Elevation	79.13 ft
Elevation Range	78.74 to 80.11
Flow Area	2.0 ft ²
Wetted Perimeter	21.77 ft
Top Width	21.35 ft
Actual Depth	0.39 ft
Critical Elevation	78.74 ft
Critical Slope	0.00 %
Velocity	1.47 ft/s
Velocity Head	0.03 ft
Specific Energy	79.16 ft
Froude Number	0.84
Flow Type	Subcritical

Calculation Messages:
Flow is divided.

Roughness Segments

Start Station	End Station	Mannings Coefficient
0+00.00	0+08.50	0.033
0+08.50	0+10.00	0.013
0+10.00	0+46.00	0.016
0+46.00	0+50.00	0.013
0+50.00	1+00.00	0.016
1+00.00	1+02.00	0.013
1+02.00	1+12.00	0.033

Natural Channel Points

Station (ft)	Elevation (ft)
0+00.00	79.36
0+08.00	79.32
0+08.50	79.32
0+10.00	78.99

Dry Lane

$$\frac{79.61 - 79.13}{0.002} = 241$$

Decatur Blvd Q10 Dev Sec C
Worksheet for Irregular Channel

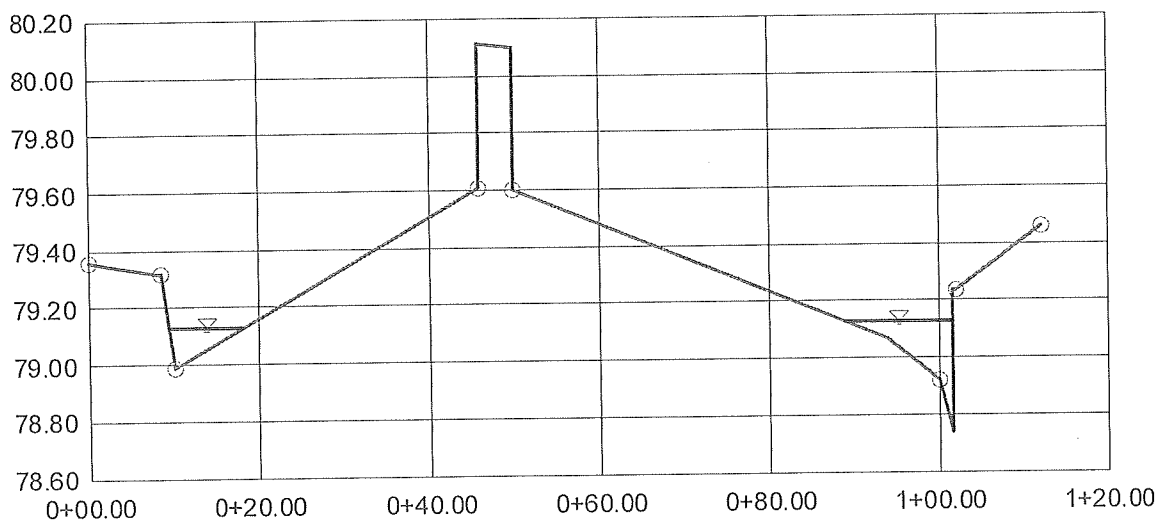
Natural Channel Points	
Station (ft)	Elevation (ft)
0+46.00	79.61
0+46.00	80.11
0+50.00	80.10
0+50.00	79.60
0+94.00	79.07
1+00.00	78.92
1+01.50	78.74
1+01.50	79.24
1+02.00	79.24
1+12.00	79.46

Decatur Blvd Q10 Dev Sec C

Cross Section for Irregular Channel

Project Description	
Worksheet	Decatur Boulevard Q10 Sec C
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.013
Channel Slope	0.40 %
Water Surface Elevation	79.13 ft
Elevation Range	78.74 to 80.11
Discharge	3.00 cfs



V:33.3333333
H:1
NTS

Decatur Blvd Q100 Dev Sec C

Worksheet for Irregular Channel

Project Description	
Worksheet	Decatur Boulevard Q100 Sec C
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.40 %
Discharge	144.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.017
Water Surface Elevation	79.72 ft
Elevation Range	78.74 to 80.11
Flow Area	45.9 ft ²
Wetted Perimeter	109.41 ft
Top Width	108.00 ft
Actual Depth	0.98 ft
Critical Elevation	78.74 ft
Critical Slope	0.00 %
Velocity	3.14 ft/s
Velocity Head	0.15 ft
Specific Energy	79.87 ft
Froude Number	0.85
Flow Type	Subcritical

Calculation Messages:

Water elevation exceeds lowest end station by 0.3618724 ft.
Flow is divided.

$$\frac{V \times \Delta}{3.14 \times 0.98 = 3.1}$$

OK

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+08.00	0.033
0+08.00	0+10.00	0.013
0+10.00	0+46.00	0.016
0+46.00	0+50.00	0.013
0+50.00	1+00.00	0.016
1+00.00	1+02.00	0.013
1+02.00	1+12.00	0.033

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	79.36
0+08.00	79.32
0+08.50	79.32

Decatur Blvd Q100 Dev Sec C
Worksheet for Irregular Channel

Natural Channel Points	
Station (ft)	Elevation (ft)
0+10.00	78.99
0+46.00	79.61
0+46.00	80.11
0+50.00	80.10
0+50.00	79.60
0+94.00	79.07
1+00.00	78.92
1+01.50	78.74
1+01.50	79.24
1+02.00	79.24
1+12.00	79.46

Decatur Blvd Q100 Dev Sec C

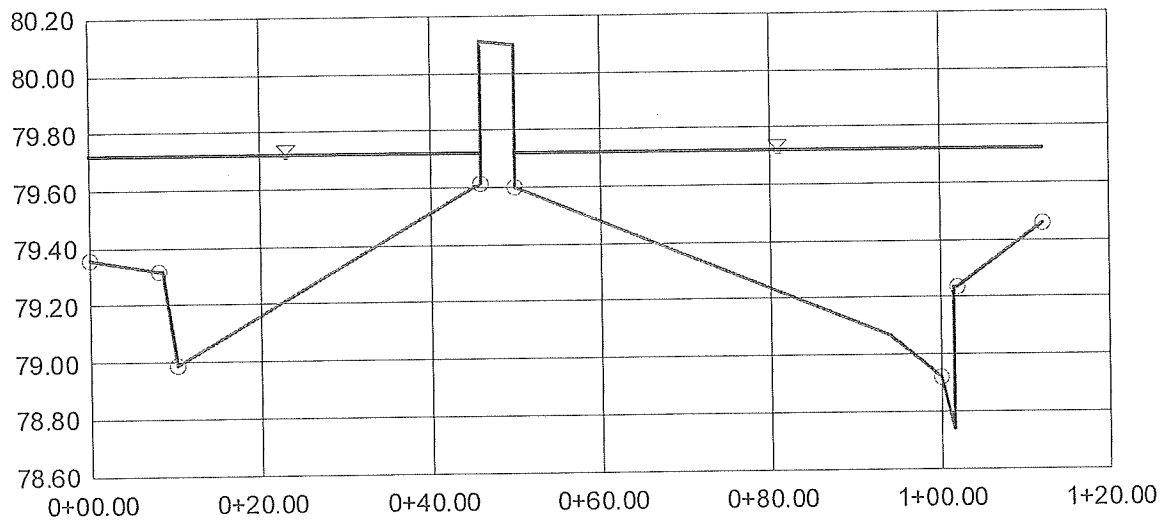
Cross Section for Irregular Channel

Project Description

Worksheet	Decatur Boulevard Q100 Sec C
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data

Mannings Coefficient	0.017
Channel Slope	0.40 %
Water Surface Elevation	79.72 ft
Elevation Range	78.74 to 80.11
Discharge	144.00 cfs



V:33.3333333
H:1
NTS

APPENDIX B

Response to Comment 4

Drop inlet sizing HEC-22

FHWA Urban Drainage Design Program, HY-22
 Drainage of Highway Pavements

Inlets on Grade
 Date: 12/12/2011

Project No. : Tropical & Centennial
 Project Name.:
 Computed by : Ray

Inlets on Grade: Curb Opening, Grate Inlet

Roadway and Discharge Data

	Cross Slope	Composite
S	Longitudinal Slope (ft/ft)	0.0090
Sx	Pavement Cross Slope (ft/ft)	0.0200
Sw	Gutter Cross Slope (ft/ft)	0.1130
n	Manning's Coefficient	0.016
W	Gutter Width (ft)	1.50
a	Gutter Depression (inch)	0.67
Q	Discharge (cfs)	3.000
T	Width of Spread (ft)	10.22

Gutter Flow

Eo	Gutter Flow Ratio	0.475
d	Depth of Flow (ft)	0.34
V	Average Velocity (ft/sec)	2.61

Inlet Interception

INLET INTERCEPTION	LT or WGR (ft)	L (ft)	E	Qi (cfs)	Qb (cfs)
Curb Opening	12.43	7.50	0.00	0.004	2.996
Parallel Bar P-1-7/8	1.50	7.49	0.85	2.538	0.458
Combination			0.85	2.542	0.458

Note: The curb opening length in the input screen is the total length of the curb opening including its length along the grate.

FHWA Urban Drainage Design Program, HY-22
 Drainage of Highway Pavements

Inlets on Sag
 Date: 12/06/2011

Project No. :MGL1101.000
 Project Name.:TROPICAL PKWY
 Computed by :

Inlets on Sag: Equal-Length Combination Inlet

Roadway and Discharge Data

	Cross Slope	Composite/Dep
Sx	Pavement Cross Slope (ft/ft)	0.0078
Sw	Gutter Cross Slope (ft/ft)	0.1130
n	Manning's Coefficient	0.016
W	Gutter Width (ft)	1.50
a	Gutter Depression (inch)	0.67

Inlet Interception

	Inlet Type *Sag*	Curb-Opening
L	Curb-Opening Length (ft)	15.00
H	Curb-Opening Height (in)	8.00
	Inlet Type *Sag*	Parallel Bar P-1-7/8
T	Width of Spread (ft)	79.88
WGR	Grate Width (ft)	1.50
L	Grate Length (ft)	15.00
	Inlet Type *Sag*	Equal Length Combination
d_ave	Depth of Flow (ft)	0.724
d_curb	Depth at Curb (ft)	0.837
Qi	Intercepted Flow (cfs)	25.000

APPENDIX C

Response to Comment 6

10-Year Interim Condition HEC-1
100-Year Interim Condition HEC-1
10-Year Developed Condition HEC-1
100-Year Developed Condition HEC-1
10-Year Existing Condition HEC-1
100-Year Existing Condition HEC-1
Reference Material Twilight at Riverwalk

10-Year Interim Condition

HEC-1

```

1*****
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*
* JUN 1998
*
* VERSION 4.1
*
* RUN DATE 09DEC11 TIME 10:51:30
*
*****
*****

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```

*
* U.S. ARMY CORPS OF ENGINEERS
*
* HYDROLOGIC ENGINEERING CENTER
*
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
*
* (916) 756-1104
*

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1 ID PROJECT NAME
2 ID TECHNICAL DRAINAGE STUDY
3 ID 10-YR INTERIM CONDITION
4 ID
5 ID RETURN PERIOD ----- 10- AND 100-YEAR
6 ID DISTRIBUTION ----- 6-HOUR SDN3
7 ID PROJECT NO. ----- MGL1101.000
8 ID FILENAME ----- INTERIM.H1
9 ID DATE ----- SEPTEMBER 2011
10 ID MODELED BY ----- SLATER HANIFAN GROUP
11 ID
12 ID SIX HOUR DEPTH-AREA REDUCTION FACTORS
13 ID DRAINAGE AREA (MI^2) DARF
14 ID 100-YR 0.990
15 ID 10-YR 0.570
16 ID
17 IT 5 0 0 300
18 IO 5 0 0
19 IN 5 0 0
20 JR PREC 0.570 0
*
21 KK DEC4
22 BA .0034
23 PB 2.77
24 PC 0 0.020 0.057 0.070 0.087 0.108 0.124 0.130 0.130 0.130
25 PC 0.130 0.130 0.130 0.133 0.140 0.142 0.148 0.158 0.172 0.181
26 PC 0.190 0.197 0.199 0.200 0.201 0.204 0.214 0.229 0.241 0.249
27 PC 0.251 0.256 0.270 0.278 0.281 0.283 0.295 0.322 0.352 0.409
28 PC 0.499 0.590 0.710 0.744 0.781 0.812 0.819 0.835 0.851 0.856
29 PC 0.860 0.868 0.876 0.888 0.910 0.926 0.937 0.950 0.970 0.976
30 PC 0.982 0.985 0.987 0.989 0.990 0.993 0.993 0.994 0.995 0.998
31 PC 0.998 0.999 1.000
32 LS 0 98.0
33 UD 0.136
*
34 KK DEC3
35 BA .0012
36 LS 0 98.0
37 UD 0.100
*
38 KK CP.11
39 KM COMBINATION POINT AT INTERSECTION DECATUR & TROPICAL
40 HC 2
*

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41 KK 005
 42 BA .0024
 43 LS 0 98.0
 44 UD 0.100
 *

1

HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

45 KK NNS
 46 KM REFERENCE FROM CNLV NN STUDY BASIN (DANN3A4)
 47 BA .50
 48 QI 0 0 0 0 0 0 0 0 0 0
 49 QI 0 0 0 0 0 0 0 0 0 0
 50 QI 0 0 0 0 0 0 0 0 0 0
 51 QI 0 0 0 0 0 0 0 0 0 0
 52 QI 0 0 0 0 0 0 0 0 0 0
 53 QI 0 0 0 0 0 0 0 0 0 0
 54 QI 0 0 0 0 0 0 0 0 0 0
 55 QI 0 0 0 0 0 0 0 0 0 0
 56 QI 0 0 0 0 0 0 0 0 0 0
 57 QI 0 0 0 0 0 0 0 0 0 0
 *

58 KK CP.I2
 59 KM COMBINATION POINT EAST OF C-STORE IN TROPICAL
 60 HC 2
 *

61 KK TROP1
 62 BA .0042
 63 LS 0 98.0
 64 UD 0.140
 *

65 KK ON1I
 66 BA .0024
 67 LS 0 83.3
 68 UD 0.100
 *

69 KK ON2I
 70 BA .0135
 71 LS 0 83.3
 72 UD 0.212
 *

73 KK CP.I3
 74 KM COMBINATION POINT JUST W OF CENT PKWY IN TROPICAL
 75 HC 4
 *

76 KK RH.5D
 77 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
 78 BA .0032
 79 LS 0 91.0
 80 UD 0.098
 *

1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

81 KK RH.6D
 82 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
 83 BA .0050
 84 LS 0 91.0
 85 UD 0.107
 *

86 KK CP.D6
 87 KM COMBINATION POINT AT INTERSECTION TWILIGHT
 88 KM COMBINATION POINT REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
 89 HC 2
 *

90 KK RH.4D
 91 BA .0005
 92 LS 0 91.0
 93 UD 0.069
 *

94 KK CENT2
 95 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
 96 BA .0026
 97 LS 0 98.0
 98 UD 0.082
 *

99 KK CENT4
 100 BA .0006
 101 LS 0 98.0
 102 UD 0.100

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      *
103      KK  CP.D7
104      KM  COMBINATION POINT NORTH OF INTERSECTION OF CENT PKWY IN TROPICAL
105      HC      4
      *

106      KK  CP.I5
107      KM  COMBINATION POINT AT INTERSECTION OF CENT PKWY IN TROPICAL
108      HC      2
      *

109      KK  OF.2I
110      KM  OFFSITE BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
111      BA  .0135
112      LS      0      83.4
113      UD  0.166
      *

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1

HEC-1 INPUT

PAGE 4

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

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```

114      KK  RIC1
115      BA  .0014
116      LS      0      98.0
117      UD  0.100
      *

118      KK  CP.I8
119      KM  COMBINATION POINT IN RICE
120      HC      2
      *

121      ZZ

```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE      (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.      (.) CONNECTOR      (<---) RETURN OF DIVERTED OR PUMPED FLOW

21      DEC4
      .
      .
34      .      DEC3
      .
      .
38      CP.I1.....
      .
      .
41      .      005
      .
      .
45      .      .      NNS
      .
      .
58      .      CP.I2.....
      .
      .
61      .      .      TROP1
      .
      .
65      .      .      .      ON1I
      .
      .
69      .      .      .      .      ON2I
      .
      .
73      .      CP.I3.....
      .
      .
76      .      .      RH.5D
      .
      .
81      .      .      .      RH.6D
      .
      .
86      .      .      CP.D6.....
      .
      .
90      .      .      .      RH.4D
      .
      .
94      .      .      .      .      CENT2
      .
      .
99      .      .      .      .      .      CENT4
      .
      .
103     .      .      CP.D7.....
      .
      .
106     .      .      CP.I5.....
      .
      .

```

109 . . . OF.2I

 114 . . . RIC1

 118 . . . CP.18.....

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

1*****

 *
 * FLOOD HYDROGRAPH PACKAGE (HEC-1) *
 * JUN 1998 *
 * VERSION 4.1 *
 *
 * RUN DATE 09DEC11 TIME 10:51:30 *
 *
 *

*
 * U.S. ARMY CORPS OF ENGINEERS
 * HYDROLOGIC ENGINEERING CENTER
 * 609 SECOND STREET
 * DAVIS, CALIFORNIA 95616
 * (916) 756-1104
 *

PROJECT NAME
 TECHNICAL DRAINAGE STUDY
 10-YR INTERIM CONDITION

 RETURN PERIOD ----- 10- AND 100-YEAR
 DISTRIBUTION ----- 6-HOUR SDN3
 PROJECT NO. ----- MGL1101.000
 FILENAME ----- INTERIM.H1
 DATE ----- SEPTEMBER 2011
 MODELED BY ----- SLATER HANIFAN GROUP

SIX HOUR DEPTH-AREA REDUCTION FACTORS
 DRAINAGE AREA (MI^2) DARF
 100-YR 0.990
 10-YR 0.570

18 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

 IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK

 COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .57

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION
				RATIO 1
				.57
HYDROGRAPH AT	DEC4	.00	1	FLOW
+				TIME
				3.
				3.58

HYDROGRAPH AT	DEC3	.00	1	FLOW	1.
+				TIME	3.50
2 COMBINED AT	CP.11	.00	1	FLOW	5.
+				TIME	3.58
HYDROGRAPH AT	005	.00	1	FLOW	3.
+				TIME	3.50
HYDROGRAPH AT	NNS	.50	1	FLOW	0.
+				TIME	.00
2 COMBINED AT	CP.12	.50	1	FLOW	3.
+				TIME	3.50
HYDROGRAPH AT	TROP1	.00	1	FLOW	4.
+				TIME	3.58
HYDROGRAPH AT	ON1I	.00	1	FLOW	1.
+				TIME	3.58
HYDROGRAPH AT	ON2I	.01	1	FLOW	4.
+				TIME	3.67
4 COMBINED AT	CP.13	.52	1	FLOW	12.
+				TIME	3.58
HYDROGRAPH AT	RH.5D	.00	1	FLOW	2.
+				TIME	3.50
HYDROGRAPH AT	RH.6D	.00	1	FLOW	4.
+				TIME	3.50
2 COMBINED AT	CP.D6	.01	1	FLOW	6.
+				TIME	3.50
HYDROGRAPH AT	RH.4D	.00	1	FLOW	0.
+				TIME	3.50
HYDROGRAPH AT	CENT2	.00	1	FLOW	3.
+				TIME	3.50
HYDROGRAPH AT	CENT4	.00	1	FLOW	1.
+				TIME	3.50
4 COMBINED AT	CP.D7	.01	1	FLOW	10.
+				TIME	3.50
2 COMBINED AT	CP.15	.53	1	FLOW	21.
+				TIME	3.58
HYDROGRAPH AT	OF.2I	.01	1	FLOW	5.
+				TIME	3.58
HYDROGRAPH AT	RIC1	.00	1	FLOW	2.
+				TIME	3.50
2 COMBINED AT	CP.18	.01	1	FLOW	6.
+				TIME	3.58

+9 cfs surface

*** NORMAL END OF HEC-1 ***

100-Year Interim Condition

HEC-1

```

1*****
*****
*
*
*   FLOOD HYDROGRAPH PACKAGE (HEC-1)
*
*   JUN   1998
*
*   VERSION 4.1
*
*
*   RUN DATE 09DEC11 TIME 10:54:47
*
*
*****
*****

```

```

*
*
*   U.S. ARMY CORPS OF ENGINEERS
*
*   HYDROLOGIC ENGINEERING CENTER
*
*   609 SECOND STREET
*
*   DAVIS, CALIFORNIA 95616
*
*   (916) 756-1104
*

```

```

X   X   XXXXXX   XXXXX   X
X   X   X       X   X   XX
X   X   X       X       X
XXXXXXX XXXX   X       XXXXX X
X   X   X       X       X
X   X   X       X   X   X
X   X   XXXXXX   XXXXX   XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1          ID      TROPICAL & CENTENNIAL ROADWAY IMPR
2          ID      TECHNICAL DRAINAGE STUDY
3          ID      100-YR INTERIM CONDITION
4          ID
5          ID      RETURN PERIOD ----- 10- AND 100-YEAR
6          ID      DISTRIBUTION ----- 6-HOUR SDN3
7          ID      PROJECT NO. ----- MGL1101.000
8          ID      FILENAME ----- INTERIM.H1
9          ID      DATE ----- SEPTEMBER 2011
10         ID      MODELED BY ----- SLATER HANIFAN GROUP
11         ID
12         ID      SIX HOUR DEPTH-AREA REDUCTION FACTORS
13         ID      DRAINAGE AREA (MI^2)      DARF
14         ID      100-YR      0.990
15         ID      10-YR      0.570
16         ID
17         IT      5          0          0          300
18         IO      5          0          0
19         IN      5          0          0
20         JR      PREC      0.990      0
*
21         KK      DEC4
22         BA      .0034
23         PB      2.77
24         PC      0          0.020      0.057      0.070      0.087      0.108      0.124      0.130      0.130      0.130
25         PC      0.130      0.130      0.130      0.133      0.140      0.142      0.148      0.158      0.172      0.181
26         PC      0.190      0.197      0.199      0.200      0.201      0.204      0.214      0.229      0.241      0.249
27         PC      0.251      0.256      0.270      0.278      0.281      0.283      0.295      0.322      0.352      0.409
28         PC      0.499      0.590      0.710      0.744      0.781      0.812      0.819      0.835      0.851      0.856
29         PC      0.860      0.868      0.876      0.888      0.910      0.926      0.937      0.950      0.970      0.976
30         PC      0.982      0.985      0.987      0.989      0.990      0.993      0.993      0.994      0.995      0.998
31         PC      0.998      0.999      1.000
32         LS      0          98.0
33         UD      0.136
*
34         KK      DEC3
35         BA      .0012
36         LS      0          98.0
37         UD      0.100
*
38         KK      CP.11
39         KM      COMBINATION POINT AT INTERSECTION DECATUR & TROPICAL
40         HC      2
*

```

41 KK 005
42 BA .0024
43 LS 0 98.0
44 UD 0.100
*

HEC-1 INPUT

PAGE 2

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

45 KK NNS
46 KM REFERENCE FROM CNLV NN STUDY BASIN (DANN3A4)
47 BA .50
48 QI 0 0 0 0 0 0 0 0 0 0
49 QI 0 0 0 0 0 0 0 0 0 0
50 QI 0 0 0 1 1 1 0 0 1 1
51 QI 1 1 1 1 1 1 1 1 1 1
52 QI 1 1 5 45 89 121 151 186 219 223
53 QI 193 151 110 73 43 24 12 4 1 1
54 QI 1 1 1 1 1 1 1 1 1 1
55 QI 1 1 1 1 1 1 1 1 1 1
56 QI 1 0 0 0 0 0 0 0 0 0
57 QI 0 0 0 0 0 0 0 0 0 0
*

58 KK CP.I2
59 KM COMBINATION POINT EAST OF C-STORE IN TROPICAL
60 HC 2
*

61 KK TROP1
62 BA .0042
63 LS 0 98.0
64 UD 0.140
*

65 KK ON1I
66 BA .0024
67 LS 0 83.3
68 UD 0.100
*

69 KK ON2I
70 BA .0135
71 LS 0 83.3
72 UD 0.212
*

73 KK CP.I3
74 KM COMBINATION POINT JUST W OF CENT PKWY IN TROPICAL
75 HC 4
*

76 KK RH.5D
77 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
78 BA .0032
79 LS 0 91.0
80 UD 0.098
*

HEC-1 INPUT

PAGE 3

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

81 KK RH.6D
82 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
83 BA .0050
84 LS 0 91.0
85 UD 0.107
*

86 KK CP.D6
87 KM COMBINATION POINT AT INTERSECTION TWILIGHT
88 KM COMBINATION POINT REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
89 HC 2
*

90 KK RH.4D
91 BA .0005
92 LS 0 91.0
93 UD 0.069
*

94 KK CENT2
95 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
96 BA .0026
97 LS 0 98.0
98 UD 0.082
*

99 KK CENT4
100 BA .0006
101 LS 0 98.0
102 UD 0.100

```

      *
103      KK  CP.D7
104      KM  COMBINATION POINT NORTH OF INTERSECTION OF CENT PKWY IN TROPICAL
105      HC      4
      *

106      KK  CP.I5
107      KM  COMBINATION POINT AT INTERSECTION OF CENT PKWY IN TROPICAL
108      HC      2
      *

109      KK  OF.2I
110      KM  OFFSITE BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
111      BA  .0135
112      LS      0      83.4
113      UD  0.166
      *

```

HEC-1 INPUT

PAGE 4

1

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

114      KK  RIC1
115      BA  .0014
116      LS      0      98.0
117      UD  0.100
      *

118      KK  CP.I8
119      KM  COMBINATION POINT IN RICE
120      HC      2
      *
121      ZZ

```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT LINE      (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.      (.) CONNECTOR      (<---) RETURN OF DIVERTED OR PUMPED FLOW

21      DEC4
      .
34      .      DEC3
      .
38      CP.I1.....
      .
41      .      005
      .
45      .      .      NNS
      .
58      .      CP.I2.....
      .
61      .      .      TROP1
      .
65      .      .      .      ON1I
      .
69      .      .      .      .      ON2I
      .
73      .      CP.I3.....
      .
76      .      .      RH.5D
      .
81      .      .      .      RH.6D
      .
86      .      .      CP.D6.....
      .
90      .      .      .      RH.4D
      .
94      .      .      .      .      CENT2
      .
99      .      .      .      .      .      CENT4
      .
103      .      .      CP.D7.....
      .
106      .      .      CP.I5.....
      .

```

109 . . . OF.2I

 114 . . . RIC1

 118 . . . CP.18.....

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

1*****

 *
 * FLOOD HYDROGRAPH PACKAGE (HEC-1) *
 * JUN 1998 *
 * VERSION 4.1 *
 *
 * RUN DATE 09DEC11 TIME 10:54:47 *
 *
 *

*
 * U.S. ARMY CORPS OF ENGINEERS
 * HYDROLOGIC ENGINEERING CENTER
 * 609 SECOND STREET
 * DAVIS, CALIFORNIA 95616
 * (916) 756-1104
 *

TROPICAL & CENTENNIAL ROADWAY IMPR
 TECHNICAL DRAINAGE STUDY
 100-YR INTERIM CONDITION
 RETURN PERIOD ----- 10- AND 100-YEAR
 DISTRIBUTION ----- 6-HOUR SDN3
 PROJECT NO. ----- MGL1101.000
 FILENAME ----- INTERIM.H1
 DATE ----- SEPTEMBER 2011
 MODELED BY ----- SLATER HANIFAN GROUP

SIX HOUR DEPTH-AREA REDUCTION FACTORS
 DRAINAGE AREA (MI^2) DARF
 100-YR 0.990
 10-YR 0.570

18 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .99

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	
				.99	
HYDROGRAPH AT					
+	DEC4	.00	1 FLOW	6.	
			TIME	3.58	

HYDROGRAPH AT	DEC3	.00	1	FLOW TIME	2. 3.50
+ 2 COMBINED AT	CP.I1	.00	1	FLOW TIME	8. 3.58
HYDROGRAPH AT	005	.00	1	FLOW TIME	5. 3.50
+ HYDROGRAPH AT	NNS	.50	1	FLOW TIME	223. 4.08
+ 2 COMBINED AT	CP.I2	.50	1	FLOW TIME	224. 4.08
HYDROGRAPH AT	TROP1	.00	1	FLOW TIME	8. 3.58
+ HYDROGRAPH AT	ON1I	.00	1	FLOW TIME	3. 3.50
+ HYDROGRAPH AT	ON2I	.01	1	FLOW TIME	13. 3.67
+ 4 COMBINED AT	CP.I3	.52	1	FLOW TIME	230. 4.08
HYDROGRAPH AT	RH.5D	.00	1	FLOW TIME	5. 3.50
+ HYDROGRAPH AT	RH.6D	.00	1	FLOW TIME	8. 3.50
+ 2 COMBINED AT	CP.D6	.01	1	FLOW TIME	13. 3.50
HYDROGRAPH AT	RH.4D	.00	1	FLOW TIME	1. 3.50
+ HYDROGRAPH AT	CENT2	.00	1	FLOW TIME	5. 3.50
+ HYDROGRAPH AT	CENT4	.00	1	FLOW TIME	1. 3.50
+ 4 COMBINED AT	CP.D7	.01	1	FLOW TIME	21. 3.50
+ 2 COMBINED AT	CP.I5	.53	1	FLOW TIME	233. 4.08
HYDROGRAPH AT	OF.2I	.01	1	FLOW TIME	14. 3.58
+ HYDROGRAPH AT	RIC1	.00	1	FLOW TIME	3. 3.50
+ 2 COMBINED AT	CP.I8	.01	1	FLOW TIME	17. 3.58

+ 155 surface from Ref.

*** NORMAL END OF HEC-1 ***

10-Year Developed Condition

HEC-1

```

1*****
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*
* JUN 1998
*
* VERSION 4.1
*
*
* RUN DATE 09DEC11 TIME 10:16:38
*
*
*****
*****

```

```

*
* U.S. ARMY CORPS OF ENGINEERS
*
* HYDROLOGIC ENGINEERING CENTER
*
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
*
* (916) 756-1104
*

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1          ID      TROPICAL & CENTENNIAL ROADWAY
2          ID      TECHNICAL DRAINAGE STUDY
3          ID      10-YEAR DEVELOPED
4          ID
5          ID      RETURN PERIOD ----- 10-YR
6          ID      DISTRIBUTION ----- 6-HOUR SDN3
7          ID      PROJECT NO. ----- MGL1101.000
8          ID      FILENAME ----- 10YRDEV.H1
9          ID      DATE ----- DECEMBER 2011
10         ID      MODELED BY ----- SLATER HANIFAN GROUP
11         ID
12         ID      SIX HOUR DEPTH-AREA REDUCTION FACTORS
13         ID      DRAINAGE AREA (MI^2)      DARF
14         ID      100-YR      0.990
15         ID      10-YR      0.570
16         ID
17         IT      5      0      0      300
18         IO      5      0      0
19         IN      5      0      0
20         JR      PREC  0.570      0
*
21         KK      DEC4
22         BA      .0034
23         PB      2.77
24         PC      0      0.020  0.057  0.070  0.087  0.108  0.124  0.130  0.130  0.130
25         PC      0.130  0.130  0.130  0.133  0.140  0.142  0.148  0.158  0.172  0.181
26         PC      0.190  0.197  0.199  0.200  0.201  0.204  0.214  0.229  0.241  0.249
27         PC      0.251  0.256  0.270  0.278  0.281  0.283  0.295  0.322  0.352  0.409
28         PC      0.499  0.590  0.710  0.744  0.781  0.812  0.819  0.835  0.851  0.856
29         PC      0.860  0.868  0.876  0.888  0.910  0.926  0.937  0.950  0.970  0.976
30         PC      0.982  0.985  0.987  0.989  0.990  0.993  0.993  0.994  0.995  0.998
31         PC      0.998  0.999  1.000
32         LS      0      98.0
33         UD      0.136
*
34         KK      DEC3
35         BA      .0012
36         LS      0      98.0
37         UD      0.100
*
38         KK      CP.D1
39         KM      COMBINATION POINT AT INTERSECTION DECATUR & TROPICAL
40         HC      2
*

```

41 KK 005
42 BA .0024
43 LS 0 98.0
44 UD 0.100
*

HEC-1 INPUT

PAGE 2

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

45 KK NNS
46 KM REFERENCE FROM CNLV NN STUDY BASIN (DANN3A4)
47 BA .50
48 QI 0 0 0 0 0 0 0 0 0 0
49 QI 0 0 0 0 0 0 0 0 0 0
50 QI 0 0 0 0 0 0 0 0 0 0
51 QI 0 0 0 0 0 0 0 0 0 0
52 QI 0 0 0 0 0 0 0 0 0 0
53 QI 0 0 0 0 0 0 0 0 0 0
54 QI 0 0 0 0 0 0 0 0 0 0
55 QI 0 0 0 0 0 0 0 0 0 0
56 QI 0 0 0 0 0 0 0 0 0 0
57 QI 0 0 0 0 0 0 0 0 0 0
58

59 KK CP.D2
60 KM COMBINATION POINT EAST OF C-STORE IN TROPICAL
61 HC 2
*

62 KK TROP1
63 BA .0042
64 LS 0 98.0
65 UD 0.140
*

66 KK ON1D
67 BA .0024
68 LS 0 98.0
69 UD 0.100
*

70 KK ON2D
71 BA .0135
72 LS 0 98.0
73 UD 0.212
*

74 KK CP.D3
75 KM COMBINATION POINT JUST W OF CENT PKWY IN TROPICAL
76 HC 4
*

77 KK RH.5D
78 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
79 BA .0032
80 LS 0 91.0
81 UD 0.098
*

HEC-1 INPUT

PAGE 3

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

82 KK RH.6D
83 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
84 BA .0050
85 LS 0 91.0
86 UD 0.107
*

87 KK CP.D6
88 KM COMBINATION POINT AT INTERSECTION TWILIGHT
89 KM COMBINATION POINT REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
90 HC 2
*

91 KK RH.4D
92 BA .0005
93 LS 0 91.0
94 UD 0.069
*

95 KK CENT2
96 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
97 BA .0026
98 LS 0 98.0
99 UD 0.082
*

100 KK CENT4
101 BA .0006
102 LS 0 98.0
103 UD 0.100

```

      *
104      KK  CP.D7
105      KM  COMBINATION POINT NORTH OF INTERSECTION OF CENT PKWY IN TROPICAL
106      HC  4
      *

107      KK  CP.D5
108      KM  COMBINATION POINT AT INTERSECTION OF CENT PKWY IN TROPICAL
109      HC  2
      *

110      KK  OF.2D
111      KM  OFFSITE BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
112      BA  .0135
113      LS  0    98.0
114      UD  0.166
      *

```

HEC-1 INPUT

PAGE 4

1

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

115      KK  RIC1
116      BA  .0014
117      LS  0    98.0
118      UD  0.100
      *

119      KK  CP.D8
120      KM  COMBINATION POINT IN RICE
121      HC  2
      *
122      ZZ

```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE  (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
      (.) CONNECTOR    (<---) RETURN OF DIVERTED OR PUMPED FLOW

NO.   (.) CONNECTOR    (<---) RETURN OF DIVERTED OR PUMPED FLOW

21     DEC4
      .
34     .      DEC3
      .
38     CP.D1.....
      .
41     .      005
      .
45     .      NNS
      .
59     .      CP.D2.....
      .
62     .      TROP1
      .
66     .      .      ON1D
      .
70     .      .      .      ON2D
      .
74     .      CP.D3.....
      .
77     .      .      RH.5D
      .
82     .      .      .      RH.6D
      .
87     .      .      CP.D6.....
      .
91     .      .      .      RH.4D
      .
95     .      .      .      .      CENT2
      .
100    .      .      .      .      .      CENT4
      .
104    .      .      CP.D7.....
      .
107    .      CP.D5.....
      .

```

110 . . . OF.2D
 115 . . . RIC1
 119 . . . CP.D8.....

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*
* JUN 1998
*
* VERSION 4.1
*
* RUN DATE 09DEC11 TIME 10:16:38
*
*****
  
```

* U.S. ARMY CORPS OF ENGINEERS
 * HYDROLOGIC ENGINEERING CENTER
 * 609 SECOND STREET
 * DAVIS, CALIFORNIA 95616
 * (916) 756-1104
 *

TROPICAL & CENTENNIAL ROADWAY
 TECHNICAL DRAINAGE STUDY
 10-YEAR DEVELOPED

RETURN PERIOD ----- 10-YR
 DISTRIBUTION ----- 6-HOUR SDN3
 PROJECT NO. ----- MGL1101.000
 FILENAME ----- 10YRDEV.H1
 DATE ----- DECEMBER 2011
 MODELED BY ----- SLATER HANIFAN GROUP

SIX HOUR DEPTH-AREA REDUCTION FACTORS
 DRAINAGE AREA (MI^2) DARF
 100-YR 0.990
 10-YR 0.570

18 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .57

*** HEC-1 ERROR 1 *** INVALID CARD IDENTIFICATION CODE OR CARD OUT OF SEQUENCE
 CARD NO. 58

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION
				RATIO 1
				.57

HYDROGRAPH AT +	DEC4	.00	1	FLOW TIME	3. 3.58
HYDROGRAPH AT +	DEC3	.00	1	FLOW TIME	1. 3.50
2 COMBINED AT +	CP.D1	.00	1	FLOW TIME	5. 3.58
HYDROGRAPH AT +	005	.00	1	FLOW TIME	3. 3.50
HYDROGRAPH AT +	NNS	.50	1	FLOW TIME	0. .00
2 COMBINED AT +	CP.D2	.50	1	FLOW TIME	3. 3.50
HYDROGRAPH AT +	TROP1	.00	1	FLOW TIME	4. 3.58
HYDROGRAPH AT +	ON1D	.00	1	FLOW TIME	3. 3.50
HYDROGRAPH AT +	ON2D	.01	1	FLOW TIME	12. 3.58
4 COMBINED AT +	CP.D3	.52	1	FLOW TIME	21. 3.58
HYDROGRAPH AT +	RH.5D	.00	1	FLOW TIME	2. 3.50
HYDROGRAPH AT +	RH.6D	.00	1	FLOW TIME	4. 3.50
2 COMBINED AT +	CP.D6	.01	1	FLOW TIME	6. 3.50
HYDROGRAPH AT +	RH.4D	.00	1	FLOW TIME	0. 3.50
HYDROGRAPH AT +	CENT2	.00	1	FLOW TIME	3. 3.50
HYDROGRAPH AT +	CENT4	.00	1	FLOW TIME	1. 3.50
4 COMBINED AT +	CP.D7	.01	1	FLOW TIME	10. 3.50
2 COMBINED AT +	CP.D5	.53	1	FLOW TIME	30. 3.58
HYDROGRAPH AT +	OF.2D	.01	1	FLOW TIME	13. 3.58
HYDROGRAPH AT +	RIC1	.00	1	FLOW TIME	2. 3.50
2 COMBINED AT +	CP.D8	.01	1	FLOW TIME	15. 3.58

+ 9 cfs surface flow

*** 1 ERROR(S) DETECTED BY HEC-1 ***
2

100-Year Developed Condition

HEC-1

```

1*****
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*
* JUN 1998
*
* VERSION 4.1
*
* RUN DATE 09DEC11 TIME 10:19:28
*
*****
*****

```

```

*
* U.S. ARMY CORPS OF ENGINEERS
*
* HYDROLOGIC ENGINEERING CENTER
*
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
*
* (916) 756-1104
*

```

```

X X XXXXXX XXXX X
X X X X XX
X X X X X
XXXXXX XXXX X XXXX X
X X X X X
X X X X X
X X XXXXXX XXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1 ID TROPICAL CENTENNIAL
2 ID TECHNICAL DRAINAGE STUDY
3 ID 100-YR CONDITION
4 ID
5 ID RETURN PERIOD ----- 10- AND 100-YEAR
6 ID DISTRIBUTION ----- 6-HOUR SDN3
7 ID PROJECT NO. ----- MGL1101.000
8 ID FILENAME ----- DEVELOPED.H1
9 ID DATE ----- SEPTEMBER 2011
10 ID MODELED BY ----- SLATER HANIFAN GROUP
11 ID
12 ID SIX HOUR DEPTH-AREA REDUCTION FACTORS
13 ID DRAINAGE AREA (MI^2) DARF
14 ID 100-YR 0.990
15 ID 10-YR 0.570
16 ID
17 IT 5 0 0 300
18 IO 5 0 0
19 IN 5 0 0
20 JR PREC 0.990 0
*
21 KK DEC4
22 BA .0034
23 PB 2.77
24 PC 0 0.020 0.057 0.070 0.087 0.108 0.124 0.130 0.130 0.130
25 PC 0.130 0.130 0.130 0.133 0.140 0.142 0.148 0.158 0.172 0.181
26 PC 0.190 0.197 0.199 0.200 0.201 0.204 0.214 0.229 0.241 0.249
27 PC 0.251 0.256 0.270 0.278 0.281 0.283 0.295 0.322 0.352 0.409
28 PC 0.499 0.590 0.710 0.744 0.781 0.812 0.819 0.835 0.851 0.856
29 PC 0.860 0.868 0.876 0.888 0.910 0.926 0.937 0.950 0.970 0.976
30 PC 0.982 0.985 0.987 0.989 0.990 0.993 0.993 0.994 0.995 0.998
31 PC 0.998 0.999 1.000
32 LS 0 98.0
33 UD 0.136
*
34 KK DEC3
35 BA .0012
36 LS 0 98.0
37 UD 0.100
*
38 KK CP.D1
39 KM COMBINATION POINT AT INTERSECTION DECATUR & TROPICAL
40 HC 2
*

```

41 KK 005
42 BA .0024
43 LS 0 98.0
44 UD 0.100
*

HEC-1 INPUT

PAGE 2

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

45 KK NNS
46 KM REFERENCE FROM CNLV NN STUDY BASIN (DANN3A4)
47 BA .50
48 QI 0 0 0 0 0 0 0 0 0 0
49 QI 0 0 0 0 0 0 0 0 0 0
50 QI 0 0 0 1 1 1 0 0 1 1
51 QI 1 1 1 1 1 1 1 1 1 1
52 QI 1 1 5 45 89 121 151 186 219 223
53 QI 193 151 110 73 43 24 12 4 1 1
54 QI 1 1 1 1 1 1 1 1 1 1
55 QI 1 1 1 1 1 1 1 1 1 1
56 QI 1 0 0 0 0 0 0 0 0 0
57 QI 0 0 0 0 0 0 0 0 0 0
58

59 KK CP.D2
60 KM COMBINATION POINT EAST OF C-STORE IN TROPICAL
61 HC 2
*

62 KK TROP1
63 BA .0042
64 LS 0 98.0
65 UD 0.140
*

66 KK ON1D
67 BA .0024
68 LS 0 98.0
69 UD 0.100
*

70 KK ON2D
71 BA .0135
72 LS 0 98.0
73 UD 0.212
*

74 KK CP.D3
75 KM COMBINATION POINT JUST W OF CENT PKWY IN TROPICAL
76 HC 4
*

77 KK RH.5D
78 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
79 BA .0032
80 LS 0 91.0
81 UD 0.098
*

HEC-1 INPUT

PAGE 3

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

82 KK RH.6D
83 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
84 BA .0050
85 LS 0 91.0
86 UD 0.107
*

87 KK CP.D6
88 KM COMBINATION POINT AT INTERSECTION TWILIGHT
89 KM COMBINATION POINT REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
90 HC 2
*

91 KK RH.4D
92 BA .0005
93 LS 0 91.0
94 UD 0.069
*

95 KK CENT2
96 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
97 BA .0026
98 LS 0 98.0
99 UD 0.082
*

100 KK CENT4
101 BA .0006
102 LS 0 98.0
103 UD 0.100

```

      *
104      KK  CP.D7
105      KM  COMBINATION POINT NORTH OF INTERSECTION OF CENT PKWY IN TROPICAL
106      HC      4
      *

107      KK  CP.D5
108      KM  COMBINATION POINT AT INTERSECTION OF CENT PKWY IN TROPICAL
109      HC      2
      *

110      KK  OF.2D
111      KM  OFFSITE BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
112      BA  .0135
113      LS      0    98.0
114      UD  0.166
      *

```

1

HEC-1 INPUT

PAGE 4

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

115      KK  RIC1
116      BA  .0014
117      LS      0    98.0
118      UD  0.100
      *

119      KK  CP.D8
120      KM  COMBINATION POINT IN RICE
121      HC      2
      *
122      ZZ

```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE      (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.      (.) CONNECTOR      (<---) RETURN OF DIVERTED OR PUMPED FLOW

21      DEC4
      .
      .
34      .      DEC3
      .
      .
38      CP.D1.....
      .
      .
41      .      005
      .
      .
45      .      .      NNS
      .
      .
59      .      CP.D2.....
      .
      .
62      .      .      TROP1
      .
      .
66      .      .      .      ON1D
      .
      .
70      .      .      .      .      ON2D
      .
      .
74      .      CP.D3.....
      .
      .
77      .      .      RH.5D
      .
      .
82      .      .      .      RH.6D
      .
      .
87      .      .      CP.D6.....
      .
      .
91      .      .      .      RH.4D
      .
      .
95      .      .      .      .      CENT2
      .
      .
100     .      .      .      .      .      CENT4
      .
      .
104     .      .      CP.D7.....
      .
      .
107     .      .      CP.D5.....
      .
      .

```

```

110      .      .      OF.2D
      .      .      .
115      .      .      .      RIC1
      .      .      .
119      .      .      CP.D8.....

(*** ) RUNOFF ALSO COMPUTED AT THIS LOCATION
1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*
*      JUN      1998
*
*      VERSION 4.1
*
*
* RUN DATE 09DEC11 TIME 10:19:28
*
*
*****
*****

```

```

*
* U.S. ARMY CORPS OF ENGINEERS
*
* HYDROLOGIC ENGINEERING CENTER
*
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
*
* (916) 756-1104
*

```

```

TROPICAL CENTENNIAL
TECHNICAL DRAINAGE STUDY
100-YR CONDITION

RETURN PERIOD ----- 10- AND 100-YEAR
DISTRIBUTION ----- 6-HOUR SDN3
PROJECT NO. ----- MGL1101.000
FILENAME ----- DEVELOPED.H1
DATE ----- SEPTEMBER 2011
MODELED BY ----- SLATER HANIFAN GROUP

```

```

SIX HOUR DEPTH-AREA REDUCTION FACTORS
DRAINAGE AREA (MI^2)      DARF
100-YR                    0.990
10-YR                     0.570

```

```

18 IO      OUTPUT CONTROL VARIABLES
      IPRNT      5 PRINT CONTROL
      IPLOT      0 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE

IT      HYDROGRAPH TIME DATA
      NMIN      5 MINUTES IN COMPUTATION INTERVAL
      IDATE      1 0 STARTING DATE
      ITIME      0000 STARTING TIME
      NQ      300 NUMBER OF HYDROGRAPH ORDINATES
      NDDATE      2 0 ENDING DATE
      NDTIME      0055 ENDING TIME
      ICENT      19 CENTURY MARK

      COMPUTATION INTERVAL .08 HOURS
      TOTAL TIME BASE 24.92 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW      CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

```

```

JP      MULTI-PLAN OPTION
      NPLAN      1 NUMBER OF PLANS

```

```

JR      MULTI-RATIO OPTION
      RATIOS OF PRECIPITATION
      .99

```

```

*** HEC-1 ERROR 1 *** INVALID CARD IDENTIFICATION CODE OR CARD OUT OF SEQUENCE
CARD NO. 58

```

1

```

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
      FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
      TIME TO PEAK IN HOURS

```

```

OPERATION      STATION      AREA      PLAN      RATIOS APPLIED TO PRECIPITATION
      RATIO 1
      .99

```

HYDROGRAPH AT	DEC4	.00	1	FLOW	6.
+				TIME	3.58
HYDROGRAPH AT	DEC3	.00	1	FLOW	2.
+				TIME	3.50
2 COMBINED AT	CP.D1	.00	1	FLOW	8.
+				TIME	3.58
HYDROGRAPH AT	005	.00	1	FLOW	5.
+				TIME	3.50
HYDROGRAPH AT	NNS	.50	1	FLOW	223.
+				TIME	4.08
2 COMBINED AT	CP.D2	.50	1	FLOW	224.
+				TIME	4.08
HYDROGRAPH AT	TROP1	.00	1	FLOW	8.
+				TIME	3.58
HYDROGRAPH AT	ON1D	.00	1	FLOW	5.
+				TIME	3.50
HYDROGRAPH AT	ON2D	.01	1	FLOW	22.
+				TIME	3.58
4 COMBINED AT	CP.D3	.52	1	FLOW	232.
+				TIME	4.08
HYDROGRAPH AT	RH.5D	.00	1	FLOW	5.
+				TIME	3.50
HYDROGRAPH AT	RH.6D	.00	1	FLOW	8.
+				TIME	3.50
2 COMBINED AT	CP.D6	.01	1	FLOW	13.
+				TIME	3.50
HYDROGRAPH AT	RH.4D	.00	1	FLOW	1.
+				TIME	3.50
HYDROGRAPH AT	CENT2	.00	1	FLOW	5.
+				TIME	3.50
HYDROGRAPH AT	CENT4	.00	1	FLOW	1.
+				TIME	3.50
4 COMBINED AT	CP.D7	.01	1	FLOW	21.
+				TIME	3.50
2 COMBINED AT	CP.D5	.53	1	FLOW	235.
+				TIME	4.08
HYDROGRAPH AT	OF.2D	.01	1	FLOW	24.
+				TIME	3.58
HYDROGRAPH AT	RIC1	.00	1	FLOW	3.
+				TIME	3.50
2 COMBINED AT	CP.D8	.01	1	FLOW	26.
+				TIME	3.58

+ 155 cts surface flow

*** 1 ERROR(S) DETECTED BY HEC-1 ***

10-Year Existing Condition

HEC-1

```

1*****
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*
* JUN 1998 *
*
* VERSION 4.1 *
*
* RUN DATE 09DEC11 TIME 13:20:57 *
*
*****
*****

```

```

*
* U.S. ARMY CORPS OF ENGINEERS
*
* HYDROLOGIC ENGINEERING CENTER
*
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
*
* (916) 756-1104
*

```

```

X X XXXXXX XXXX X
X X X X X XX
X X X X X X
XXXXXX XXXX X XXXX X
X X X X X X
X X X X X X
X X XXXXXX XXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1      ID      PROJECT NAME
2      ID      TECHNICAL DRAINAGE STUDY
3      ID      10-YEAR EXISTING CONDITION
4      ID
5      ID      RETURN PERIOD ----- 10- AND 100-YEAR
6      ID      DISTRIBUTION ----- 6-HOUR SDN3
7      ID      PROJECT NO. ----- MGL1101.000
8      ID      FILENAME ----- EXISTING.H1
9      ID      DATE ----- SEPTEMBER 2011
10     ID      MODELED BY ----- SLATER HANIFAN GROUP
11     ID
12     ID      SIX HOUR DEPTH-AREA REDUCTION FACTORS
13     ID      DRAINAGE AREA (MI^2)      DARF
14     ID      100-YR      0.990
15     ID      10-YR      0.570
16     ID
17     IT      5      0      0      300
18     IO      5      0      0
19     IN      5      0      0
20     JR      PREC  0.570      0
*
21     KK      DEC4
22     BA      .0034
23     PB      2.77
24     PC      0      0.020  0.057  0.070  0.087  0.108  0.124  0.130  0.130  0.130
25     PC      0.130  0.130  0.130  0.133  0.140  0.142  0.148  0.158  0.172  0.181
26     PC      0.190  0.197  0.199  0.200  0.201  0.204  0.214  0.229  0.241  0.249
27     PC      0.251  0.256  0.270  0.278  0.281  0.283  0.295  0.322  0.352  0.409
28     PC      0.499  0.590  0.710  0.744  0.781  0.812  0.819  0.835  0.851  0.856
29     PC      0.860  0.868  0.876  0.888  0.910  0.926  0.937  0.950  0.970  0.976
30     PC      0.982  0.985  0.987  0.989  0.990  0.993  0.993  0.994  0.995  0.998
31     PC      0.998  0.999  1.000
32     LS      0      98.0
33     UD      0.136
*
34     KK      DEC3
35     BA      .0012
36     LS      0      98.0
37     UD      0.100
*
38     KK      CP.E1
39     KM      COMBINATION POINT AT INTERSECTION DECATUR & TROPICAL
40     HC      2
*

```

41 KK 005
42 BA .0024
43 LS 0 98.0
44 UD 0.100
*

HEC-1 INPUT

PAGE 2

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

45 KK NNS
46 KM REFERENCE FROM CNLV NN STUDY BASIN (DANN3A4)
47 BA .50
48 QI 0 0 0 0 0 0 0 0 0 0
49 QI 0 0 0 0 0 0 0 0 0 0
50 QI 0 0 0 0 0 0 0 0 0 0
51 QI 0 0 0 0 0 0 0 0 0 0
52 QI 0 0 0 0 0 0 0 0 0 0
53 QI 0 0 0 0 0 0 0 0 0 0
54 QI 0 0 0 0 0 0 0 0 0 0
55 QI 0 0 0 0 0 0 0 0 0 0
56 QI 0 0 0 0 0 0 0 0 0 0
57 QI 0 0 0 0 0 0 0 0 0 0
*

58 KK CP.E2
59 KM COMBINATION POINT EAST OF C-STORE IN TROPICAL
60 HC 2
*

61 KK TROP1
62 BA .0032
63 LS 0 98.0
64 UD 0.139
*

65 KK ON1E
66 BA .0024
67 LS 0 83.3
68 UD 0.100
*

69 KK ON2E
70 BA .0152
71 LS 0 83.3
72 UD 0.212
*

73 KK CP.E3
74 KM COMBINATION POINT JUST W OF CENT PKWY IN TROPICAL
75 HC 4
*

76 KK RH.5D
77 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
78 BA .0032
79 LS 0 91.0
80 UD 0.098
*

HEC-1 INPUT

PAGE 3

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

81 KK RH.6D
82 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
83 BA .0050
84 LS 0 91.0
85 UD 0.107
*

86 KK CP.D6
87 KM COMBINATION POINT AT INTERSECTION TWILIGHT
88 KM COMBINATION POINT REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
89 HC 2
*

90 KK RH.4D
91 BA .0005
92 LS 0 91.0
93 UD 0.069
*

94 KK CENT2
95 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
96 BA .0026
97 LS 0 98.0
98 UD 0.082
*

99 KK CENT4
100 BA .0002
101 LS 0 98.0
102 UD 0.100

```

*
103      KK  CP.D7
104      KM  COMBINATION POINT NORTH OF INTERSECTION OF CENT PKWY IN TROPICAL
105      HC      4
      *

106      KK  CP.E5
107      KM  COMBINATION POINT AT INTERSECTION OF CENT PKWY IN TROPICAL
108      HC      2
      *

109      KK  OF.2E
110      KM  OFFSITE BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
111      BA  .0135
112      LS      0      83.4
113      UD  0.166
      *

```

1 HEC-1 INPUT PAGE 4

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

114      KK  RIC1
115      BA  .0014
116      LS      0      98.0
117      UD  0.100
      *

118      KK  CP.E8
119      KM  COMBINATION POINT IN RICE
120      HC      2
      *
121      ZZ

```

1 SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE  (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.    (.) CONNECTOR  (<---) RETURN OF DIVERTED OR PUMPED FLOW

21      DEC4
      .
34      .      DEC3
      .
38      CP.E1.....
      .
41      .      005
      .
45      .      .      NNS
      .
58      CP.E2.....
      .
61      .      .      TROP1
      .
65      .      .      .      ON1E
      .
69      .      .      .      .      ON2E
      .
73      CP.E3.....
      .
76      .      .      RH.5D
      .
81      .      .      .      RH.6D
      .
86      .      .      CP.D6.....
      .
90      .      .      .      RH.4D
      .
94      .      .      .      .      CENT2
      .
99      .      .      .      .      .      CENT4
      .
103     .      .      CP.D7.....
      .
106     CP.E5.....
      .

```

109 . . OF.2E
 114 . . RIC1
 118 . . CP.E8.....

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

 *
 * FLOOD HYDROGRAPH PACKAGE (HEC-1) *
 * JUN 1998 *
 * VERSION 4.1 *
 *
 * RUN DATE 09DEC11 TIME 13:20:57 *
 *
 *

*
 * U.S. ARMY CORPS OF ENGINEERS
 * HYDROLOGIC ENGINEERING CENTER
 * 609 SECOND STREET
 * DAVIS, CALIFORNIA 95616
 * (916) 756-1104
 *

PROJECT NAME
 TECHNICAL DRAINAGE STUDY
 10-YEAR EXISTING CONDITION

 RETURN PERIOD ----- 10- AND 100-YEAR
 DISTRIBUTION ----- 6-HOUR SDN3
 PROJECT NO. ----- MGL1101.000
 FILENAME ----- EXISTING.H1
 DATE ----- SEPTEMBER 2011
 MODELED BY ----- SLATER HANIFAN GROUP

SIX HOUR DEPTH-AREA REDUCTION FACTORS
 DRAINAGE AREA (MI^2) DARF
 100-YR 0.990
 10-YR 0.570

18 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

 IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK

 COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .57

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	
				.57	
HYDROGRAPH AT	DEC4	.00	1	FLOW	3.
+				TIME	3.58

HYDROGRAPH AT	DEC3	.00	1	FLOW TIME	1. 3.50
+ 2 COMBINED AT	CP.E1	.00	1	FLOW TIME	5. 3.58
HYDROGRAPH AT	005	.00	1	FLOW TIME	3. 3.50
+ HYDROGRAPH AT	NNS	.50	1	FLOW TIME	0. .00
+ 2 COMBINED AT	CP.E2	.50	1	FLOW TIME	3. 3.50
HYDROGRAPH AT	TROP1	.00	1	FLOW TIME	3. 3.58
+ HYDROGRAPH AT	ON1E	.00	1	FLOW TIME	1. 3.58
+ HYDROGRAPH AT	ON2E	.02	1	FLOW TIME	5. 3.67
+ 4 COMBINED AT	CP.E3	.52	1	FLOW TIME	11. 3.58
HYDROGRAPH AT	RH.5D	.00	1	FLOW TIME	2. 3.50
+ HYDROGRAPH AT	RH.6D	.00	1	FLOW TIME	4. 3.50
+ 2 COMBINED AT	CP.D6	.01	1	FLOW TIME	6. 3.50
HYDROGRAPH AT	RH.4D	.00	1	FLOW TIME	0. 3.50
+ HYDROGRAPH AT	CENT2	.00	1	FLOW TIME	3. 3.50
+ HYDROGRAPH AT	CENT4	.00	1	FLOW TIME	0. 3.50
+ 4 COMBINED AT	CP.D7	.01	1	FLOW TIME	10. 3.50
+ 2 COMBINED AT	CP.E5	.53	1	FLOW TIME	20. 3.58
HYDROGRAPH AT	OF.2E	.01	1	FLOW TIME	5. 3.58
+ HYDROGRAPH AT	RIC1	.00	1	FLOW TIME	2. 3.50
+ 2 COMBINED AT	CP.E8	.01	1	FLOW TIME	6. 3.58

+ oblate 9c/s flow

*** NORMAL END OF HEC-1 ***

100-Year Existing Condition

HEC-1

```

1*****
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*
* JUN 1998
*
* VERSION 4.1
*
*
* RUN DATE 09DEC11 TIME 13:21:51
*
*
*****
*****

```

```

*
* U.S. ARMY CORPS OF ENGINEERS
*
* HYDROLOGIC ENGINEERING CENTER
*
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
*
* (916) 756-1104
*

```

```

X X XXXXXX XXXX X
X X X X X XX
X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXX XXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1 ID PROJECT NAME
2 ID TECHNICAL DRAINAGE STUDY
3 ID 100-YEAR EXISTING CONDITION
4 ID
5 ID RETURN PERIOD ----- 10- AND 100-YEAR
6 ID DISTRIBUTION ----- 6-HOUR SDN3
7 ID PROJECT NO. ----- MGL1101.000
8 ID FILENAME ----- EXISTING.H1
9 ID DATE ----- SEPTEMBER 2011
10 ID MODELED BY ----- SLATER HANIFAN GROUP
11 ID
12 ID SIX HOUR DEPTH-AREA REDUCTION FACTORS
13 ID DRAINAGE AREA (MI^2) DARF
14 ID 100-YR 0.990
15 ID 10-YR 0.570
16 ID
17 IT 5 0 0 300
18 IO 5 0 0
19 IN 5 0 0
20 JR PREC 0.990 0
*
21 KK DEC4
22 BA .0034
23 PB 2.77
24 PC 0 0.020 0.057 0.070 0.087 0.108 0.124 0.130 0.130 0.130
25 PC 0.130 0.130 0.130 0.133 0.140 0.142 0.148 0.158 0.172 0.181
26 PC 0.190 0.197 0.199 0.200 0.201 0.204 0.214 0.229 0.241 0.249
27 PC 0.251 0.256 0.270 0.278 0.281 0.283 0.295 0.322 0.352 0.409
28 PC 0.499 0.590 0.710 0.744 0.781 0.812 0.819 0.835 0.851 0.856
29 PC 0.860 0.868 0.876 0.888 0.910 0.926 0.937 0.950 0.970 0.976
30 PC 0.982 0.985 0.987 0.989 0.990 0.993 0.993 0.994 0.995 0.998
31 PC 0.998 0.999 1.000
32 LS 0 98.0
33 UD 0.136
*
34 KK DEC3
35 BA .0012
36 LS 0 98.0
37 UD 0.100
*
38 KK CP.E1
39 KM COMBINATION POINT AT INTERSECTION DECATUR & TROPICAL
40 HC 2
*

```

41 KK 005
42 BA .0024
43 LS 0 98.0
44 UD 0.100
*

HEC-1 INPUT

PAGE 2

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

45 KK NNS
46 KM REFERENCE FROM CNLV NN STUDY BASIN (DANN3A4)
47 BA .50
48 QI 0 0 0 0 0 0 0 0 0 0
49 QI 0 0 0 0 0 0 0 0 0 0
50 QI 0 0 0 1 1 1 0 0 1 1
51 QI 1 1 1 1 1 1 1 1 1 1
52 QI 1 1 5 45 89 121 151 186 219 223
53 QI 193 151 110 73 43 24 12 4 1 1
54 QI 1 1 1 1 1 1 1 1 1 1
55 QI 1 1 1 1 1 1 1 1 1 1
56 QI 1 0 0 0 0 0 0 0 0 0
57 QI 0 0 0 0 0 0 0 0 0 0
*

58 KK CP.E2
59 KM COMBINATION POINT EAST OF C-STORE IN TROPICAL
60 HC 2
*

61 KK TROP1
62 BA .0032
63 LS 0 98.0
64 UD 0.139
*

65 KK ON1E
66 BA .0024
67 LS 0 83.3
68 UD 0.100
*

69 KK ON2E
70 BA .0152
71 LS 0 83.3
72 UD 0.212
*

73 KK CP.E3
74 KM COMBINATION POINT JUST W OF CENT PKWY IN TROPICAL
75 HC 4
*

76 KK RH.5D
77 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
78 BA .0032
79 LS 0 91.0
80 UD 0.098
*

HEC-1 INPUT

PAGE 3

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

81 KK RH.6D
82 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
83 BA .0050
84 LS 0 91.0
85 UD 0.107
*

86 KK CP.D6
87 KM COMBINATION POINT AT INTERSECTION TWILIGHT
88 KM COMBINATION POINT REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
89 HC 2
*

90 KK RH.4D
91 BA .0005
92 LS 0 91.0
93 UD 0.069
*

94 KK CENT2
95 KM BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
96 BA .0026
97 LS 0 98.0
98 UD 0.082
*

99 KK CENT4
100 BA .0002
101 LS 0 98.0
102 UD 0.100

```

      *
103      KK  CP.D7
104      KM  COMBINATION POINT NORTH OF INTERSECTION OF CENT PKWY IN TROPICAL
105      HC    4
      *

106      KK  CP.E5
107      KM  COMBINATION POINT AT INTERSECTION OF CENT PKWY IN TROPICAL
108      HC    2
      *

109      KK  OF.2E
110      KM  OFFSITE BASIN REFERENCED FROM TWILIGHT AT RIVERWALK RANCH
111      BA  .0135
112      LS    0    83.4
113      UD  0.166
      *

```

HEC-1 INPUT

PAGE 4

1

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

114      KK  RIC1
115      BA  .0014
116      LS    0    98.0
117      UD  0.100
      *

118      KK  CP.E8
119      KM  COMBINATION POINT IN RICE
120      HC    2
      *
121      ZZ

```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE      (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.      (.) CONNECTOR      (<---) RETURN OF DIVERTED OR PUMPED FLOW

21      DEC4
      .
34      .      DEC3
      .
38      CP.E1.....
      .
41      .      005
      .
45      .      NNS
      .
58      .      CP.E2.....
      .
61      .      TROP1
      .
65      .      .      ON1E
      .
69      .      .      .      ON2E
      .
73      .      CP.E3.....
      .
76      .      .      RH.5D
      .
81      .      .      .      RH.6D
      .
86      .      .      CP.D6.....
      .
90      .      .      .      RH.4D
      .
94      .      .      .      .      CENT2
      .
99      .      .      .      .      .      CENT4
      .
103     .      .      .      CP.D7.....
      .
106     .      .      CP.E5.....
      .

```

109 . . . OF.2E
 114 . . . RIC1
 118 . . . CP.E8.....

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

 *
 * FLOOD HYDROGRAPH PACKAGE (HEC-1) *
 * JUN 1998 *
 * VERSION 4.1 *
 *
 * RUN DATE 09DEC11 TIME 13:21:51 *
 *
 *

*
 * U.S. ARMY CORPS OF ENGINEERS
 * HYDROLOGIC ENGINEERING CENTER
 * 609 SECOND STREET
 * DAVIS, CALIFORNIA 95616
 * (916) 756-1104
 *

PROJECT NAME
 TECHNICAL DRAINAGE STUDY
 100-YEAR EXISTING CONDITION

 RETURN PERIOD ----- 10- AND 100-YEAR
 DISTRIBUTION ----- 6-HOUR SDN3
 PROJECT NO. ----- MGL1101.000
 FILENAME ----- EXISTING.H1
 DATE ----- SEPTEMBER 2011
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SIX HOUR DEPTH-AREA REDUCTION FACTORS
 DRAINAGE AREA (MI^2) DARF
 100-YR 0.990
 10-YR 0.570

18 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

 IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK

 COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 24.92 HOURS

 ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

 JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

 JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .99

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	
				.99	
HYDROGRAPH AT	DEC4	.00	1	FLOW	6.
+				TIME	3.58

HYDROGRAPH AT	DEC3	.00	1	FLOW	2.
+				TIME	3.50
2 COMBINED AT	CP.E1	.00	1	FLOW	8.
+				TIME	3.58
HYDROGRAPH AT	005	.00	1	FLOW	5.
+				TIME	3.50
HYDROGRAPH AT	NNS	.50	1	FLOW	223.
+				TIME	4.08
2 COMBINED AT	CP.E2	.50	1	FLOW	224.
+				TIME	4.08
HYDROGRAPH AT	TROP1	.00	1	FLOW	6.
+				TIME	3.58
HYDROGRAPH AT	ON1E	.00	1	FLOW	3.
+				TIME	3.50
HYDROGRAPH AT	ON2E	.02	1	FLOW	14.
+				TIME	3.67
4 COMBINED AT	CP.E3	.52	1	FLOW	230.
+				TIME	4.08
HYDROGRAPH AT	RH.5D	.00	1	FLOW	5.
+				TIME	3.50
HYDROGRAPH AT	RH.6D	.00	1	FLOW	8.
+				TIME	3.50
2 COMBINED AT	CP.D6	.01	1	FLOW	13.
+				TIME	3.50
HYDROGRAPH AT	RH.4D	.00	1	FLOW	1.
+				TIME	3.50
HYDROGRAPH AT	CENT2	.00	1	FLOW	5.
+				TIME	3.50
HYDROGRAPH AT	CENT4	.00	1	FLOW	0.
+				TIME	3.50
4 COMBINED AT	CP.D7	.01	1	FLOW	20.
+				TIME	3.50
2 COMBINED AT	CP.E5	.53	1	FLOW	233.
+				TIME	4.08
HYDROGRAPH AT	OF.2E	.01	1	FLOW	14.
+				TIME	3.58
HYDROGRAPH AT	RIC1	.00	1	FLOW	3.
+				TIME	3.50
2 COMBINED AT	CP.E8	.01	1	FLOW	17.
+				TIME	3.58

+ 155 surface flow

*** NORMAL END OF HEC-1 ***

Reference Material

Twilight at Riverwalk, SHG

```
*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* RUN DATE 03/15/2005 TIME 15:19:16 *
*****
```

```
*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****
```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

```

::::::::::::::::::::::::::::::::::::
::::::::::::::::::::::::::::::::::::
::: Full Microcomputer Implementation :::
::: by :::
::: Haestad Methods, Inc. :::
::: :::
::::::::::::::::::::::::::::::::::::
::::::::::::::::::::::::::::::::::::

```

37 Brookside Road * Waterbury, Connecticut 06708 * (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1	ID 10-YR ULTIMATE CONDITION - RIVERWALK TWILIGHT
2	IT 5 300
3	IO 5 0
4	KK RT.1D
5	KM
6	KO 22
7	BA .0051
8	PB 1.58
9	PC .000 .020 .057 .070 .087 .108 .124 .130 .130 .130
10	PC .130 .130 .130 .133 .140 .142 .148 .158 .172 .181
11	PC .190 .197 .199 .200 .201 .204 .214 .229 .241 .249
12	PC .251 .256 .270 .278 .281 .283 .295 .322 .352 .409
13	PC .499 .590 .710 .744 .781 .812 .819 .835 .851 .856
14	PC .860 .868 .876 .888 .910 .926 .937 .950 .970 .976
15	PC .982 .985 .987 .989 .990 .993 .993 .994 .995 .998
16	PC .998 .999 1.000
17	LS 95
18	UD .109
19	KK RT.2D
20	KM
21	KO 22
22	BA .0049
23	LS 95
24	UD .110
25	KK CP.D1
26	KM
27	KO 22
28	HC 2
29	KK DI6
30	KM WATER CAPTURED BY DROP INLET 6
31	KO 22
32	DT RDI6 18

33	DI	0	9	18
34	DQ	0	8	11

35	KK	RT.3D		
36	KM			
37	KO			22
38	BA	.0065		
39	LS		95	
40	UD	.1		

41	KK	RT.4D		
42	KM			
43	KO			22
44	BA	.0088		
45	LS		95	
46	UD	.114		

HEC-1 INPUT

PAGE 2

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
------	---

47	KK	CP.D2		
48	KM			
49	KO			22
50	HC	3		

51	KK	RT.5D		
52	KM			
53	KO			22
54	BA	.0126		
55	LS		95	
56	UD	.158		

57	KK	RT.6D		
58	KM			
59	KO			22
60	BA	.002		
61	LS		95	
62	UD	.069		

63	KK	CP.D3		
64	KM			
65	KO			22
66	HC	3		

67	KK	CEN1		
68	KM			
69	KO			22
70	BA	.0050		
71	LS		98	
72	UD	.100		

73	KK	OF.1D		
74	KM			
75	KO			22
76	BA	.0172		
77	LS		94	
78	UD	.137		

79	KK	DEC3		
80	KM			
81	KO			22
82	BA	.0014		
83	LS		98	
84	UD	.073		

85	KK	CP.D5		
86	KM			
87	KO			22
88	HC	3		

HEC-1 INPUT

PAGE 3

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
------	---

89	KK	RH.2P		
90	KM			
91	KO			22
92	BA	.0105		
93	LS		91	
94	UD	.138		

95	KK	CEN2		
96	KM			
97	KO			22
98	BA	.0026		
99	LS		98	
100	UD	.082		

101	KK	CP.D4		
102	KM			
103	KO			22
104	HC	2		

105	KK	CP.D6		
106	KM			
107	KO			22
108	HC	2		
109	KK	RT.7D		
110	KM			
111	KO			22
112	BA	.0035		
113	LS		95	
114	UD	.085		
115	KK	TROP1		
116	KM			
117	KO			22
118	BA	.0053		
119	LS		98	
120	UD	.104		
121	KK	OF.4D		
122	KM			
123	KO			22
124	BA	.0014		
125	LS		96	
126	UD	.082		
127	KK	CP.D7		
128	KM			
129	KO			22
130	HC	4		

HEC-1 INPUT

PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

131	KK	RDI6		
132	KM	RUNOFF CAPUTRED BY DI6 ADDED BACK INTO TOTAL CAPTURED		
133	KO			22
134	DR	RDI6		
135	KK	CP.D8		
136	KM			
137	KO			22
138	HC	3		
139	KK	DEC4		
140	KM			
141	KO			22
142	BA	.0033		
143	LS		98	
144	UD	.05		
145	KK	RDEC4		
146	KM	ROUTE DEC4 TO CENTENNIAL PKWY		
147	KO			22
148	RK	1400 .005 .015	TRAP 49	2
149	KK	RMRH		
150	KM	RICE - MONTGOMERY - RANCH HOUSE		
151	KO			22
152	BA	.0054		
153	LS		98	
154	UD	.139		
155	KK	OF.2D		
156	KM			
157	KO			22
158	BA	.0135		
159	LS		94	
160	UD	.132		
161	KK	OF.3D		
162	KM			
163	KO			22
164	BA	.0188		
165	LS		95	
166	UD	.129		
167	KK	RH.1P		
168	KM			
169	KO			22
170	BA	.0108		
171	LS		92	
172	UD	.140		

HEC-1 INPUT

PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

173	KK	CEN3		
174	KM			
175	KO			22

22

```
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* MAY 1991
* VERSION 4.0.1E
*
* RUN DATE 03/15/2005 TIME 15:19:16
*
*****
```

*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

[illegible]

	RT.5D	11.	3.58	1.	0.	0.	0.01
HYDROGRAPH AT	RT.6D	2.	3.50	0.	0.	0.	0.00
3 COMBINED AT	CP.D3	27.	3.58	4.	1.	1.	0.04
HYDROGRAPH AT	CEN1	6.	3.50	1.	0.	0.	0.00
HYDROGRAPH AT	OF.1D	15.	3.58	2.	0.	0.	0.02
HYDROGRAPH AT	DEC3	2.	3.50	0.	0.	0.	0.00
3 COMBINED AT	CP.D5	21.	3.58	3.	1.	1.	0.02
HYDROGRAPH AT	RH.2P	7.	3.58	1.	0.	0.	0.01
HYDROGRAPH AT	CEN2	3.	3.50	0.	0.	0.	0.00
2 COMBINED AT	CP.D4	14.	3.58	1.	0.	0.	0.01
2 COMBINED AT	CP.D6	31.	3.58	4.	1.	1.	0.04
HYDROGRAPH AT	RT.7D	4.	3.50	0.	0.	0.	0.00
HYDROGRAPH AT	TROP1	6.	3.50	1.	0.	0.	0.01
HYDROGRAPH AT	OF.4D	2.	3.50	0.	0.	0.	0.00
4 COMBINED AT	CP.D7	41.	3.50	5.	1.	1.	0.05
HYDROGRAPH AT	RDI6	8.	3.50	1.	0.	0.	0.00
3 COMBINED AT	CP.D8	76.	3.50	10.	3.	2.	0.09
HYDROGRAPH AT	DEC4	4.	3.50	0.	0.	0.	0.00
ROUTED TO	RDEC4	4.	3.58	0.	0.	0.	0.00
HYDROGRAPH AT	RMRH	6.	3.58	1.	0.	0.	0.01
HYDROGRAPH AT	OF.2D	12.	3.58	1.	0.	0.	0.01
HYDROGRAPH AT	OF.3D	17.	3.58	2.	1.	1.	0.02
HYDROGRAPH AT	RH.1P	8.	3.58	1.	0.	0.	0.01
HYDROGRAPH AT	CEN3	4.	3.50	0.	0.	0.	0.00
6 COMBINED AT	CP.D9	49.	3.58	6.	2.	2.	0.06
2 COMBINED AT	DUMMY	124.	3.58	17.	4.	4.	0.14

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	INTERPOLATED TO COMPUTATION INTERVAL			
						DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)
RDEC4	MANE	3.74	4.11	218.20	1.42	5.00	3.70	215.00	1.42

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2392E+00 EXCESS=0.0000E+00 OUTFLOW=0.2494E+00 BASIN STORAGE=0.2241E-04 PERCENT ERROR= -4.3

*** NORMAL END OF HEC-1 ***

```
*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* RUN DATE 03/18/2005 TIME 13:53:35 *
*****
```

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*****
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* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****
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X   X   XXXXXXX   XXXXX   X
X   X   X   X   X   X   XX
X   X   X   X   X   X   X
XXXXXXX XXXX   X   XXXXX   X
X   X   X   X   X   X   X
X   X   X   X   X   X   X
X   X   XXXXXXX   XXXXX   XXX

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::::::::::::::::::::::::::::::::::::
::::::::::::::::::::::::::::::::::::
::: Full Microcomputer Implementation :::
::: by :::
::: Haestad Methods, Inc. :::
::: :::
::::::::::::::::::::::::::::::::::::
::::::::::::::::::::::::::::::::::::

```

37 Brookside Road * Waterbury, Connecticut 06708 * (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1	ID 100-YR ULTIMATE CONDITION - RIVERWALK TWILIGHT
2	IT 5 300
3	IO 5 0
4	KK RT.1D
5	KM
6	KO 22
7	BA .0051
8	FB 2.77
9	PC .000 .020 .057 .070 .087 .108 .124 .130 .130 .130
10	PC .130 .130 .130 .133 .140 .142 .148 .158 .172 .181
11	PC .190 .197 .199 .200 .201 .204 .214 .229 .241 .249
12	PC .251 .256 .270 .278 .281 .283 .295 .322 .352 .409
13	PC .499 .590 .710 .744 .781 .812 .819 .835 .851 .856
14	PC .860 .868 .876 .888 .910 .926 .937 .950 .970 .976
15	PC .982 .985 .987 .989 .990 .993 .993 .994 .995 .998
16	PC .998 .999 1.000
17	LS 95
18	UD .109
19	KK RT.2D
20	KM
21	KO 22
22	BA .0049
23	LS 95
24	UD .110
25	KK CP.D1
26	KM
27	KO 22
28	HC 2
29	KK DI6
30	KM WATER CAPTURED BY DROP INLET 6
31	KO 22
32	DT RDI6 18

41	KK	RT.4D		
42	KM			
43	KO			22
44	BA	.0088		
45	LS		95	
46	UD	.114		

PAGE 2

85	KK	NNS									
86	KM	REFERENCE FROM CNLV NN STUDY BASIN (DANN3A4)									
87	KO	22									
88	BA	.50									
89	QI	0	0	0	0	0	0	0	0	0	0
90	QI	0	0	0	0	0	0	0	0	0	0
91	QI	0	0	0	1	1	1	0	0	1	1
92	QI	1	1	1	1	1	1	1	1	1	1
93	QI	1	1	5	45	89	121	151	186	219	223

PAGE 3

103	KK	RH.2P	
104	KM		
105	KO		22

106	BA	.0105	
107	LS		91
108	UD	.138	
109	KK	CEN2	
110	KM		
111	KO		22
112	BA	.0026	
113	LS		98
114	UD	.082	
115	KK	CP.D4	
116	KM		
117	KO		22
118	HC	2	
119	KK	CP.D6	
120	KM		
121	KO		22
122	HC	2	
123	KK	RT.7D	
124	KM		
125	KO		22
126	BA	.0035	
127	LS		95
128	UD	.085	
129	KK	TROP1	
130	KM		
131	KO		22
132	BA	.0053	
133	LS		98
134	UD	.104	
135	KK	OF.4D	
136	KM		
137	KO		22
138	BA	.0014	
139	LS		96
140	UD	.082	

HEC-1 INPUT

PAGE 4

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
141	KK CP.D7
142	KM
143	KO 22
144	HC 4
145	KK RDI6
146	KM RUNOFF CAPUTRED BY DI6 ADDED BACK INTO TOTAL CAPTURED
147	KO 22
148	DR RDI6
149	KK CP.D8
150	KM
151	KO 22
152	HC 3
153	KK DEC4
154	KM
155	KO 22
156	BA .0033
157	LS 98
158	UD .05
159	KK RDEC4
160	KM ROUTE DEC4 TO CENTENNIAL PKWY
161	KO 22
162	RK 1400 .005 .015 TRAP 49 2
163	KK RMRH
164	KM RICE - MONTGOMERY - RANCH HOUSE
165	KO 22
166	BA .0054
167	LS 98
168	UD .139
169	KK OF.2D
170	KM
171	KO 22
172	BA .0135
173	LS 94
174	UD .132
175	KK OF.3D
176	KM
177	KO 22
178	BA .0188
179	LS 95
180	UD .129

22

PAGE 5

22

22

22

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*****
*
*   FLOOD HYDROGRAPH PACKAGE   (HEC-1)
*           MAY   1991
*           VERSION 4.0.1E
*
*   RUN DATE 03/18/2005   TIME 13:53:35
*
*****
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* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*

3	IO	OUTPUT CONTROL VARIABLES	
		IPRNT	5 PRINT CONTROL
		IPILOT	0 PLOT CONTROL
		QSCAL	0. HYDROGRAPH PLOT SCALE
IT		HYDROGRAPH TIME DATA	
		NMIN	5 MINUTES IN COMPUTATION INTERVAL
		IDATE	1 0 STARTING DATE
		ITIME	0000 STARTING TIME
		NQ	300 NUMBER OF HYDROGRAPH ORDINATES
		NDDATE	2 0 ENDING DATE
		NDTIME	0055 ENDING TIME
		ICENT	19 CENTURY MARK
		COMPUTATION INTERVAL	0.08 HOURS
		TOTAL TIME BASE	24.92 HOURS

ENGLISH UNITS	
DRAINAGE AREA	SQUARE MILES
PRECIPITATION DEPTH	INCHES
LENGTH, ELEVATION	FEET
FLOW	CUBIC FEET PER SECOND
STORAGE VOLUME	ACRE-FEET
SURFACE AREA	ACRES
TEMPERATURE	DEGREES FAHRENHEIT

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

[illegible]

	RT.3D	12.	3.50	2.	0.	0.	0.01
HYDROGRAPH AT	RT.4D	16.	3.50	2.	1.	1.	0.01
3 COMBINED AT	CP.D2	35.	3.50	4.	1.	1.	0.03
HYDROGRAPH AT	RT.5D	21.	3.58	3.	1.	1.	0.01
HYDROGRAPH AT	RT.6D	4.	3.50	0.	0.	0.	0.00
3 COMBINED AT	CP.D3	58.	3.50	8.	2.	2.	0.04
HYDROGRAPH AT	CEN1	10.	3.50	1.	0.	0.	0.00
HYDROGRAPH AT	OF.1D	21.	3.58	3.	1.	1.	0.02
HYDROGRAPH AT	DEC3	3.	3.50	0.	0.	0.	0.00
HYDROGRAPH AT	NNS	223.	4.08	23.	6.	6.	0.50
4 COMBINED AT	CP.D5	229.	4.08	28.	7.	7.	0.52
HYDROGRAPH AT	RH.2P	16.	3.58	2.	1.	1.	0.01
HYDROGRAPH AT	CEN2	5.	3.50	1.	0.	0.	0.00
2 COMBINED AT	CP.D4	21.	3.58	3.	1.	1.	0.01
2 COMBINED AT	CP.D6	233.	4.08	30.	8.	7.	0.54
HYDROGRAPH AT	RT.7D	7.	3.50	1.	0.	0.	0.00
HYDROGRAPH AT	TROP1	10.	3.50	1.	0.	0.	0.01
HYDROGRAPH AT	OF.4D	3.	3.50	0.	0.	0.	0.00
4 COMBINED AT	CP.D7	236.	4.08	33.	8.	8.	0.55
HYDROGRAPH AT	RDI6	11.	3.50	2.	0.	0.	0.00
3 COMBINED AT	CP.D8	250.	4.00	43.	11.	10.	0.59
HYDROGRAPH AT	DEC4	8.	3.50	1.	0.	0.	0.00
ROUTED TO	RDEC4	7.	3.58	1.	0.	0.	0.00
HYDROGRAPH AT	RMRH	10.	3.58	1.	0.	0.	0.01
HYDROGRAPH AT	OF.2D	23.	3.58	3.	1.	1.	0.01
HYDROGRAPH AT	OF.3D	33.	3.58	4.	1.	1.	0.02
HYDROGRAPH AT	RH.1P	17.	3.58	2.	1.	1.	0.01
HYDROGRAPH AT	CEN3	8.	3.50	1.	0.	0.	0.00
6 COMBINED AT	CP.D9	95.	3.58	13.	3.	3.	0.06
2 COMBINED AT	DUMMY	279.	3.58	56.	14.	13.	0.64

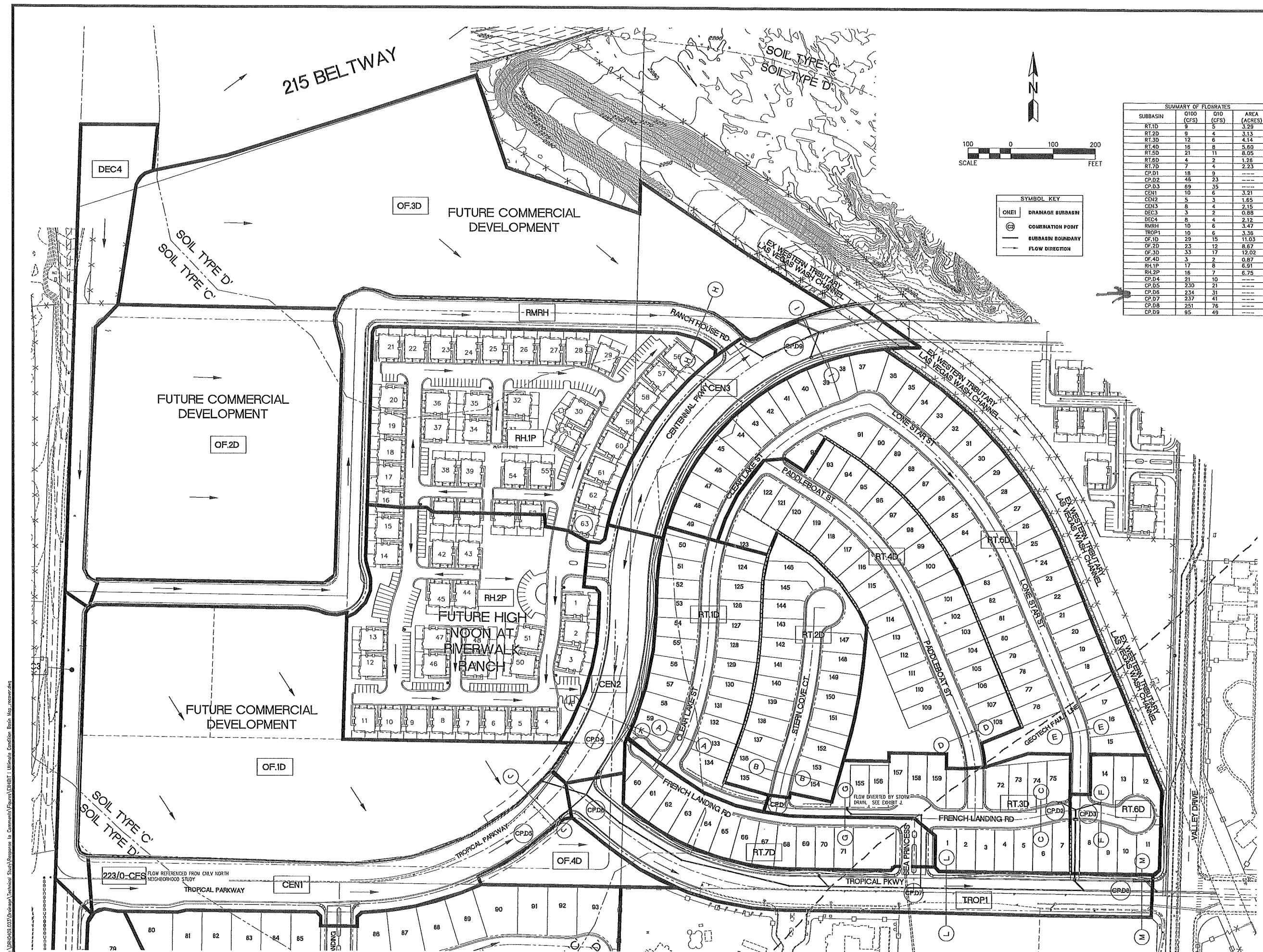
SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO	

				PEAK		PEAK		
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)
RDEC4	MANE	3.05	7.32	214.88	2.60	5.00	7.29	215.00
								2.61

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4469E+00 EXCESS=0.0000E+00 OUTFLOW=0.4577E+00 BASIN STORAGE=0.2321E-04 PERCENT ERROR= -2.4

*** NORMAL END OF HEC-1 ***



SUMMARY OF FLOWRATES			
SUBBASIN	Q100 (CFS)	Q10 (CFS)	AREA (ACRES)
RT1D	9	5	3.39
RT2D	9	4	3.13
RT3D	12	6	4.14
RT4D	16	8	5.60
RT5D	21	11	8.05
RT6D	4	2	1.28
RT7D	7	4	2.23
CP.D1	18	9	6.44
CP.D2	46	23	16.88
CP.D3	69	35	25.99
CEN1	6	6	3.21
CEN2	5	3	1.65
CEN3	8	4	2.15
DEC3	3	2	0.88
DEC4	8	4	2.12
RURH	10	6	3.47
TRGP1	10	6	3.36
OF1D	29	15	11.03
OF2D	23	12	8.67
OF3D	33	17	12.02
OF4D	3	2	0.87
RH.1P	17	8	6.01
RH.2P	16	7	6.75
CP.D4	21	10	7.44
CP.D5	230	21	84.44
CP.D6	234	31	88.44
CP.D7	237	41	114.44
CP.D8	251	76	124.44
CP.D9	95	49	34.44

SYMBOL KEY

ONE1	DRAINAGE SUBBASIN
C2	COLLECTION POINT
————	SUBBASIN BOUNDARY
————→	FLOW DIRECTION

S-I-G SLATER
HANIFAN
GROUP
CONSULTING ENGINEERS & PLANNERS
PHONE (702) 284-5300 FAX (702) 284-5399
S. ARVILLE STREET #216, LAS VEGAS, NV 89118

DRAINAGE BASIN MAP - ULTIMATE CONDITIONS

DR HORTON

DATE: 03/18/05

DRAFTER: JDS

DESIGNER: JDS

CHECKED: MJF

PROJECT NO.
DRH0409.003

EXHIBIT I

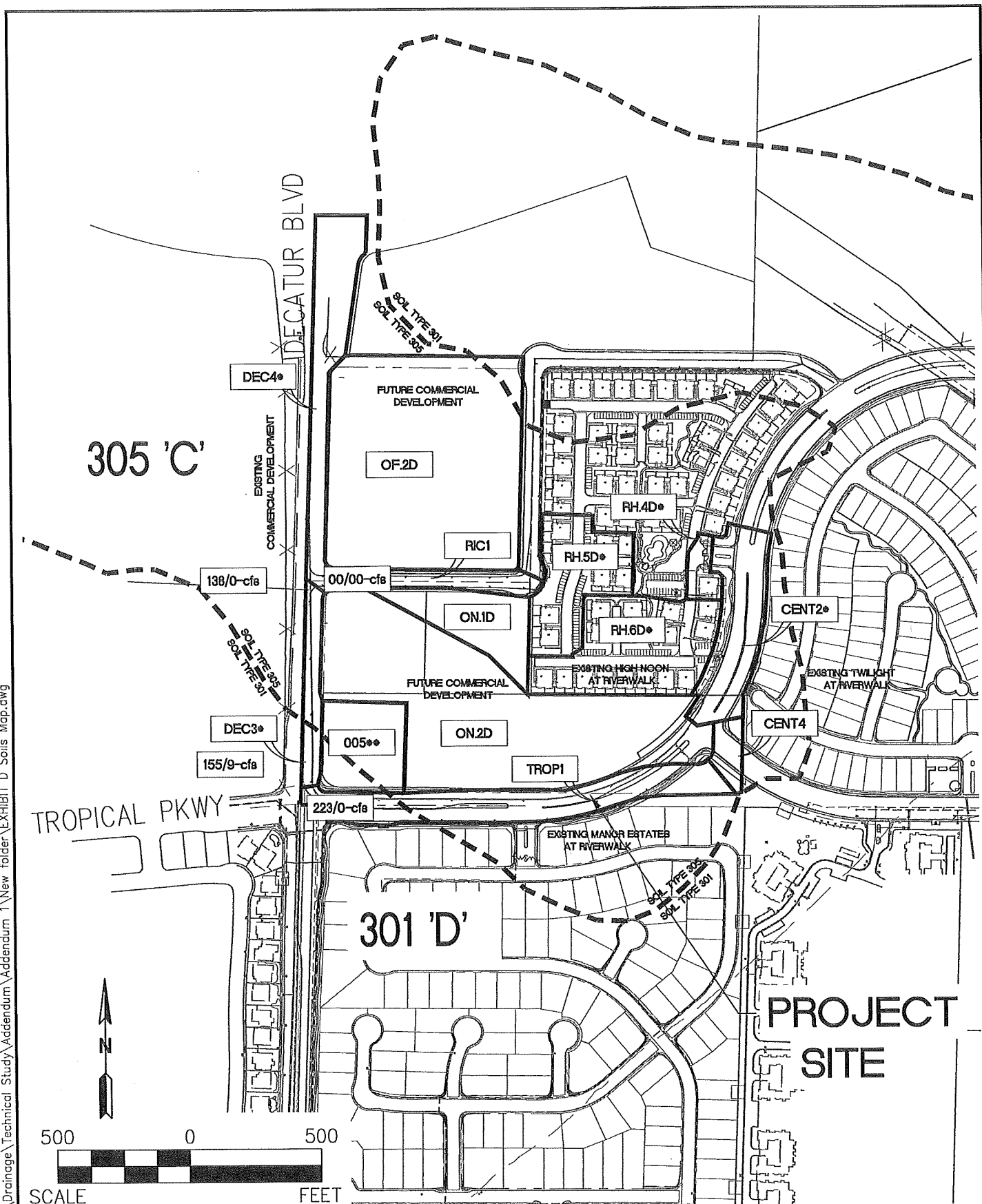
SHEET 1 OF 1

APPENDIX D

Response to Comment 8

Soils Map

File: J:\MGL1101-000\Drainage\Technical Study\Addendum 1\New folder\EXHIBIT D Soils Map.dwg



S-I-G SLATER
HANIFAN
GROUP
CONSULTING ENGINEERS & PLANNERS

5740 S. ARVILLE STREET #216, LAS VEGAS, NV 89118
PHONE (702) 284-5300 FAX (702) 284-5399

SOILS MAP
**CENTENNIAL/TROPICAL
REALIGNMENT**

DATE: 12/06/11

DRAFTER: RFF

DESIGNER: RFF

CHECKED: RFF

PROJECT NO.

MGL1101.000

EXHIBIT D

SHEET 1 OF 1

APPENDIX E

Response to Comment 9

Revised Soil and CN Table

Soil & Curve Number Computation

Project Name: Tropical Pkwy

Date: 9/22/2011

File Name: MGL1101-000

By: RFF

Data:

Reference:

Soil Type & Description	A	B	C	D
301 Las Vegas gravelly fine sandy loam, 2 to 4 percent slopes	0%	5%	0%	95%
305 Las Vegas-Destazo complex, 0 to 2 percent slopes	5%	30%	5%	60%

Exhibit G
SCS Soil Data

Land Use	A	B	C	D
Desert Shrub (poor)	63	77	85	88
Commercial	89	92	94	95
Roadway	98	98	98	98

BASIN ID	SOIL TYPE	SUBAREA PERCENT	LAND USE	HYDROLOGIC SOIL GROUP				LAND USE CN				SUBAREA ACRES	CALCULATED CN
				A	B	C	D	A	B	C	D		
OF.2E	301	3.5%	Desert Shrub (poor)	0%	5%	0%	95%	63	77	85	88	0.30	3.03
	305	96.5%	Desert Shrub (poor)	5%	30%	5%	60%	63	77	85	88	8.35	80.41
TOTAL PERCENT		100.0%						TOTAL AREA				8.65	83.44

BASIN ID	SOIL TYPE	SUBAREA PERCENT	LAND USE	HYDROLOGIC SOIL GROUP				LAND USE CN				SUBAREA ACRES	CALCULATED CN
				A	B	C	D	A	B	C	D		
ON.1E	305	100.0%	Desert Shrub (poor)	5%	30%	5%	60%	63	77	85	88	1.54	83.30
TOTAL PERCENT		100.0%						TOTAL AREA				1.54	83.30

BASIN ID	SOIL TYPE	SUBAREA PERCENT	LAND USE	HYDROLOGIC SOIL GROUP				LAND USE CN				SUBAREA ACRES	CALCULATED CN
				A	B	C	D	A	B	C	D		
ON.2E	305	100.0%	Desert Shrub (poor)	5%	30%	5%	60%	63	77	85	88	10.00	83.30
TOTAL PERCENT		100.0%						TOTAL AREA				10.00	83.30

BASIN ID	SOIL TYPE	SUBAREA PERCENT	LAND USE	HYDROLOGIC SOIL GROUP				LAND USE CN				SUBAREA ACRES	CALCULATED CN
				A	B	C	D	A	B	C	D		
DEC.3	305	30.3%	Roadway	5%	30%	5%	60%	98	98	98	98	0.23	29.66
	301	69.7%	Roadway	0%	5%	0%	95%	98	98	98	98	0.53	68.34
TOTAL PERCENT		30.3%						TOTAL AREA				0.76	98.00

BASIN ID	SOIL TYPE	SUBAREA PERCENT	LAND USE	HYDROLOGIC SOIL GROUP				LAND USE CN				SUBAREA ACRES	CALCULATED CN
				A	B	C	D	A	B	C	D		
TROP.1	301	28.8%	Roadway	0%	5%	0%	95%	98	98	98	98	0.59	28.20
	305	71.2%	Roadway	5%	30%	5%	60%	98	98	98	98	1.46	69.80
TOTAL PERCENT		100.0%						TOTAL AREA				2.05	98.00

BASIN ID	SOIL TYPE	SUBAREA PERCENT	LAND USE	HYDROLOGIC SOIL GROUP				LAND USE CN				SUBAREA ACRES	CALCULATED CN
				A	B	C	D	A	B	C	D		
CENT.2	305	100.0%	Roadway	5%	30%	5%	60%	98	98	98	98	0.14	98.00
TOTAL PERCENT		100.0%						TOTAL AREA				0.14	98.00

BASIN ID	SOIL TYPE	SUBAREA PERCENT	LAND USE	HYDROLOGIC SOIL GROUP				LAND USE CN				SUBAREA ACRES	CALCULATED CN
				A	B	C	D	A	B	C	D		
RICE-1	305	100.0%	Roadway	5%	30%	5%	60%	98	98	98	98	0.90	98.00
TOTAL PERCENT		100.0%						TOTAL AREA				0.90	98.00

APPENDIX F

Response to Comment 10

Revised FlowMaster Calcs

Centennial Pkwy Q10 Int/Dev Sec E East 1/2

Worksheet for Irregular Channel

Project Description	
Worksheet	Centennial Parkway Q10 Int/Dev Sec E E1/2
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.90 %
Discharge	2.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.013
Water Surface Elevation	67.01 ft
Elevation Range	66.74 to 67.75
Flow Area	1.2 ft ²
Wetted Perimeter	21.43 ft
Top Width	21.15 ft
Actual Depth	0.27 ft
Critical Elevation	67.02 ft
Critical Slope	0.64 %
Velocity	1.61 ft/s
Velocity Head	0.04 ft
Specific Energy	67.05 ft
Froude Number	1.17
Flow Type	Supercritical

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+02.00	0.013
0+02.00	0+38.00	0.016
0+38.00	0+45.00	0.013

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	67.75
0+01.50	67.59
0+02.00	67.59
0+02.00	67.09
0+38.00	66.91
0+39.50	66.74
0+39.50	67.24
0+40.00	67.24
0+45.00	67.34

Dry Lane

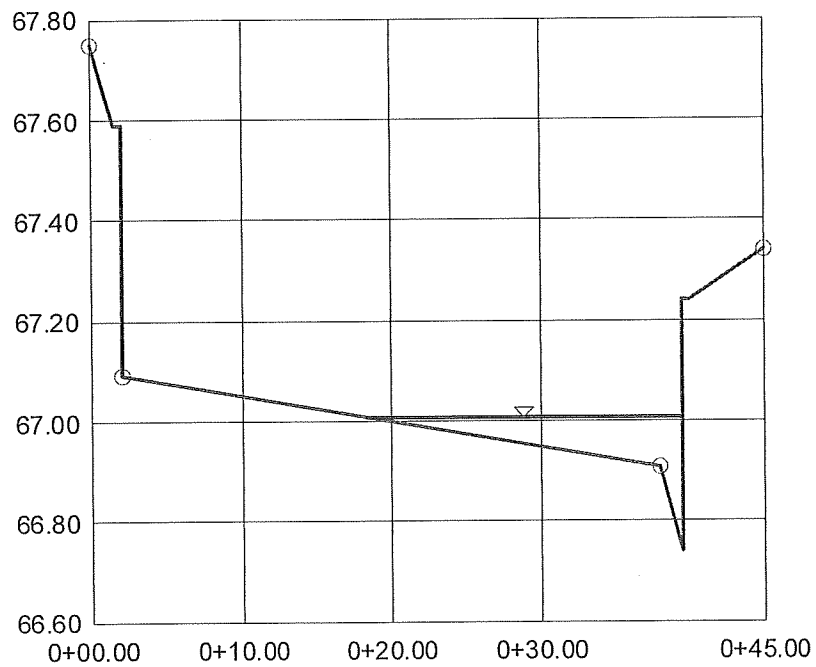
$$\frac{67.09 - 67.01}{0.02} = 4' \times 2$$

All flow goes into
7.5' DI then
dry lane is met

Centennial Pkwy Q10 Int/Dev Sec E **Cross Section for Irregular Channel**

Project Description	
Worksheet	Centennial Parkway Q10 Int/Dev Sec E E1/2
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.013
Channel Slope	0.90 %
Water Surface Elevation	67.01 ft
Elevation Range	66.74 to 67.75
Discharge	2.00 cfs



V:33.3333333
H:1
NTS

Centennial Pkwy Q100 Int/Dev Sec E East 1/2

Worksheet for Irregular Channel

Project Description	
Worksheet	Centennial Parkway Q100 Int/Dev Sec E E1/2
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.90 %
Discharge	4.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.014
Water Surface Elevation	67.05 ft
Elevation Range	66.74 to 67.75
Flow Area	2.2 ft ²
Wetted Perimeter	29.43 ft
Top Width	29.11 ft
Actual Depth	0.31 ft
Critical Elevation	67.06 ft
Critical Slope	0.69 %
Velocity	1.79 ft/s
Velocity Head	0.05 ft
Specific Energy	67.10 ft
Froude Number	1.13
Flow Type	Supercritical

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+02.00	0.013
0+02.00	0+38.00	0.016
0+38.00	0+45.00	0.013

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	67.75
0+01.50	67.59
0+02.00	67.59
0+02.00	67.09
0+38.00	66.91
0+39.50	66.74
0+39.50	67.24
0+40.00	67.24
0+45.00	67.34

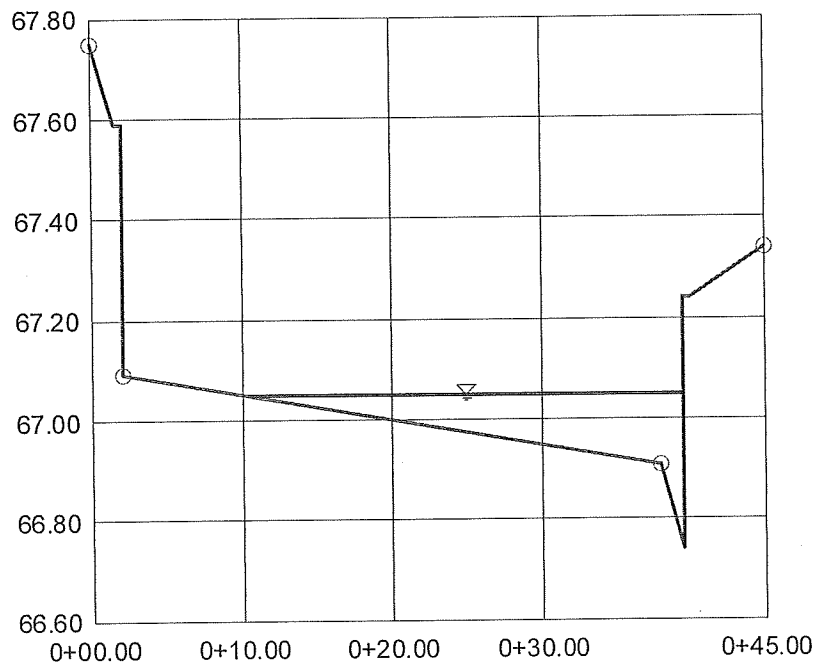
$$V \times \Delta$$

$$1.79 \times 0.31 = 0.55$$

Centennial Pkwy Q100 Int/Dev Sec E **Cross Section for Irregular Channel**

Project Description	
Worksheet	Centennial Parkway Q100 Int/Dev Sec E E1/2
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.014
Channel Slope	0.90 %
Water Surface Elevation	67.05 ft
Elevation Range	66.74 to 67.75
Discharge	4.00 cfs



V:33.3333333
H:1
NTS

Centennial Pkwy Q10 Int/Dev Sec E West1/2

Worksheet for Irregular Channel

Project Description	
Worksheet	Centennial Parkway Q10 Int/Dev Sec WE1/2
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.70 %
Discharge	8.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.015
Water Surface Elevation	66.55 ft
Elevation Range	66.13 to 67.45
Flow Area	3.6 ft ²
Wetted Perimeter	26.44 ft
Top Width	26.00 ft
Actual Depth	0.42 ft
Critical Elevation	66.56 ft
Critical Slope	0.62 %
Velocity	2.23 ft/s
Velocity Head	0.08 ft
Specific Energy	66.63 ft
Froude Number	1.06
Flow Type	Supercritical

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+02.00	0.013
0+02.00	0+38.00	0.016
0+38.00	0+40.00	0.013
0+40.00	0+53.20	0.022

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	67.45
0+01.50	67.17
0+02.00	67.17
0+02.00	66.67
0+38.00	66.30
0+39.50	66.13
0+39.50	66.63
0+40.00	66.63
0+53.20	66.89

Dry Lane

$$\frac{66.67 - 66.55}{0.02} = 6'$$

All Flow is captured by
15-ft DI in West Half
of Cent sta: 11+08.
So Dry lane = 36'

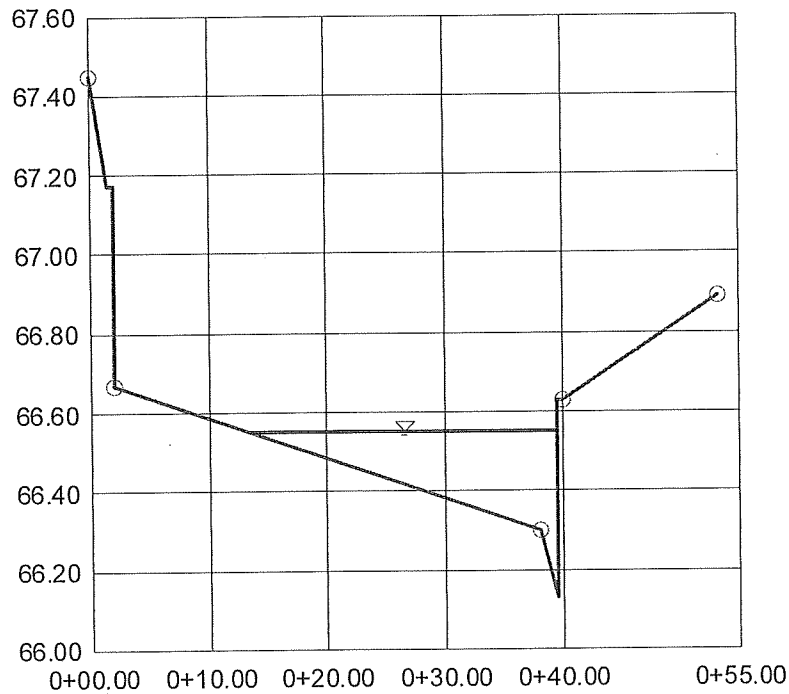
Centennial Pkwy Q10 Int/Dev Sec E West 1/2 **Cross Section for Irregular Channel**

Project Description

Worksheet	Centennial Parkway Q10 Int/Dev Sec W E1/2
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data

Mannings Coefficient	0.015
Channel Slope	0.70 %
Water Surface Elevation	66.55 ft
Elevation Range	66.13 to 67.45
Discharge	8.00 cfs



V:33.3333333
H:1
NTS

Centennial Pkwy Q100 Int/Dev Sec E West1/2

Worksheet for Irregular Channel

Project Description	
Worksheet	Centennial Parkway Q100 Int/Dev Sec W E1/2
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.70 %
Discharge	17.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.015
Water Surface Elevation	66.65 ft
Elevation Range	66.13 to 67.45
Flow Area	6.6 ft ²
Wetted Perimeter	37.47 ft
Top Width	36.95 ft
Actual Depth	0.52 ft
Critical Elevation	66.66 ft
Critical Slope	0.60 %
Velocity	2.57 ft/s
Velocity Head	0.10 ft
Specific Energy	66.75 ft
Froude Number	1.07
Flow Type	Supercritical

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+02.00	0.013
0+02.00	0+38.00	0.016
0+38.00	0+40.00	0.013
0+40.00	0+53.20	0.022

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	67.45
0+01.50	67.17
0+02.00	67.17
0+02.00	66.67
0+38.00	66.30
0+39.50	66.13
0+39.50	66.63
0+40.00	66.63
0+53.20	66.89

$V \times \Delta$

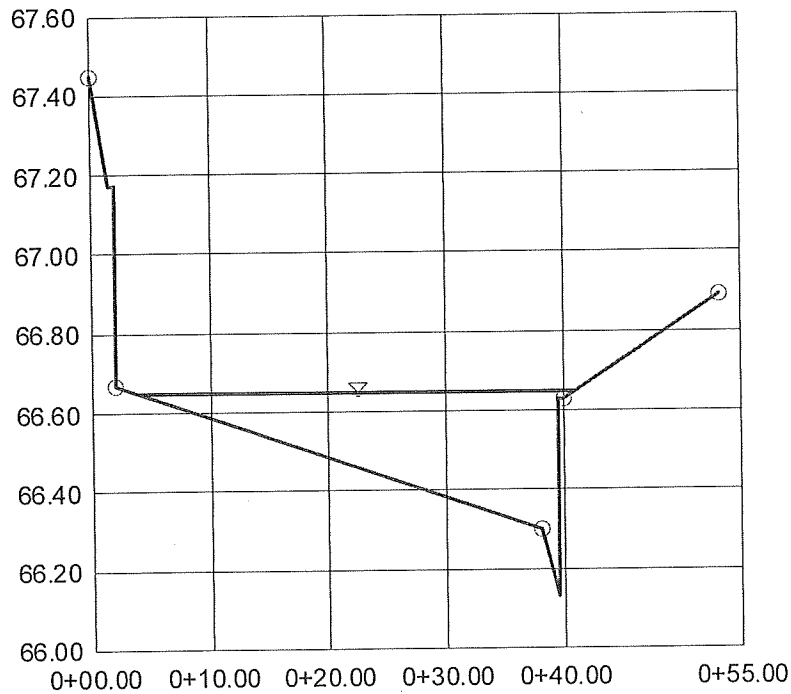
$2.57 \times 0.52 = 1.3$

Z
OK

Centennial Pkwy Q100 Int/Dev Sec E West 1/2 **Cross Section for Irregular Channel**

Project Description	
Worksheet	Centennial Parkway Q100 Int/Dev Sec W E1/2
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.015
Channel Slope	0.70 %
Water Surface Elevation	66.65 ft
Elevation Range	66.13 to 67.45
Discharge	17.00 cfs



V:33.333333
H:1
NTS

Tropical Pkwy Q10 EX Sec A

Worksheet for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec A Q10 EX
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.70 %
Discharge	3.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.013
Water Surface Elevation	71.62 ft
Elevation Range	71.34 to 73.95
Flow Area	1.3 ft ²
Wetted Perimeter	10.46 ft
Top Width	10.18 ft
Actual Depth	0.28 ft
Critical Elevation	71.64 ft
Critical Slope	0.50 %
Velocity	2.35 ft/s
Velocity Head	0.09 ft
Specific Energy	71.71 ft
Froude Number	1.17
Flow Type	Supercritical

Dry Lane

$$\frac{72.40 - 71.62}{0.02} = 39' \checkmark \text{ OK}$$

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+13.00	0.034
0+13.00	0+26.00	0.016
0+26.00	0+39.50	0.013
0+39.50	0+40.00	0.016
0+40.00	0+83.00	0.013
0+83.00	0+95.00	0.022

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	73.95
0+08.00	71.72
0+13.00	72.09
0+26.00	72.44
0+26.00	72.78
0+26.50	72.78
0+39.50	72.78
0+40.00	72.78

Tropical Pkwy Q10 EX Sec A **Worksheet for Irregular Channel**

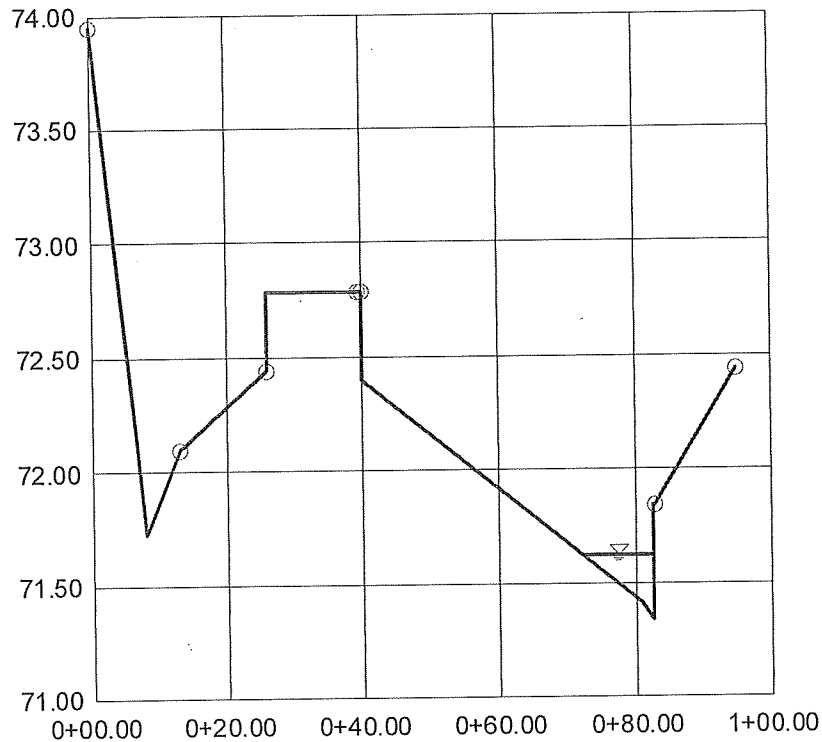
Natural Channel Points	
Station (ft)	Elevation (ft)
0+40.00	72.40
0+81.00	71.41
0+82.50	71.34
0+82.50	71.84
0+83.00	71.84
0+95.00	72.44

Tropical Pkwy Q10 Ex Sec A

Cross Section for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec A Q10 EX
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.013
Channel Slope	0.70 %
Water Surface Elevation	71.62 ft
Elevation Range	71.34 to 73.95
Discharge	3.00 cfs



V:33.3333333
H:1
NTS

Tropical Pkwy Q100 EX Sec A

Worksheet for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec A Q100 EX
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.70 %
Discharge	224.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.014
Water Surface Elevation	72.52 ft
Elevation Range	71.34 to 73.95
Flow Area	39.3 ft ²
Wetted Perimeter	76.80 ft
Top Width	75.87 ft
Actual Depth	1.18 ft
Critical Elevation	72.65 ft
Critical Slope	0.34 %
Velocity	5.70 ft/s
Velocity Head	0.50 ft
Specific Energy	73.02 ft
Froude Number	1.40
Flow Type	Supercritical

$$\frac{V \times D}{5.70 \times 1.18 = 6.7}$$

Calculation Messages:
 Water elevation exceeds lowest end station by 0.79194188e-1 ft.
 Flow is divided.

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+13.00	0.034
0+13.00	0+26.00	0.016
0+26.00	0+39.50	0.013
0+39.50	0+40.00	0.016
0+40.00	0+83.00	0.013
0+83.00	0+95.00	0.022

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	73.95
0+08.00	71.72
0+13.00	72.09
0+26.00	72.44

Tropical Pkwy Q100 EX Sec A **Worksheet for Irregular Channel**

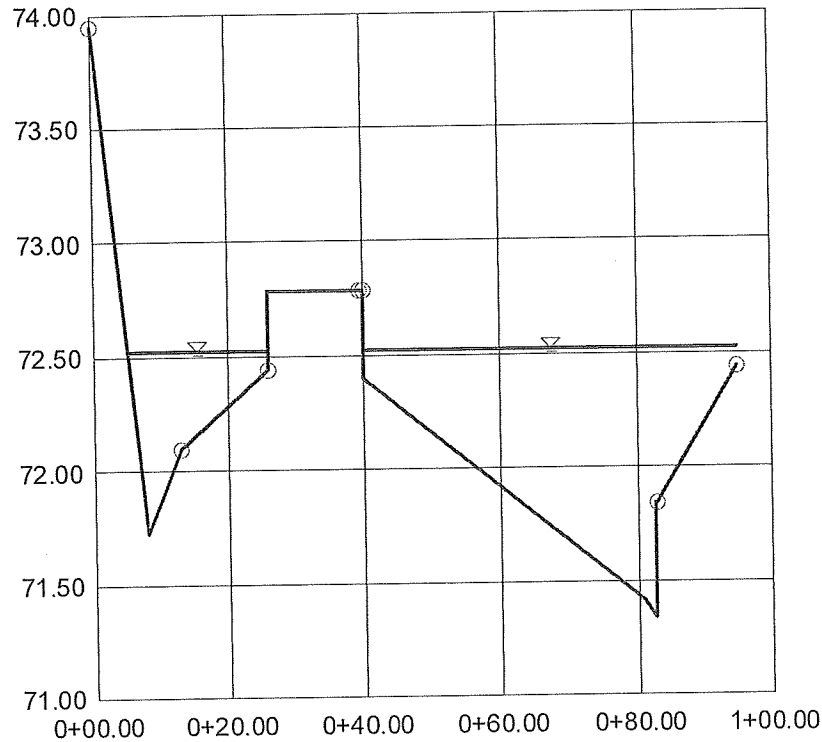
Natural Channel Points	
Station (ft)	Elevation (ft)
0+26.00	72.78
0+26.50	72.78
0+39.50	72.78
0+40.00	72.78
0+40.00	72.40
0+81.00	71.41
0+82.50	71.34
0+82.50	71.84
0+83.00	71.84
0+95.00	72.44

Tropical Pkwy Q100 Ex Sec A

Cross Section for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec A Q100 EX
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.014
Channel Slope	0.70 %
Water Surface Elevation	72.52 ft
Elevation Range	71.34 to 73.95
Discharge	224.00 cfs



V:33.333333
H:1
NTS

Tropical Pkwy Sec B Q10 EX

Worksheet for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec B Q10 EX
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.60 %
Discharge	11.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.016
Water Surface Elevation	66.43 ft
Elevation Range	66.21 to 67.02
Flow Area	4.8 ft ²
Wetted Perimeter	26.42 ft
Top Width	26.22 ft
Actual Depth	0.22 ft
Critical Elevation	66.21 ft
Critical Slope	0.00 %
Velocity	2.29 ft/s
Velocity Head	0.08 ft
Specific Energy	66.51 ft
Froude Number	0.94
Flow Type	Subcritical

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+04.00	0.022
0+04.00	0+29.50	0.016
0+29.50	0+30.00	0.013
0+30.00	0+40.00	0.022

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	67.02
0+04.00	66.30
0+18.00	66.21
0+29.50	66.25
0+29.50	66.74
0+30.00	66.74
0+40.00	67.00

Dry Lane

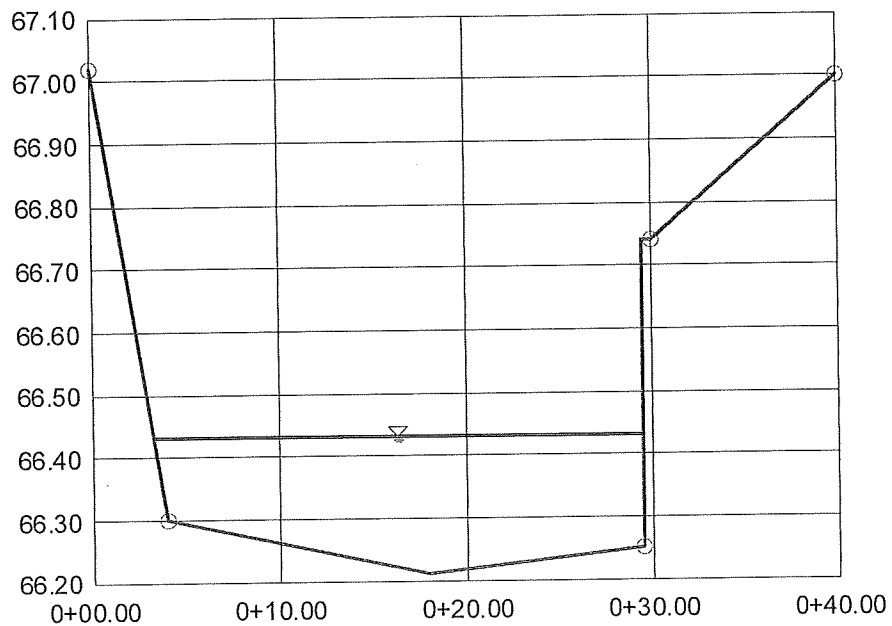
$$\frac{66.25 - 66.43}{0.02} = 0$$
2

Tropical Pkwy Sec B Q10 EX

Cross Section for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec B Q10 EX
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.016
Channel Slope	0.60 %
Water Surface Elevation	66.43 ft
Elevation Range	66.21 to 67.02
Discharge	11.00 cfs



V:33.3333333
H:1
NTS

Tropical Pkwy Sec B Q100 EX Worksheet for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec B Q100 EX
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.60 %
Discharge	230.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.016
Water Surface Elevation	67.35 ft
Elevation Range	66.21 to 67.02
Flow Area	36.0 ft ²
Wetted Perimeter	41.23 ft
Top Width	40.00 ft
Actual Depth	1.14 ft
Critical Elevation	67.46 ft
Critical Slope	0.41 %
Velocity	6.40 ft/s
Velocity Head	0.64 ft
Specific Energy	67.98 ft
Froude Number	1.19
Flow Type	Supercritical

Calculation Messages:

Water elevation exceeds lowest end station by 0.34720672 ft.

$$\checkmark \times \Delta$$

$$\underline{6.4 \times 1.14 = 7.3}$$

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+04.00	0.022
0+04.00	0+29.50	0.016
0+29.50	0+30.00	0.013
0+30.00	0+40.00	0.022

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	67.02
0+04.00	66.30
0+18.00	66.21
0+29.50	66.25
0+29.50	66.74
0+30.00	66.74
0+40.00	67.00

Tropical Pkwy Sec B Q100 EX

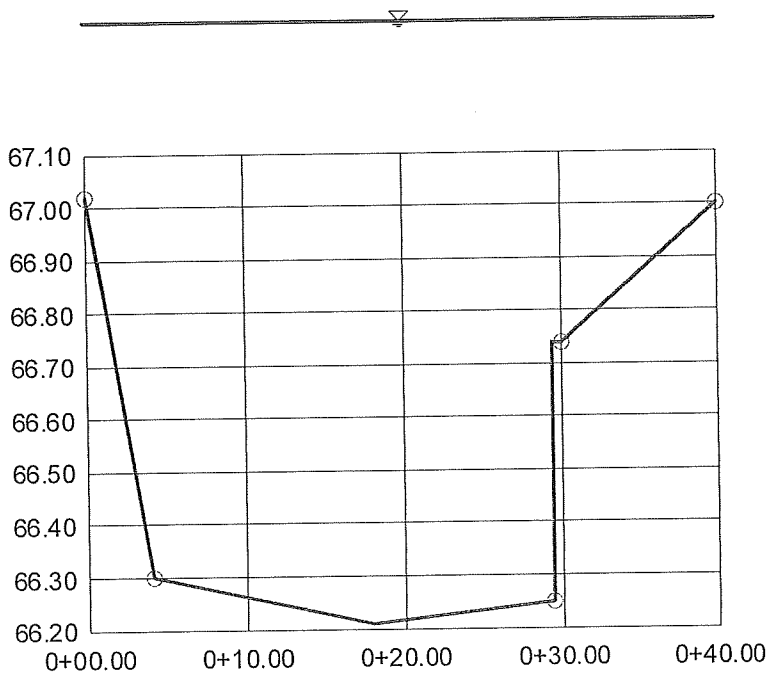
Cross Section for Irregular Channel

Project Description

Worksheet	Tropical Parkway Sec B Q100 EX
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data

Mannings Coefficient	0.016
Channel Slope	0.60 %
Water Surface Elevation	67.35 ft
Elevation Range	66.21 to 67.02
Discharge	230.00 cfs



V:33.333333
H:1
NTS

Tropical Pkwy Q10 INT Sec B

Worksheet for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec B Q10 INT
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.60 %
Discharge	12.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.014
Water Surface Elevation	67.51 ft
Elevation Range	67.05 to 70.44
Flow Area	5.3 ft²
Wetted Perimeter	35.40 ft
Top Width	34.50 ft
Actual Depth	0.46 ft
Critical Elevation	67.51 ft
Critical Slope	0.58 %
Velocity	2.26 ft/s
Velocity Head	0.08 ft
Specific Energy	67.59 ft
Froude Number	1.02
Flow Type	Supercritical

Calculation Messages:
Flow is divided.

$$\frac{67.94 - 67.51}{0.02} = 21.5'$$

016

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+14.00	0.022
0+14.00	0+16.00	0.013
0+16.00	0+52.00	0.016
0+52.00	0+55.00	0.013
0+55.00	1+01.50	0.016
1+01.50	1+03.50	0.013
1+03.50	1+28.50	0.022

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	67.79
0+14.00	67.55
0+14.50	67.55
0+14.50	67.05

Tropical Pkwy Q10 INT Sec B
Worksheet for Irregular Channel

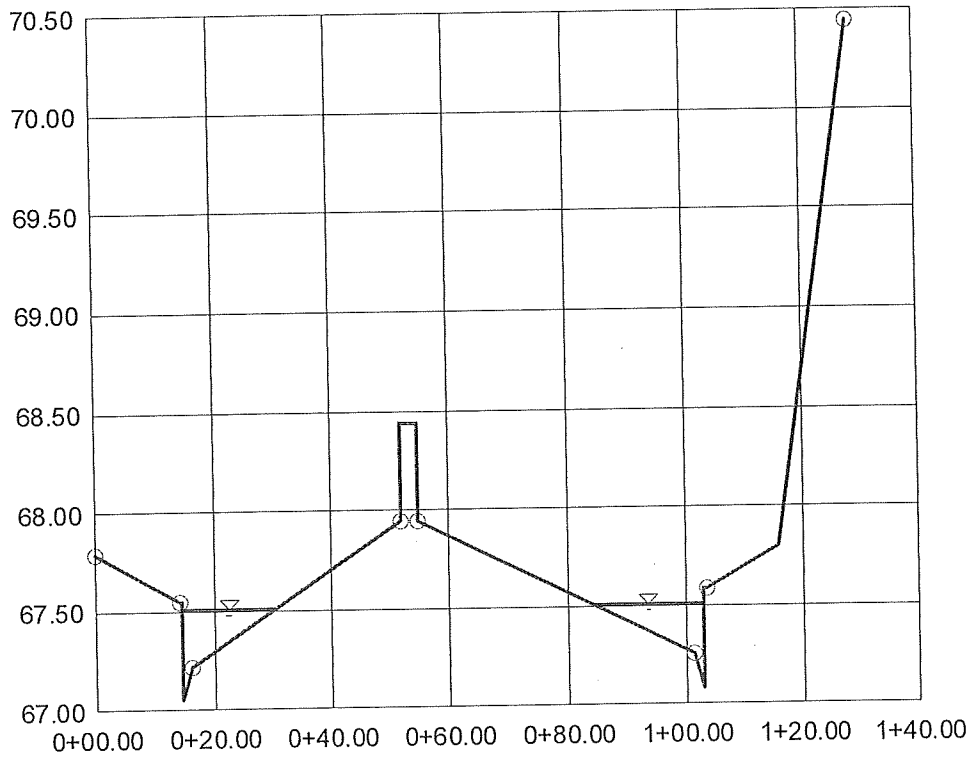
Natural Channel Points	
Station (ft)	Elevation (ft)
0+16.00	67.22
0+52.00	67.94
0+52.00	68.44
0+55.00	68.44
0+55.00	67.94
1+01.50	67.25
1+03.00	67.08
1+03.00	67.58
1+03.50	67.58
1+16.00	67.80
1+28.50	70.44

Tropical Pkwy Q10 INT Sec B

Cross Section for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec B Q10 INT
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.014
Channel Slope	0.60 %
Water Surface Elevation	67.51 ft
Elevation Range	67.05 to 70.44
Discharge	12.00 cfs



V:33.333333
H:1
NTS

Tropical Pkwy Q100 INT Sec B

Worksheet for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec B Q100 INT
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.60 %
Discharge	230.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.016
Water Surface Elevation	68.08 ft
Elevation Range	67.05 to 70.44
Flow Area	54.2 ft ²
Wetted Perimeter	115.93 ft
Top Width	114.31 ft
Actual Depth	1.03 ft
Critical Elevation	68.10 ft
Critical Slope	0.50 %
Velocity	4.25 ft/s
Velocity Head	0.28 ft
Specific Energy	68.36 ft
Froude Number	1.09
Flow Type	Supercritical

Calculation Messages:

Water elevation exceeds lowest end station by 0.28563381 ft.
Flow is divided.

$$\sqrt{4.25 \times 1.03} = 4.4$$

Z
OK

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+14.00	0.022
0+14.00	0+16.00	0.013
0+16.00	0+52.00	0.016
0+52.00	0+55.00	0.013
0+55.00	1+01.50	0.016
1+01.50	1+03.50	0.013
1+03.50	1+28.50	0.022

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	67.79
0+14.00	67.55
0+14.50	67.55

Tropical Pkwy Q100 INT Sec B

Worksheet for Irregular Channel

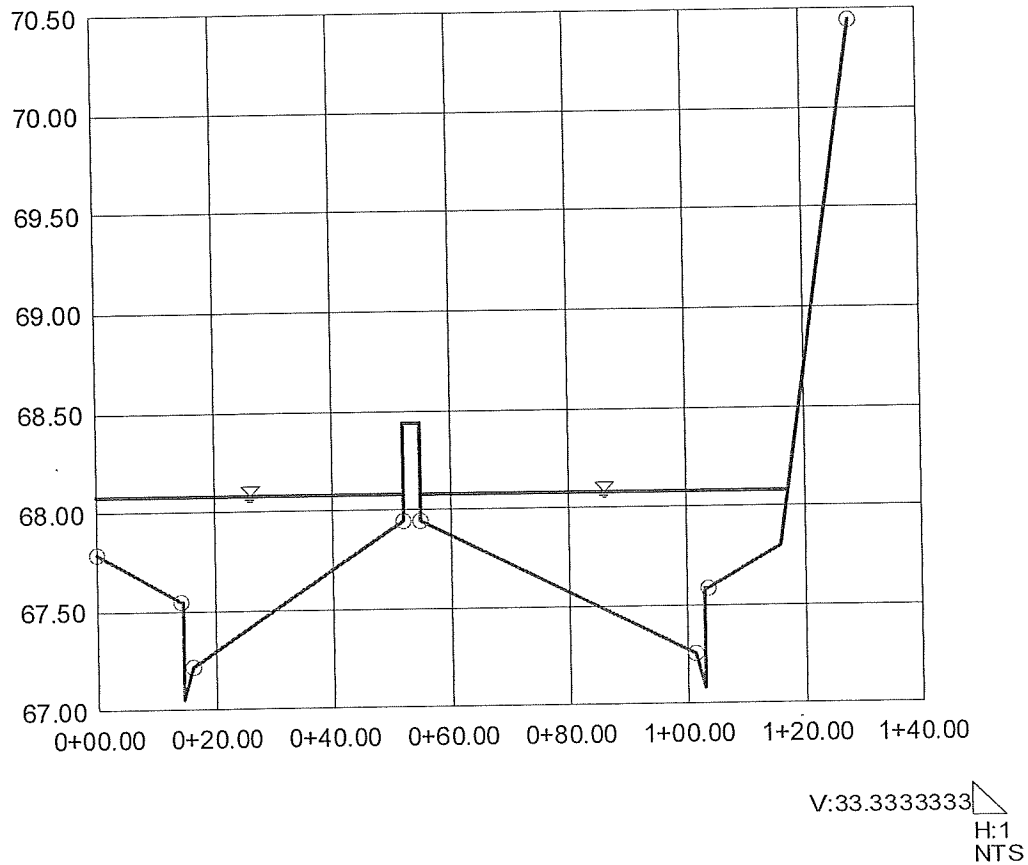
Natural Channel Points	
Station (ft)	Elevation (ft)
0+14.50	67.05
0+16.00	67.22
0+52.00	67.94
0+52.00	68.44
0+55.00	68.44
0+55.00	67.94
1+01.50	67.25
1+03.00	67.08
1+03.00	67.58
1+03.50	67.58
1+16.00	67.80
1+28.50	70.44

Tropical Pkwy Q100 INT Sec B

Cross Section for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec B Q100 INT
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.016
Channel Slope	0.60 %
Water Surface Elevation	68.08 ft
Elevation Range	67.05 to 70.44
Discharge	230.00 cfs



Tropical Pkwy Q10 Dev Sec B Worksheet for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec B Q10 DEV
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.60 %
Discharge	21.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.015
Water Surface Elevation	67.59 ft
Elevation Range	67.05 to 70.44
Flow Area	8.5 ft ²
Wetted Perimeter	48.46 ft
Top Width	47.44 ft
Actual Depth	0.54 ft
Critical Elevation	67.59 ft
Critical Slope	0.57 %
Velocity	2.46 ft/s
Velocity Head	0.09 ft
Specific Energy	67.68 ft
Froude Number	1.02
Flow Type	Supercritical

Calculation Messages:
Flow is divided.

Dry Lane

$$\frac{67.94 - 67.59}{0.02} = 17.5'$$

Z
OK

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+14.00	0.022
0+14.00	0+16.00	0.013
0+16.00	0+52.00	0.016
0+52.00	0+55.00	0.013
0+55.00	1+01.50	0.016
1+01.50	1+03.50	0.013
1+03.50	1+28.50	0.022

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	67.79
0+14.00	67.55
0+14.50	67.55
0+14.50	67.05

Tropical Pkwy Q10 Dev Sec B

Worksheet for Irregular Channel

Natural Channel Points	
Station (ft)	Elevation (ft)
0+16.00	67.22
0+52.00	67.94
0+52.00	68.44
0+55.00	68.44
0+55.00	67.94
1+01.50	67.25
1+03.00	67.08
1+03.00	67.58
1+03.50	67.58
1+16.00	67.80
1+28.50	70.44

Tropical Pkwy Q10 Dev Sec B

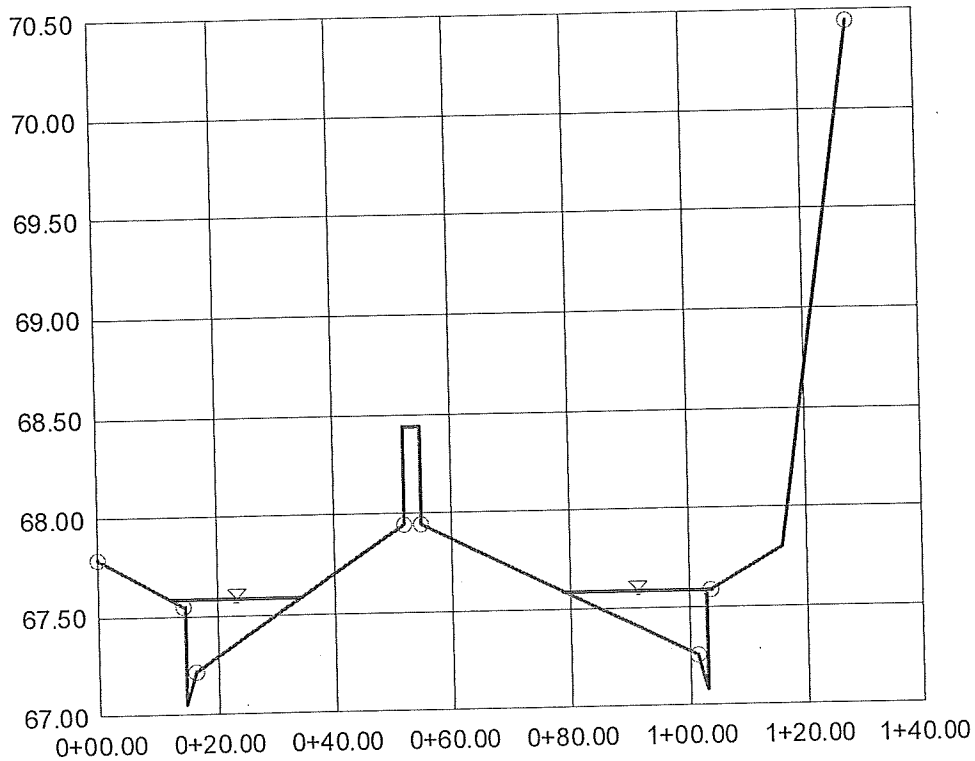
Cross Section for Irregular Channel

Project Description

Worksheet	Tropical Parkway Sec B Q10 DEV
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data

Mannings Coefficient	0.015
Channel Slope	0.60 %
Water Surface Elevation	67.59 ft
Elevation Range	67.05 to 70.44
Discharge	21.00 cfs



V:33.3333333
H:1
NTS

Tropical Pkwy Q100 Dev Sec B Worksheet for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec B Q100 DEV
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.60 %
Discharge	232.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.016
Water Surface Elevation	68.08 ft
Elevation Range	67.05 to 70.44
Flow Area	54.5 ft ²
Wetted Perimeter	115.95 ft
Top Width	114.32 ft
Actual Depth	1.03 ft
Critical Elevation	68.11 ft
Critical Slope	0.50 %
Velocity	4.26 ft/s
Velocity Head	0.28 ft
Specific Energy	68.36 ft
Froude Number	1.09
Flow Type	Supercritical

$$\frac{V \times D}{4.26 \times 1.03 = 4.4}$$

Calculation Messages:
Water elevation exceeds lowest end station by 0.28820327 ft.
Flow is divided.

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+14.00	0.022
0+14.00	0+16.00	0.013
0+16.00	0+52.00	0.016
0+52.00	0+55.00	0.013
0+55.00	1+01.50	0.016
1+01.50	1+03.50	0.013
1+03.50	1+28.50	0.022

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	67.79
0+14.00	67.55
0+14.50	67.55

Tropical Pkwy Q100 Dev Sec B **Worksheet for Irregular Channel**

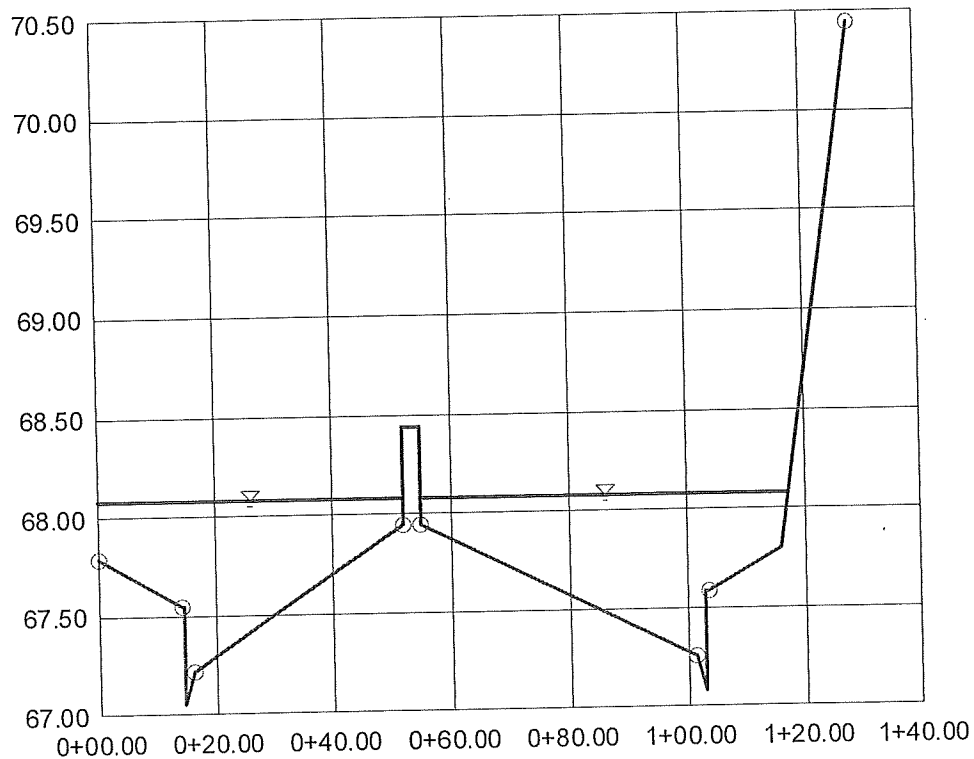
Natural Channel Points	
Station (ft)	Elevation (ft)
0+14.50	67.05
0+16.00	67.22
0+52.00	67.94
0+52.00	68.44
0+55.00	68.44
0+55.00	67.94
1+01.50	67.25
1+03.00	67.08
1+03.00	67.58
1+03.50	67.58
1+16.00	67.80
1+28.50	70.44

Tropical Pkwy Q100 Dev Sec B

Cross Section for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec B Q100 DEV
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.016
Channel Slope	0.60 %
Water Surface Elevation	68.08 ft
Elevation Range	67.05 to 70.44
Discharge	232.00 cfs



V:33.333333
H:1
NTS

Tropical Pkwy Q10 Dev Worksheet for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec A Q10 DEV
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.70 %
Discharge	3.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.013
Water Surface Elevation	71.78 ft
Elevation Range	71.42 to 73.01
Flow Area	1.4 ft ²
Wetted Perimeter	12.75 ft
Top Width	12.20 ft
Actual Depth	0.36 ft
Critical Elevation	71.79 ft
Critical Slope	0.55 %
Velocity	2.15 ft/s
Velocity Head	0.07 ft
Specific Energy	71.85 ft
Froude Number	1.12
Flow Type	Supercritical

Calculation Messages:
Flow is divided.

$$\frac{72.51 - 71.78}{0.02} = 36.5'$$

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+12.00	0.022
0+12.00	0+14.00	0.013
0+14.00	0+50.00	0.016
0+50.00	0+53.00	0.013
0+53.00	0+96.00	0.016
0+96.00	1+03.00	0.013

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	72.44
0+12.00	72.11
0+12.50	72.11
0+12.50	71.61
0+14.00	71.78

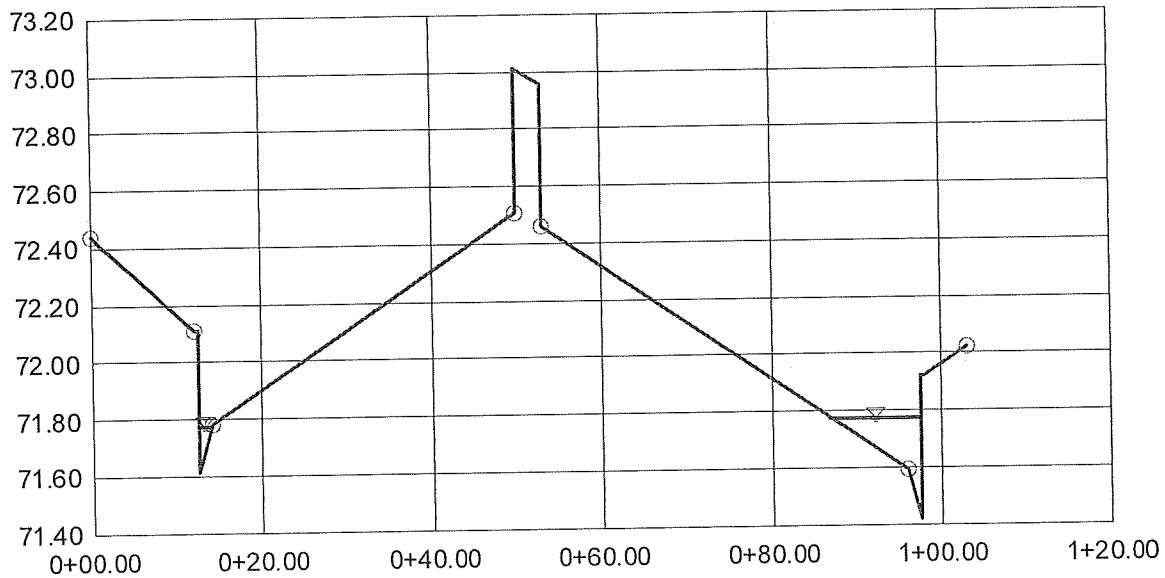
Tropical Pkwy Q10 Dev Worksheet for Irregular Channel

Natural Channel Points	
Station (ft)	Elevation (ft)
0+50.00	72.51
0+50.00	73.01
0+53.00	72.96
0+53.00	72.46
0+96.00	71.59
0+97.50	71.42
0+97.50	71.92
0+98.00	71.92
1+03.00	72.02

Tropical Pkwy Q10 Dev Cross Section for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec A Q10 DEV
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.013
Channel Slope	0.70 %
Water Surface Elevation	71.78 ft
Elevation Range	71.42 to 73.01
Discharge	3.00 cfs



V:33.3333333
H:1
NTS

Sec A

Tropical Pkwy Q100 Dev

Worksheet for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec A Q100 DEV
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.70 %
Discharge	224.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.015
Water Surface Elevation	72.55 ft
Elevation Range	71.42 to 73.01
Flow Area	46.6 ft²
Wetted Perimeter	101.80 ft
Top Width	100.00 ft
Actual Depth	1.13 ft
Critical Elevation	72.62 ft
Critical Slope	0.43 %
Velocity	4.81 ft/s
Velocity Head	0.36 ft
Specific Energy	72.91 ft
Froude Number	1.24
Flow Type	Supercritical

Calculation Messages:

Water elevation exceeds lowest end station by 0.52819847 ft.
Flow is divided.

$$\frac{V \times d}{4.81 \times 1.13 = 5.4}$$

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+12.00	0.022
0+12.00	0+14.00	0.013
0+14.00	0+50.00	0.016
0+50.00	0+53.00	0.013
0+53.00	0+96.00	0.016
0+96.00	1+03.00	0.013

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	72.44
0+12.00	72.11
0+12.50	72.11
0+12.50	71.61

**Tropical Pkwy Q100 Dev
Worksheet for Irregular Channel**

Natural Channel Points	
Station (ft)	Elevation (ft)
0+14.00	71.78
0+50.00	72.51
0+50.00	73.01
0+53.00	72.96
0+53.00	72.46
0+96.00	71.59
0+97.50	71.42
0+97.50	71.92
0+98.00	71.92
1+03.00	72.02

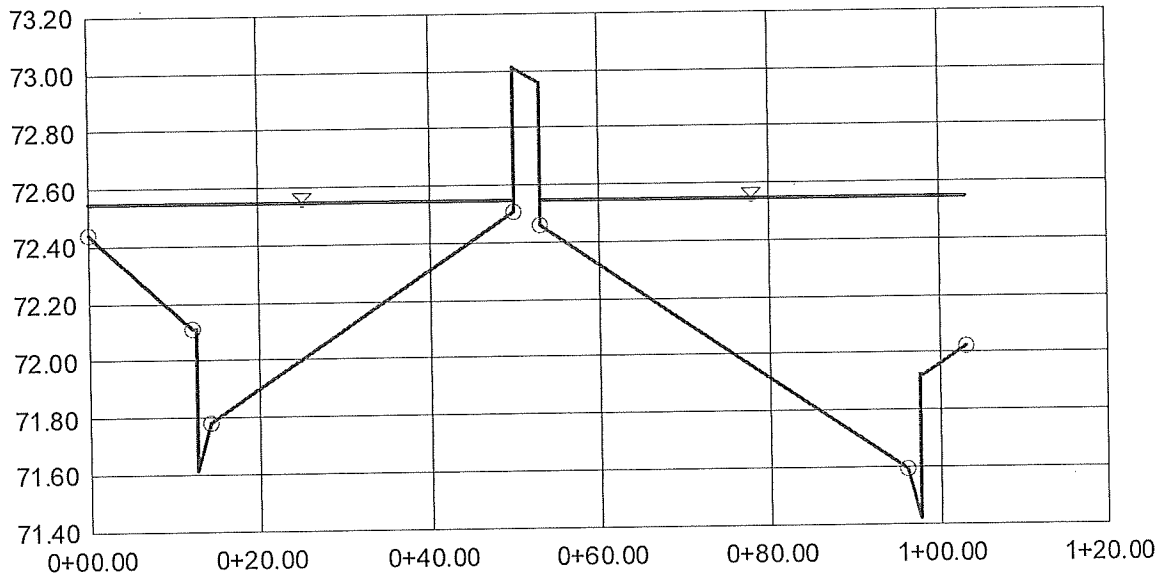
Tropical Pkwy Q100 Dev Cross Section for Irregular Channel

Project Description

Worksheet	Tropical Parkway Sec A Q100 DEV
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data

Mannings Coefficient	0.015
Channel Slope	0.70 %
Water Surface Elevation	72.55 ft
Elevation Range	71.42 to 73.01
Discharge	224.00 cfs



V:33.3333333
H:1
NTS

SEC A

Tropical Pkwy Q10 INT Worksheet for Irregular Channel

Project Description

Worksheet	Tropical Parkway Sec A Q10 INT
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Channel Slope	0.70 %
Discharge	3.00 cfs

Options

Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results

Mannings Coefficient	0.013
Water Surface Elevation	71.78 ft
Elevation Range	71.42 to 73.01
Flow Area	1.4 ft ²
Wetted Perimeter	12.75 ft
Top Width	12.20 ft
Actual Depth	0.36 ft
Critical Elevation	71.79 ft
Critical Slope	0.55 %
Velocity	2.15 ft/s
Velocity Head	0.07 ft
Specific Energy	71.85 ft
Froude Number	1.12
Flow Type	Supercritical

Calculation Messages:
Flow is divided.

Roughness Segments

Start Station	End Station	Mannings Coefficient
0+00.00	0+12.00	0.022
0+12.00	0+14.00	0.013
0+14.00	0+50.00	0.016
0+50.00	0+53.00	0.013
0+53.00	0+96.00	0.016
0+96.00	1+03.00	0.013

Natural Channel Points

Station (ft)	Elevation (ft)
0+00.00	72.44
0+12.00	72.11
0+12.50	72.11
0+12.50	71.61
0+14.00	71.78

Dry Lane

$$\frac{72.51 - 71.78}{0.02} = 36.5'$$

Tropical Pkwy Q10 INT
Worksheet for Irregular Channel

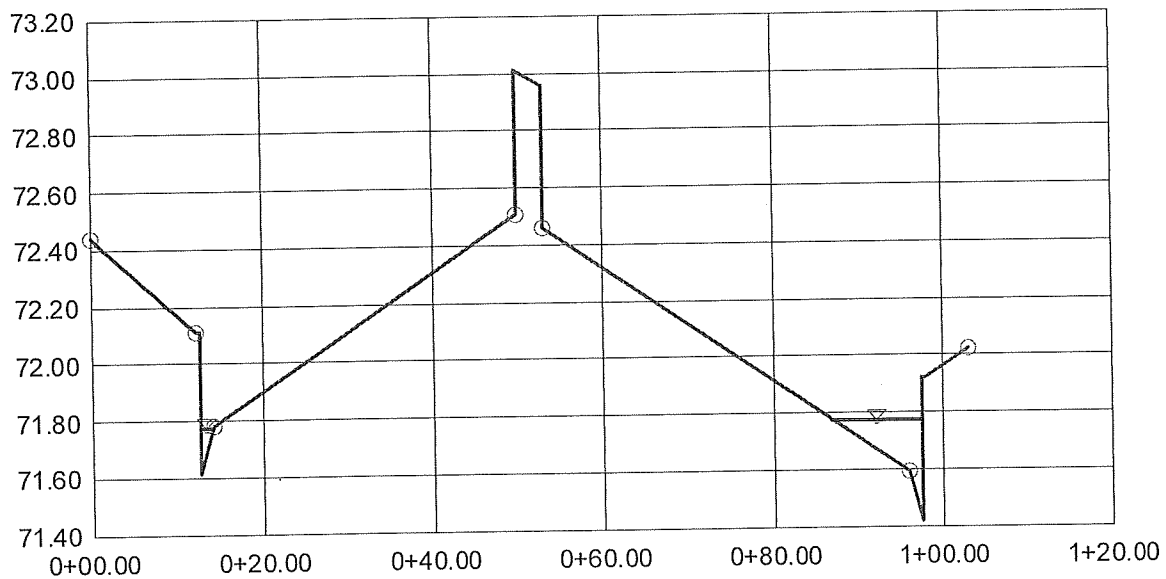
Natural Channel Points	
Station (ft)	Elevation (ft)
0+50.00	72.51
0+50.00	73.01
0+53.00	72.96
0+53.00	72.46
0+96.00	71.59
0+97.50	71.42
0+97.50	71.92
0+98.00	71.92
1+03.00	72.02

Tropical Pkwy Q10 INT

Cross Section for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec A Q10 INT
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.013
Channel Slope	0.70 %
Water Surface Elevation	71.78 ft
Elevation Range	71.42 to 73.01
Discharge	3.00 cfs



V:33.3333333

H:1
NTS

SEC A

Tropical Pkwy Q100 INT Worksheet for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec A Q100 INT
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Channel Slope	0.70 %
Discharge	224.00 cfs

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results	
Mannings Coefficient	0.016
Water Surface Elevation	72.54 ft
Elevation Range	71.42 to 73.01
Flow Area	47.1 ft ²
Wetted Perimeter	101.97 ft
Top Width	100.00 ft
Actual Depth	1.12 ft
Critical Elevation	72.61 ft
Critical Slope	0.45 %
Velocity	4.76 ft/s
Velocity Head	0.35 ft
Specific Energy	72.89 ft
Froude Number	1.22
Flow Type	Supercritical

Calculation Messages:

Water elevation exceeds lowest end station by 0.52148249 ft.
Flow is divided.

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00.00	0+12.00	0.022
0+12.00	0+14.00	0.013
0+14.00	0+50.00	0.016
0+50.00	0+53.00	0.013
0+53.00	0+96.00	0.016
0+96.00	1+03.00	0.013

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00.00	72.24
0+12.00	72.11
0+12.50	72.11
0+12.50	71.61

✓ x ↓
~~Dry Lane~~
 $4.76 \times 1.12 = 5.3$
Z
OK

Tropical Pkwy Q100 INT
Worksheet for Irregular Channel

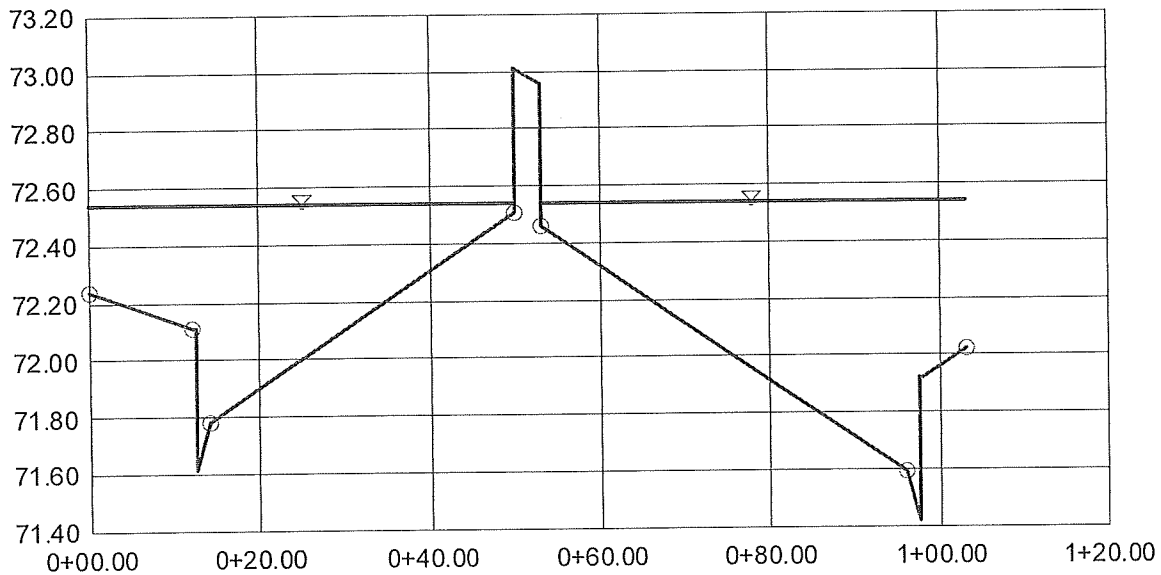
Natural Channel Points	
Station (ft)	Elevation (ft)
0+14.00	71.78
0+50.00	72.51
0+50.00	73.01
0+53.00	72.96
0+53.00	72.46
0+96.00	71.59
0+97.50	71.42
0+97.50	71.92
0+98.00	71.92
1+03.00	72.02

Tropical Pkwy Q100 INT

Cross Section for Irregular Channel

Project Description	
Worksheet	Tropical Parkway Sec A Q100 INT
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.016
Channel Slope	0.70 %
Water Surface Elevation	72.54 ft
Elevation Range	71.42 to 73.01
Discharge	224.00 cfs



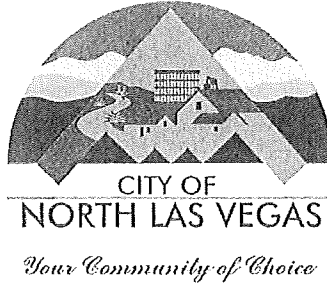
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NTS

APPENDIX G

Response to Comment 14 City of North Las Vegas Comment Letter

Mayor
Shari L. Buck

Council Members
Robert L. Eliason
Anita G. Wood
Pamela A. Goynes-Brown
Wade W. Wagner



City Manager
Timothy R. Hacker

PUBLIC WORKS – DEVELOPMENT AND FLOOD CONTROL
2250 N. Las Vegas Blvd., Suite 220 • North Las Vegas, Nevada 89030
Telephone: (702) 633-1200 • Fax: (702) 649-4696 • TDD: (800) 326-6868
www.cityofnorthlasvegas.com

November 30, 2011

Mailed via: E-mail

Ray Fredericksen, P.E.

Slater Hanifan Group
5740 S Arville Street, Suite #216
Las Vegas, Nevada 89118

**Re: Technical Drainage Study for Tropical Pkwy./Centennial Pkwy. Roadway
Improvements.**
CNLV No. 43988

Dear Mr. Fredericksen :

CNLV staff has reviewed the above referenced study, dated November 7, 2011, and offers the following comments:

1. Concurrence must be obtained by the City of Las Vegas (CLV) due to the proposed improvements's proximity to the CLV jurisdiction. Please submit a copy of this study and all addenda to CLV upon acceptance from CNLV.
2. This Technical Drainage Study (TDS) is only for the proposed street improvements adjacent to the site, a separate drainage study and planning commission conditions must be submitted, in the future, for the undeveloped area within the same parcel.
3. A quick review of the general topography in the area shows that the area surrounding the project site drains southeasterly direction. It appears that Decatur Boulevard, adjacent to the site, may intercept some offsite flows from upstream of the project site.

Section 1.5 of TDS states that "Improvements west pf Decatur have effectively cut off flows and routed them into the existing storm drain in Decatur." Please provide approved reference materials to illustrate that all flows are being contained within the existing storm drain in Decatur Boulevard. Please note that all 10-year and 100-year street capacity calculations must be revised to reflect any flow changes. Also, 12' dry lane criterion must also be met for the future condition.

4. Please note that the CNLV requires that all drop inlet sizing be performed with the HEC-22 software which can be acquired from the Federal Highway Administration's website.

5. Please explain and demonstrate how the $Q_{100}=118$ cfs and $Q_{10}=38$ cfs (hydraulic Section D-D of the Existing Condition Street Flows) were obtained since the flows for the Interim and Future conditions at hydraulic Section D-D are $Q_{100}=3$ cfs and $Q_{10}=2$ cfs.
6. Please explain/show how the $Q_{100}/10$ in This Study and the Twilight Study were obtained in Tables 3 and 5 of the TDS. The flow values in Tables 3 and 5 do not match with the flow values in the drainage basin maps and the reference materials for the Twilight Study.
7. Please explain and demonstrate how the $Q_{approaching}=26$ cfs in Table 8 of the TDS was obtained. The Interim and Future Condition Basin Maps show that $Q_{100}=21$ cfs instead of $Q_{100}=26$ cfs at Section E-E.

Also, it appears that a portion of the $Q_{100}=302$ cfs and $Q_{10}=78$ cfs from Tropical Parkway will turn north adding to the flows in Centennial Parkway at the proposed drop inlets. Please evaluate and perform the necessary flow split calculations and revise all street and drop inlet capacity calculations to reflect the revision as necessary.

8. Please discuss and show how soil type boundaries were determined as delineated on the drainage basin maps? Provide any pertinent soil type chart for the project area.
9. It is unclear where is drainage basin DEC-5 as shown in the Soil and Curve Number Computation table of the TDS.
10. Please revised the Flowmaster calculations for the interim and future conditions of Centennial Parkway and Tropical Parkway to show the proposed concrete median islands.
11. Below are comments pertaining the Improvement Plans:
 - a. If the landscapes areas along the meandering sidewalks are to be installed with the street improvements, the Engineer must show grades and flow lines within all landscape areas. Flows from the landscape areas will not be allowed to sheet flow over the adjacent sidewalks. Drainage swales should be graded to direct flows to discharge into the sidewalk underdrains.
 - b. Since the 100-year depth of flows will overtop the curbs (i.e. Tropical Parkway), the proposed landscape berms used to protect future developed properties from flows in the adjacent streets must meet the criterium of being twice the depth of flow above the adjacent flowline up to 18" above adjacent water surface.

Also, for 100-year street flow with depths greater than 0.6' and velocities higher than 5 fps, erosion resistant landscaping or pony walls must be provided.
 - c. Please note that any proposed storm drains within the public right-of-way must be reinforced concrete pipe with diameter of 18" minimum. Please revise the portion of the proposed storm drain pipe on the east half of Centennial Parkway to reflect the above described requirements. Also, CNLV highly discourages the installation of storm drain under the curb and gutter. Please redesign the proposed storm drain lateral on the east side of Centennial Parkway to locate away from the curb and gutter.
 - d. Please provide the Benchmark information.

- e. The size of the drop inlets on Sheet P-6 are different from the sizes shown in the drop-inlet calculations in the TDS. Please revise the drawing to reflect the correct size of the drop inlets.
 - f. Please provide two driveways per the conditions of the approved Site Plan Review (SPR 11-11). The first driveway should be located on Rice Ave. at approximate station 13+00 and second driveway should be on Tropical Pkwy. at approximate station 108+50.
 - g. Please note that tack-on curb is not allowed in the public ROW. Please revise Sheets P-3 and P-4 to show "A" type curb per CCAUSD #219 for Tropical Pkwy.
 - h. The proposed meandering sidewalk on Tropical Pkwy., at approximate station 105+00, does not tie into the existing sidewalk at that location. Please revise drawing accordingly.
 - i. Since Rice Ave. is a new street (undeveloped on both sides), please submit a design for a new street without saw cutting and matching the existing asphalt pavement. All existing asphalt pavements on Rice Ave. are temporary and need to be removed and a half street improvements with 16' overpaved will be required as part of this development. In addition, a median island and a concrete valley gutter must be constructed within Rice Ave. at Decatur Blvd. intersection.
 - j. Please remove approval signature line for CNLV Traffic Engineer from all Plan and Profile sheets.
12. Additional comments may be generated on the second review.
13. A copy of this letter must accompany the subsequent submittal to the City of North Las Vegas.

It is recommended that the Engineer review the Drainage Study Checklist before resubmitting the drainage study addendum to the City. The City, its officials, or employees assume no liability for information, data, calculations and conclusions presented by the consulting engineers. We, therefore, make no warranties, either expressed or implied, in conducting this review. If you have any questions concerning this matter, please contact me at (702)633-1932.

Sincerely,



Dan Le, P.E., CFM
Senior Engineer
Development and Flood Control Division

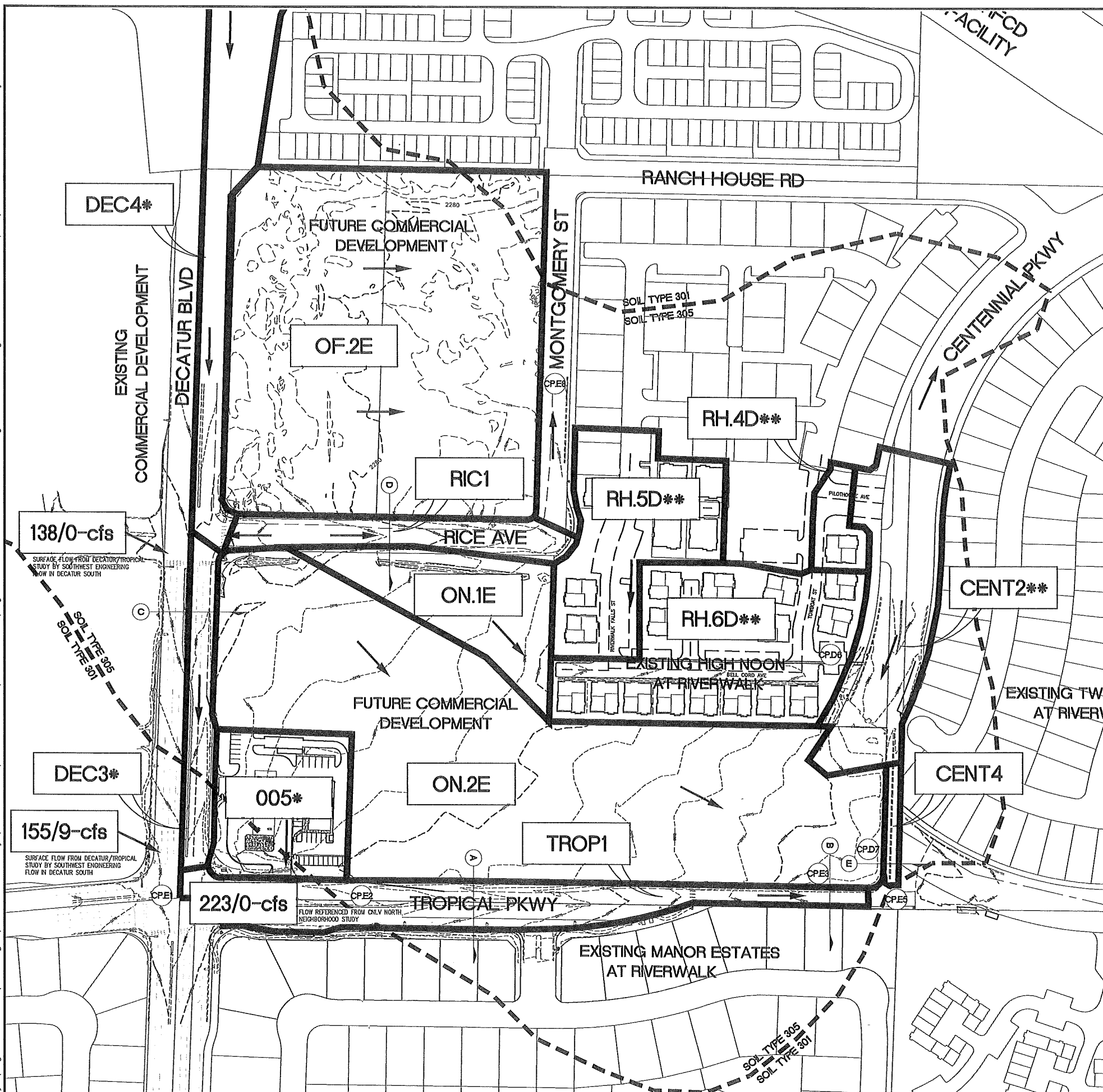
APPENDIX H

Figures

Existing

Interim

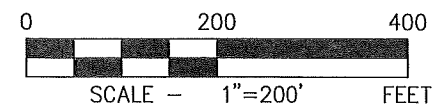
Future



Flow Summary			
Existing Condition			
Subbasin ID	Area (ac)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
DEC.4	2.19	3	6
DEC.3	0.76	1	2
CP.E1	N/A	13	163
005*	1.55	3	5
CP.E2	N/A	3	224
TROP1	2.05	3	6
ON.1E	1.54	1	3
ON.2E	9.7	5	14
CP.E3	N/A	11	230
RH.5D**	2.07	2	5
RH.6D**	3.17	4	8
CP.D6**	N/A	6	13
RH.4D**	0.34	<0.5	1
CENT2**	1.65	3	5
CENT4	0.14	<1	<1
CP.D7	N/A	10	20
CP.E5	N/A	20	233
OF.2E	8.84	5	14
RIC1	0.9	2	3
CP.E8	N/A	6	17

*Referenced from the Tropical Decatur Convenience Store Proposed Condition Analysis, by Kimley Horn
 **Referenced from the Twilight at Riverwalk Ranch Ultimate Condition Analysis, by SHG

Perimeter Street Flow Summary							
Existing Condition							
Section	Slope (%)	Q ₁₀₀ (cfs)	Depth (ft)	Velocity (fps)	VxD	Q ₁₀ (cfs)	Dry Lane Width (ft)
SECTION A Tropical Pkwy (100' ROW) (Q = CP.E2)	0.70	224.0	1.18	5.70	6.7	3.0	39.00
SECTION B Tropical Pkwy (100' ROW) (Q = CP.E3)	0.60	230.0	1.14	6.40	7.3	11.0	0.00
SECTION C Decatur Blvd (100' ROW) (North of C-Store)	0.60	144.0	0.91	3.84	3.5	3.0	22.0
SECTION D Rice Ave (60' ROW) (Q = RIC1)	0.61	118.0	1.03	3.94	4.1	38.0	n/a
SECTION E Centennial Pkwy (100' ROW) (Q = CP.D7)	0.43	20.0	0.63	3.37	2.1	10.0	0.0



LEGEND

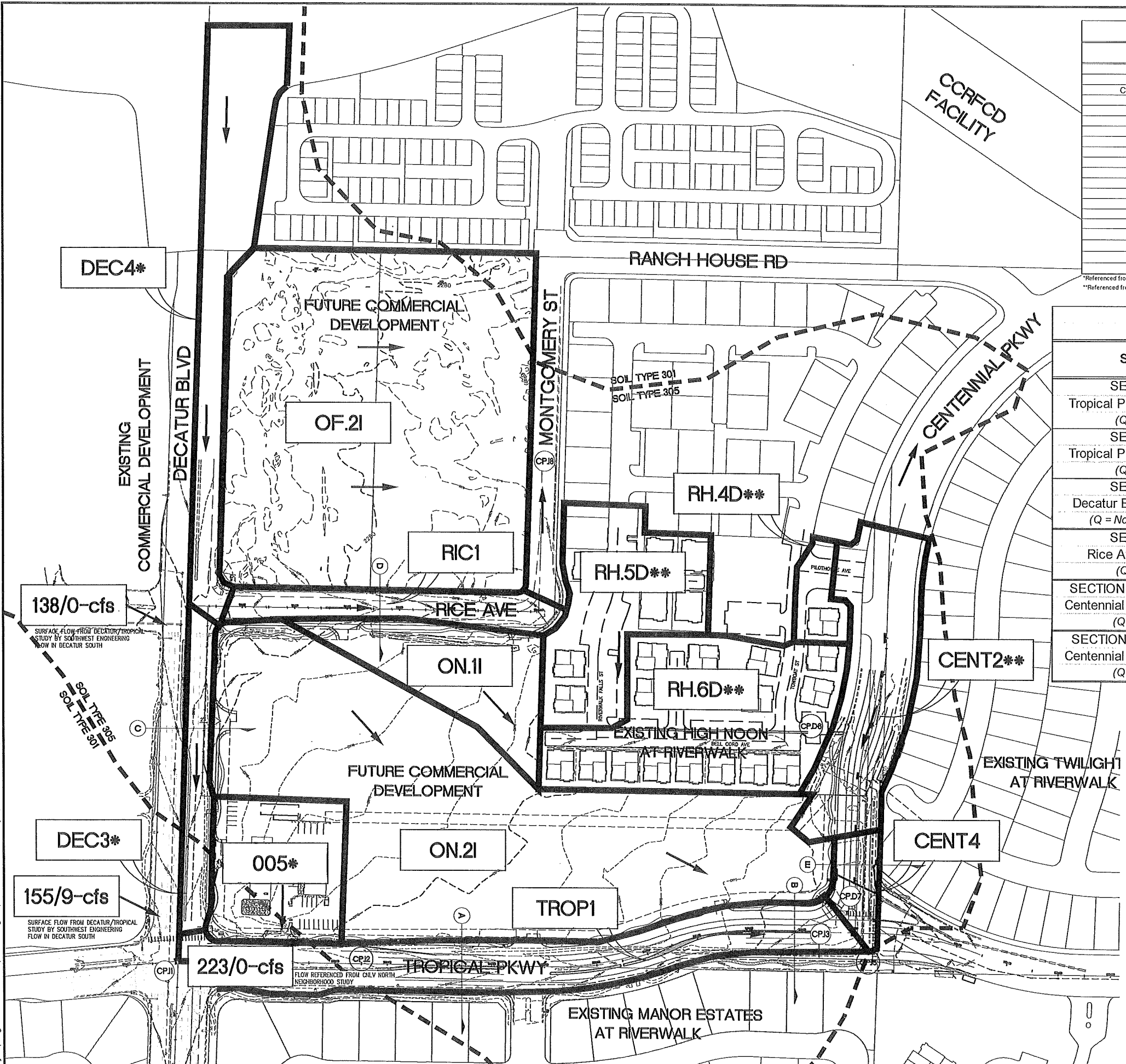
	BASIN BOUNDARY
	BASIN ID
	FLOW DIRECTION
	CONCENTRATION POINT
	SOIL BOUNDARY
	FLOWMASTER SECTION

**S-I-E SLATER
HANIFAN
GROUP**
CONSULTING ENGINEERS & PLANNERS
5740 S. ARVILLE STREET #216, LAS VEGAS, NV 89118
PHONE (702) 284-5300 FAX (702) 284-5399

[illegible]

M GRAPE LLC
TROPICAL PARKWAY REALIGNMENT EXISTING CONDITION BASIN MAP

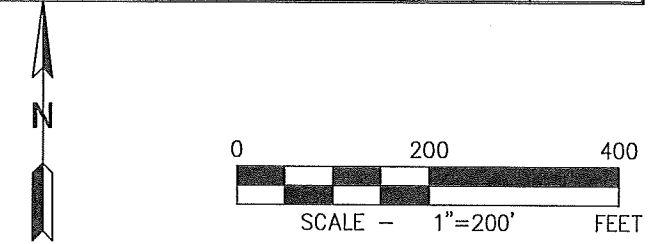
DATE:	9/23/11
DRAFTER:	RFF
DESIGNER:	RFF
CHECKED:	RFF
PROJECT NO.	MGL1101.000
EXHIBIT E	
SHEET 1 OF 3	



Flow Summary Interim Condition				
Subbasin ID	Area (ac)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)	
DEC.4	2.19	3	6	
DEC.3	0.76	1	2	
CP.11 (SOUTH IN DECATUR)	N/A	13	163	INCLUDES flow
005*	1.55	3	5	
CP.12	N/A	3	224	INCLUDES North Neighborhood flows
TROP1	2.69	4	8	0/223 cfs
ON.11	1.54	1	3	
ON.21	8.64	4	13	
CP.13	N/A	12	230	INCLUDES North Neighborhood flows
RH.5D**	2.07	2	5	0/223 cfs
RH.6D**	3.17	4	8	
CP.D6**	N/A	6	13	
RH.4D**	0.34	<0.5	1	
CENT2**	1.65	3	5	
CENT4	0.38	<1	<1	
CP.D7	N/A	10	21	
CP.15	N/A	21	233	INCLUDES North Neighborhood flows
OF.21	8.64	5	14	0/223 cfs
RIC1	0.9	2	3	
CP.18	N/A	6	17	

*Referenced from the Tropical Decatur Convenience Store Proposed Condition Analysis, by Kinney Horn
**Referenced from the Twilight at Riverwalk Ranch Ultimate Condition Analysis, by SHS

Perimeter Street Flow Summary Interim Condition							
Section	Slope (%)	Q ₁₀₀ (cfs)	Depth (ft)	Velocity (fps)	VxD	Q ₁₀ (cfs)	Dry Lane Width (ft)
SECTION A Tropical Pkwy (100' ROW) (Q = CP.12)	0.70	224.0	1.12	4.76	5.3	3.0	36.50
SECTION B Tropical Pkwy (100' ROW) (Q = CP.13)	0.60	230.0	1.03	4.25	4.4	12.0	21.50
SECTION C Decatur Blvd (100' ROW) (Q = North of C-Store)	0.40	144.0	0.98	3.14	3.1	3.0	24.0
SECTION D Rice Ave (60' ROW) (Q = RIC1)	0.61	3.0	0.32	1.62	0.5	2.0	n/a
SECTION E (West 1/2 St) Centennial Pkwy (90' ROW) (Q = CP.D7)	0.70	17.0	0.52	2.57	1.3	8.0	36'
SECTION E (East 1/2 St) Centennial Pkwy (90' ROW) (Q = CP.D7)	0.90	4.0	0.31	1.79	0.6	2.0	36'



LEGEND

BASIN BOUNDARY

ON-D1

BASIN ID

FLOW DIRECTION

PT1

CONCENTRATION POINT

SOIL BOUNDARY

000

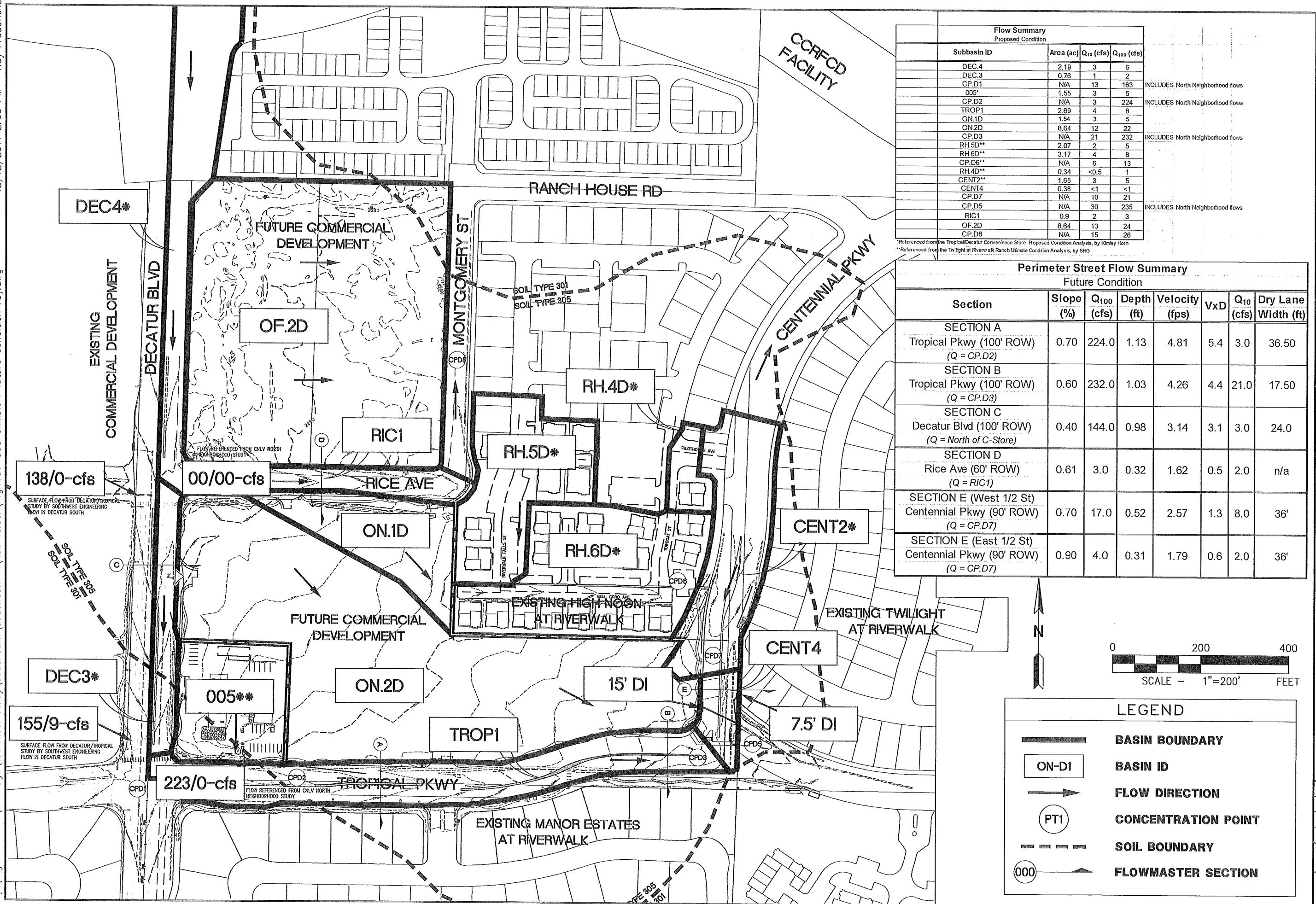
FLOWMASTER SECTION

SLATER
HANIFAN
GROUP
CONSULTING ENGINEERS & PLANNERS
5740 S. ARVILLE STREET #216, LAS VEGAS, NV 89118
PHONE (702) 284-5300 FAX (702) 284-5399

DATE: 9/23/11
DRAFTER: RFF
DESIGNER: RFF
CHECKED: RFF
PROJECT NO.
MGL1101.000
EXHIBIT F
SHEET 2 OF 3

M GRAPE LLC

TROPICAL PARKWAY REALIGNMENT
INTERIM CONDITION BASIN MAP



	Flow Summary Proposed Condition			
	Subbasin ID	Area (ac)	Q ₁₀ (cfs)	Q ₁₀₀ (cfs)
	DEC.4	2.19	3	6
	DEC.3	0.76	1	2
	CP.D1	N/A	13	163
	005*	1.55	3	5
	CP.D2	N/A	3	224
	TROP1	2.69	4	8
	ON.1D	1.54	3	5
	ON.2D	8.64	12	22
	CP.D3	N/A	21	232
	RH.5D**	2.07	2	5
	RH.6D**	3.17	4	8
	CP.D6**	N/A	6	13
	RH.4D**	0.34	<0.5	1
	CENT2**	1.65	3	5
	CENT4	0.38	<1	<1
	CP.D7	N/A	10	21
	CP.D5	N/A	30	235
	RIC1	0.9	2	3
	OF.2D	8.64	13	24
	CP.D8	N/A	15	26

Perimeter Street Flow Summary							
Future Condition							
Section	Slope (%)	Q ₁₀₀ (cfs)	Depth (ft)	Velocity (fps)	VxD	Q ₁₀ (cfs)	Dry Lane Width (ft)
SECTION A Tropical Pkwy (100' ROW) (Q = CP.D2)	0.70	224.0	1.13	4.81	5.4	3.0	36.50
SECTION B Tropical Pkwy (100' ROW) (Q = CP.D3)	0.60	232.0	1.03	4.26	4.4	21.0	17.50
SECTION C Decatur Blvd (100' ROW) (Q = North of C-Store)	0.40	144.0	0.98	3.14	3.1	3.0	24.0
SECTION D Rice Ave (60' ROW) (Q = RIC1)	0.61	3.0	0.32	1.62	0.5	2.0	n/a
SECTION E (West 1/2 St) Centennial Pkwy (90' ROW) (Q = CP.D7)	0.70	17.0	0.52	2.57	1.3	8.0	36'
SECTION E (East 1/2 St) Centennial Pkwy (90' ROW) (Q = CP.D7)	0.90	4.0	0.31	1.79	0.6	2.0	36'

S-I-G SLATER
HANIFAN
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CONSULTING ENGINEERS & PLANNERS

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PHONE (702) 284-5300 FAX (702) 284-5399

[illegible]

M GRAPE, LLC.

TROPICAL PARKWAY REALIGNMENT

FUTURE CONDITION BASIN MAP

DATE:	9/23/11
DRAFTER:	RFF
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PROJECT NO.	MGL1101.000
EXHIBIT G	
SHEET 3 OF 3	